

NASA Contractor Report 4659

M-46 44415

Aircraft Emission Inventories Projected in Year 2015 for a High Speed Civil Transport (HSCT) Universal Airline Network

Steven L. Baughcum and Stephen C. Henderson

grand to the second of the sec

16.50



Aircraft Emission Inventories Projected in Year 2015 for a High Speed Civil Transport (HSCT) Universal Airline Network

Steven L. Baughcum and Stephen C. Henderson Boeing Commercial Airplane Group • Seattle, Washington

Printed copies available from the following:

NASA Center for AeroSpace Information 800 Elkridge Landing Road Linthicum Heights, MD 21090-2934 (301) 621-0390 National Technical Information Service (NTIS) 5285 Port Royal Road Springfield, VA 22161-2171 (703) 487-4650

Executive Summary

This report describes the development of a database of aircraft fuel burned and emissions from projected fleets of high speed civil transports (HSCTs) on a universal airline network. Inventories for 500 and 1000 HSCT fleets were calculated. Inventories of Year 2015 subsonic aircraft fleets in service with these HSCT fleets were also calculated. These emissions inventories were developed under the NASA High Speed Research Systems Studies (HSRSS) contract NAS1-19360, Task Assignment 40.

The objective of this work was to evaluate the changes in geographical distribution of the HSCT emissions as the fleet size grew from 500 to 1000 HSCTs. For this work, a new expanded HSCT network has been used and flights projected using a market penetration analysis rather than assuming equal penetration (as was assumed for the emission scenarios developed for the 1993 AESA assessment). Emission inventories on this network were calculated for both Mach 2.0 and Mach 2.4 HSCT fleets with NOx cruise emission indices of approximately 5 and 15 grams NOx/kilogram fuel.

These emissions inventories will be available for use by atmospheric scientists conducting the Atmospheric Effects of Stratospheric Aircraft (AESA) modeling studies. Fuel burned and emissions of nitrogen oxides (NOx as NO₂), carbon monoxide, and hydrocarbons have been calculated on a 1 degree latitude x 1 degree longitude x 1 kilometer altitude grid and delivered to NASA as electronic files. This report describes the assumptions and methodology for the calculations and summarizes the results of these calculations.

The work presented here shows that the total global fuel burned and emissions from a fleet of 500 HSCTs is not very different whether the expanded HSCT network or the 1993 AESA assessment network is used. The geographical distribution of emissions at stratospheric cruise is sensitive to the market penetration assumptions used to distribute projected HSCT passenger demand.

An increase in HSCT fleet size from 500 to 1000 units has been shown to approximately double emissions at stratospheric cruise. However, as the fleet grows, emissions in different geographical regions grow at different rates. Consequently, stratospheric emissions in northern mid-latitudes are not projected to double as the fleet size doubles, while emissions in the northern tropics and southern hemisphere mid-latitudes are expected to more than double.

For an HSCT combustor with a NOx emission index of 5, the analyses show that the total NOx emissions below 13 kilometers altitude are not very sensitive to the presence or absence of an HSCT fleet. This suggests that to first-order the assessment of the effects of an HSCT fleet are largely decoupled from the assessment of subsonic aircraft effects.

During this work, we discovered several errors made in our previous study (NASA CR 4592) and present the corrected data in this report. For the HSCT, it was found that the operating empty weight used in the emission scenario calculation had been incorrectly entered into the analysis data file and was not consistent with the performance data for the baseline model used in the study. This was corrected and revised emission inventories for Mach 2.0 and Mach 2.4 HSCTs on the 1993 AESA assessment network were calculated. delivered to NASA Langley, and described in this report. The fuel burned for the revised Mach 2.4 HSCT scenario on the 1993 AESA assessment network increased by 7% and the cruise altitude decreased by about 1100 feet when compared with the results presented earlier in NASA CR 4592. In addition, the fuel performance improvement factor for the very large aircraft (P900) projected for 2015 was incorrectly implemented. This was corrected and revised 2015 subsonic aircraft emission scenarios are described in this report. This correction increased the total projected fuel burned by a future all subsonic fleet by 2 %, well below the uncertainty in projected future emissions.

Table of Contents

Sect	tion Title	Page
Table List of	cutive Summary e of Contents of Figures of Tables sary	iii V Vii Xi Xiii
1.	Introduction	1
2.	New expanded HSCT Network	4
	 2.1 Total Passenger Demand Forecast for 2015 2.2 HSCT Universal Route System 2.3 Passenger Traffic Demand - Market Penetration 2.4 HSCT Flight Paths - Waypoint Routing 2.5 HSCT Scheduling 2.6 2015 Subsonic Traffic 	4 5 5 10 14 14
3.	Emissions Calculation Procedure	15
	 3.1 Overview of Emissions Calculation 3.2 HSCT Description 3.3 Mission Profiles 3.4 Emissions Calculation Procedures 	15 16 18 21
4.	Emission Inventory Results	24
	4.1 Mach 2.4 HSCT fleet results4.2 Mach 2.0 HSCT fleet results4.3 2015 Subsonic fleet results	26 37 39
5.	Analysis and Discussion	42
	5.1 Comparison of HSCT fleet emissions with old network results	42
	 5.2 Fleet growth effects 5.3 Comparison of fleet growth effects on 2015 subsonic emissions inventory 	47 52
	5.4 Total 2015 Aircraft emissions for fleets of 0, 500, and 1000 HSCTs	53
	5.5 Conclusions 5.6 Database Availability	56 56
6.	References	57

Table of Contents (cont)

Section Title

Appendix A. World Passenger Demand Forecast

Appendix B. HSCT Routes System Gateway Cities

Appendix C. HSCT Departure Statistics

Appendix D. HSCT Routing Table

Appendix E. Universal Airline System Scheduling

Appendix F. Altitude Distribution of Emissions for Mach 2.4 HSCT Fleets

Appendix G. Altitude Distribution of Emissions for Mach 2.0 HSCT Fleets

Appendix H. Altitude Distribution of Emissions for Year 2015

Subsonic Fleets

Appendix I. Three Dimensional Scenario Data Format

List of Figures

Figure No.	Title	Page
Figure 2-1.	Universal Network Route System, 500 HSCT fleet	7
Figure 2-2.	Universal Network Route System, 1000 HSCT fleet	8
Figure 2-3.	Universal Network Route System, New Routes added when increasing fleet to 1000 HSCTs.	9
Figure 2-4.	Example of Waypoint Routing	11
Figure 2.5	Waypoint Routing Efficiency	12
Figure 2.6	Trip Time Savings - HSCT Fleets	13
Figure 3-1.	Mach 2.4 HSCT Characteristics	17
Figure 3-2.	Mission profile for Mach 2.4 HSCT from Seattle to Tokyo.	20
Figure 3-3.	Mission profile for Mach 2.4 HSCT from Seattle to London.	21
Figure 4-1	NOx emissions for a fleet of 500 Mach 2.4 HSCTs on the universal airline network as a function of altitude and latitude (top panel) and as a function of latitude and longitude (bottom panel).	28
Figure 4-2	Fuel burned and emissions as a function of altitude for the universal HSCT network for fleets of 500 (dashed line) and 1000 (solid line) Mach 2.4 HSCTs with an EI(NOx) of approximately 5 at supersonic cruise.	30
Figure 4-3	Cumulative fraction of fuel burned and emissions as a function of altitude for the universal HSCT network for fleets of 500 (dashed line) and 1000 (solid line) Mach 2.4 HSCTs with an EI(NOx) of approximately 5 at supersonic cruise.	31
Figure 4-4	Emission indices as a function of altitude for the universal HSCT network for fleets of 500 (dashed line) and 1000 (solid line) Mach 2.4 HSCTs with an El(NOx) of approximately 5 at supersonic cruise.	32
Figure 4-5	Fuel burned and emissions as a function of latitude for the universal HSCT network for a fleet of 500 Mach 2.4 HSCTs with an approximate EI(NOx) of 5 at supersonic cruise.	33

List of Figures (cont)

Figure No.	Title	Page
Figure 4-6	Cumulative fraction of fuel burned and emissions as a function of latitude for the universal HSCT network for fleets of 500 (dashed line) and 1000 (solid line) Mach 2.4 HSCTs with an EI(NOx) of approximately 5 at supersonic cruise.	34
Figure 4-7	Fuel burned and emissions above 13 km altitude as a function of latitude for the universal HSCT network for fleets of 500 (dashed line) and 1000 (solid line) Mach 2.4 HSCTs with an EI(NOx) of approximately 5 at supersonic cruise.	35
Figure 4-8	Cumulative fraction of fuel burn and emissions above 13 km altitude as a function of latitude for the universal HSCT network for fleets of 500 (dashed line) and 1000 (solid line) Mach 2.4 HSCTs with an EI(NOx) of approximately 5 at supersonic cruise.	36
Figure 5-1	Comparison of NOx emissions from the universal airline network and the revised 1993 AESA assessment network for 500 Mach 2.4 [EI(NOx)=5] HSCTs.	43
Figure 5-2	NOx emissions above 13 kilometers as a function of latitude, comparing the new universal airline scenario with the 1993 AESA assessment network scenario (revised) for 500 Mach 2.4 HSCTs.	44
Figure 5-3	Differences in fuel burn and NOx emissions between the new universal HSCT network and the 1993 AESA assessment network (revised) for a fleet of 500 Mach 2.4 HSCTs with EI(NOx) at cruise of approximately 5 as a function of latitude.	45
Figure 5-4	Cumulative fraction of NOx emissions above 13 km as a function of latitude, comparing the universal airline network with the AESA assessment network (revised) for the Mach 2.4 HSCT (EI(NOx)=5).	46
Figure 5-5	Stratospheric NOx injections as a function of latitude for 500 and 1000 HSCTs on the universal airline network.	47

List of Figures (cont)

Figure No.	Title	Page
Figure 5-6	NOx emissions above 13 kilometers, comparing a fleet of 1000 HSCTs with doubling the results for a 500 HSCT fleet.	48
Figure 5-7	Comparison of NOx emissions from the 1000 HSCT fleet with emissions from doubling the 500 HSCT fleet on the universal airline network for Mach 2.4, [EI(NOx)=5] HSCTs.	49
Figure 5-8	Differences in fuel burn and NOx emissions between 1000 HSCTs and simply doubling the 500 HSCT fleet, as a function of latitude for the new universal HSCT network.	51
Figure 5-9	Cumulative fraction of stratospheric NOx emissions as a function of latitude for the 500 and 1000 HSCT fleets on the universal airline network.	52
Figure 5-10	Total projected NOx emissions from 2015 scheduled air traffic for different altitude bands for fleets of 0, 500, and 1000 Mach 2.4 HSCTs with EI(NOx) at supersonic cruise of approximately 5.	55

List of Tables

Table No.	Title	Page
Table 2-1.	World Traffic Forecast	4
Table 2-2.	Example of waypoint routing - Frankfurt to Bangkok	10
Table 2-3.	Utilization statistics for the universal airline HSCT network.	14
Table 3-1.	Recommended emission indices in units of grams emission/kilogram fuel for 1990 and 2015.	15
Table 3-2.	Summary of HSCT aircraft characteristics used in the development of the Mach 2.0 and Mach 2.4 HSCT emission scenarios.	16
Table 4-1	Summary of departure statistics for HSCT networks.	24
Table 4-2	Summary of fuel use and emissions for the different scenarios.	25
Table 4-3	Daily mileage, fuel consumption, NOx emissions, and NOx emission index for the Mach 2.4 HSCT, EI=5 flight segments (Universal Network, 500 HSCTs)	26
Table 4-4	Daily mileage, fuel consumption, NOx emissions, and NOx emission index for the Mach 2.4 HSCT, EI=5 flight segments (Universal Network, 1000 HSCTs)	27
Table 4-5	Daily mileage, fuel consumption, NOx emissions, and NOx emission index for the Mach 2.4 HSCT, EI=5 flight segments (1993 AESA assessment network(revised), 500 HSCTs)	27
Table 4-6	Daily mileage, fuel consumption, NOx emissions, and NOx emission index for the Mach 2.0 HSCT, EI=5 flight segments (Universal Network, passenger demand corresponding to 500 Mach 2.4 HSCTs)	37
Table 4-7	Daily mileage, fuel consumption, NOx emissions, and NOx emission index for the Mach 2.0 HSCT, EI=5 flight segments (Universal Network, passenger demand corresponding to 1000 Mach 2.4 HSCTs)	38

List of Tables (cont)

Table No.	Title	Page
Table 4-8	Daily mileage, fuel consumption, NOx emissions, and NOx emission index for the Mach 2.0 HSCT, El=5 flight segments (1993 AESA assessment network, passenger demand corresponding to 500 Mach 2.4 HSCTs)	38
Table 4-9	Classes of "Generic" Subsonic Passenger Aircraft used in the 2015 Scenario Construction	39
Table 4-10	Globally Computed Fuel Burned, emissions, and emission indices by aircraft type for 2015 scheduled subsonic airliners if 500 Mach 2.4 HSCTs are in operation on the universal network.	40
Table 4-11	Globally Computed Fuel Burned, emissions, and emission indices by aircraft type for 2015 scheduled subsonic airliners if 1000 Mach 2.4 HSCTs are in operation on the universal network.	40
Table 4-12	Globally Computed Fuel Burned, emissions, and emission indices by aircraft type for 2015 scheduled subsonic airliners if no HSCT fleet exists	41
Table 5-1	Comparison of the new universal network fuel use and emissions with the revised 1993 AESA assessment network results.	42
Table 5-2	Comparison of the fuel use and emissions between the 500 and 1000 aircraft HSCT fleets.	47
Table 5-3	Comparison of the fuel use and emissions for the subsonic scheduled passenger fleets with and without the HSCT fleets.	53
Table 5-4	Summary of fuel use, NOx, hydrocarbons, and carbon monoxides for the total scheduled air traffic scenarios for 2015.	54

GLOSSARY

AEAP Atmospheric Effects of Aviation Project
AESA Atmospheric Effects of Stratospheric Aircraft

APU Auxiliary power unit

ASM Available seat mile (the number of seats an airline provides

times the number of miles they are flown)

ATC Air traffic control

ATM Available ton-miles (the number of tons capable of being

carried times the number of miles flown)

BCAG Boeing Commercial Airplane Group
BMAP Boeing Mission Analysis Process

CO Carbon Monoxide CO₂ Carbon Dioxide

EI(CO) Emission Index (grams CO/kg fuel burn)

EI(HC) Emission Index [grams hydrocarbon (as CH4)/kg fuel burn]

EI(NOx) Emission Index (grams NOx (as NO₂)/kg fuel burn)

FAA Federal Aviation Administration
GAEC Global Atmospheric Emissions Code

GCD Great circle distance GE General Electric

gm gram

HC Unburned hydrocarbon

H₂O Water

HSCT High Speed Civil Transport

HSRP High Speed Research Program (NASA)
ICAO International Civil Aviation Organization
ISA International standard atmosphere

kg kilogram Ib pound

Load Factor Percentage of an airplane's seat capacity occupied by

passengers on a given flight

LTO cycle Landing takeoff cycle

M Mach number

MDC McDonnell Douglas Corporation

MTOW Maximum takeoff weight

NASA National Aeronautics and Space Administration

nm Nautical mile

NOx Oxides of nitrogen (NO + NO₂) in units of gram equivalent

NO₂

OAG Official Airline Guide
OEW Operating Empty Weight

P&W Pratt & Whitney
PAX passengers
RAM Revenue air mile

RPM Revenue passenger miles (the number of paying

passengers times the number of miles they fly)

RTM Revenue ton-miles (number of tons carried times the number of miles flown)

Sulfur dioxide SO₂

Turbine bypass engine Takeoff gross weight TBE TOGW

ton 2000 pounds

Three dimensional 3D

1. Introduction

A major goal of the NASA High Speed Research Program (HSRP) and of the Boeing High Speed Civil Transport (HSCT) program is to design an HSCT that will not cause a significant impact on the stratospheric ozone layer. To help achieve that goal, NASA has funded the Atmospheric Effects of Stratospheric Aircraft (AESA) project to assess the effect of a fleet of commercial supersonic transports on the atmosphere. To support that assessment, Boeing was contracted to calculate three-dimensional inventories of emissions from fleets of HSCTs. Scenarios of projected subsonic air traffic, both with and without HSCT fleets, were also calculated for use in the atmospheric assessment. Both HSCT and subsonic fleets were projected for the year 2015.

Earlier projections of HSCT emission inventories used in the 1993 AESA assessment were based on an average of Boeing and McDonnell Douglas forecasts to project future passenger demand. (Baughcum, et. al., 1994; Wuebbles, et. al., 1993; Landau, et. al., 1994) Simple ground rules were defined to identify the accessible HSCT market and to create projected departure schedules. Market penetration (the proportion of the passenger demand captured by the HSCT) was assumed to be equal for all HSCT city pairs. Emission scenarios were calculated for Mach 2.0 and Mach 2.4 HSCT fleets by Boeing (Baughcum, et. al., 1994) and for Mach 1.6 by McDonnell Douglas. (Landau, et. al., 1994)

Two-dimensional modeling calculations have shown that the HSCT impact on the ozone layer depends on both the amount of NOx emissions injected into the stratosphere and on the HSCT flight altitudes. (Albritton, et. al., 1993; Stolarski and Wesoky, 1993). More recent calculations have shown that the calculated impact depends on the geographical location as well. (Considine, et. al., 1995) Their model predicts that flights in the tropics will have a much larger impact than flights at mid-latitudes. Thus, in developing emission scenarios, it is important that we realistically project the geographical location of future flights, as well as the total quantity of emissions. It is also important that we understand how sensitive these geographical distributions of emissions are to our assumptions about the HSCT market.

The work presented herein is an extension of the earlier Boeing work (Baughcum, et. al., 1994) of scheduled air traffic emissions. For this study, the Boeing baseline forecast (Boeing, 1993) of passenger demand has been projected to year 2015. A new HSCT route system and schedule have been developed with HSCT passenger demand calculated via a market penetration analysis, rather than assuming that penetrations of all markets will be equal. The flights were then scheduled assuming a single universal airline. As with the previous study, it was assumed that the HSCT would fly supersonically only over water.

The work presented here is for fleets of approximately 500 and 1000 HSCTs in active flight operations. (The total number manufactured would be higher to account for maintenance, inspections, etc.)

Future fleets of HSCTs must be able to compete economically with subsonic aircraft; so,the HSCT will be utilized on routes which can take advantage of its speed. Since it is anticipated that the HSCT will only fly supersonically over water, this means that some routes will be more attractive than others. In this study, the HSCT market capture for flights between individual cities is calculated explicitly taking into account the time saved by supersonic flights. It is believed that this will give a more realistic geographical distribution of future HSCT emissions than was obtained with the scenarios calculated for the 1993 AESA assessment, which assumed equal market penetration for all city pairs which satisfied certain simple ground rules.

In order to evaluate how growth of an HSCT fleet would alter the geographical distribution of HSCT emissions used in the AESA assessments, schedules corresponding to the passenger demands of approximately 500 and 1000 active HSCTs were created. The emission inventories developed from these schedules can then be used to evaluate how parametric changes in fleet size affect the HSCT impact on the stratospheric ozone layer.

Fuel consumption and emissions of nitrogen oxides (NOx), carbon monoxide (CO), and hydrocarbons (HC) were calculated for all flight segments and are reported on a three-dimensional grid with a resolution of 1 degree latitude x 1 degree longitude x 1 km altitude. Given the fuel burned in each grid cell, emissions of water vapor, carbon dioxide, and sulfur dioxide can be determined from the fuel properties. The following scenarios were calculated:

- Projected 2015 HSCT traffic for 500 and 1000 Mach 2.4 HSCTs with nominal NO_X emission indices of 5 and 15 gm NO_X/kg fuel burned at cruise.
- Projected 2015 HSCT traffic for Mach 2.0 HSCTs with nominal NO_X emission indices of 5 and 15 gm NO_X/kg fuel burned at cruise (passenger demand corresponding to 500 and 1000 Mach 2.4 HSCTs).
- Projected 2015 scheduled subsonic aircraft (assuming no HSCT fleet exists).
- Projected 2015 scheduled subsonic aircraft (assuming an HSCT fleet with passenger demand corresponding to 500 Mach 2.4 HSCTs was flying).
- Projected 2015 scheduled subsonic aircraft (assuming an HSCT fleet with passenger demand corresponding to 1000 Mach 2.4 HSCTs was flying).

The fuel burned and emission characteristics of the HSCT and future subsonic aircraft were based on estimated performance. The HSCT performance and emissions were the best estimate available at the beginning of this study and were "frozen" in order to develop new emission scenarios in time for the 1995 AESA assessment. Since then, preliminary design work has continued on both the airframe and the engine. The final design of the HSCT will likely have some characteristics different from those assumed for this study; hopefully, it will be more fuel efficient. The HSCT emission projections are based on the HSRP program goal and the estimates of the engine companies and are treated parametrically in this study and in the AESA assessment. As combustor rig test data becomes available, it will be possible to better refine these projections.

The details of the emission calculation process are described in NASA CR-4592 (Baughcum, et. al., 1994) and will only be summarized in this report. The results obtained in this study are compared with the emission scenarios calculated for the 1993 AESA assessment (Baughcum, et. al., 1994). The effects of fleet growth on the geographical distribution of HSCT emissions are analyzed and discussed.

During this work, we discovered several errors made in our previous study and present the corrected data in this report. For the HSCT, it was found that the operating empty weight used in the emission scenario calculation had been incorrectly entered into the analysis data file and was not consistent with the performance data for the baseline model used in the study. This was corrected and revised emission inventories for Mach 2.0 and Mach 2.4 HSCTs on the 1993 AESA assessment network were calculated, delivered to NASA Langley, and described in this report. In addition, the fuel performance improvement factor for the very large aircraft (P900) projected for 2015 was incorrectly implemented. This was corrected and revised 2015 subsonic aircraft emission scenarios are described in this report.

The work on HSCT and Year 2015 emission scenarios described in this report was conducted under NASA Langley Contract NAS1-19360, Task 40. The NASA Langley Task Manager was Donald L. Maiden.

Within the Boeing HSCT engineering group, overall program management was provided by Thomas Derbyshire, John D. Vachal, and John H. Gerstle. The principal investigator of the task was Steven L. Baughcum. Chief contributors were Stephen C. Henderson, Terry Higman, Thomas T. Odell, and Richard Bateman in market analysis; Peter S. Hertel in computer support; and Debra R. Maggiora in data analysis.

2.0 New Expanded HSCT Network

2.1 Total Passenger Demand Forecast for 2015

The total passenger demand forecast for the year 2015 was created by escalating 1991 reported regional flow passenger demand data using the annual growth rates developed by Boeing and published in the 1993 Current Market Outlook (Boeing, 1993). This yearly publication shows the Boeing Commercial Airplane Group's traffic and airplane demand forecasts. The results of this forecast, including regional flow growth rates and passenger demand (revenue passenger miles or RPMs), are summarized in Table 2-1 below. A more detailed table of the passenger demand for each of the forecast regions is shown on Appendix A, with the interim years of 1995, 2000, 2005 and 2010 also shown, along with the interim year-to-year growth rates.

Table 2-1. World Traffic Forecast

	Average Annual		ual
Regional Flow	1991 RPMs	Growth Rate 1991-	2015 RPMs
	(millions)	2015	(millions)
Intra & Domestic N. America	358,741	4.01%	921,565
N. America-Europe	121,400	4.78%	372,129
N. America-Asia/Pacific	87,065	7.03%	445,013
Other N. America	3,565	4.08%	9,306
N. America-Latin America	36,476	5.20%	123,092
Intra & Domestic Europe	148,216	4.62%	437,999
Europe-Asia/Pacific	46,430	8.05%	297,690
Europe-Indian Sub Continent	9,718	3.54%	22,376
Europe-Mid East	19,578	5.07%	64,163
Europe-Africa	25,811	4.48%	73,850
Europe-Latin America	26,869	5.34%	93,627
Intra & Domestic Asia/Pacific	86,003	7.92%	535,482
Misc. Long Range	40,348	5.70%	152,698
Japan	33,773	4.16%	89,918
Intra & Dom Indian Sub Continent	6,779	5.81%	26,316
Other Indian Subcontinent	14,261	4.75%	43,461
Intra & Domestic Mid East/Africa	18,455	5.01%	59,695
Other African	8,002	5.38%	28,163
Intra & Domestic Latin America	27,023	5.26%	92,463
CIS International	13,842	3.70%	33,098
MAC Charter	5,657	-2.36%	3,191
Total	1,138,012	5.29%	3,925,296

2.2 HSCT Universal Route System

The "Universal" HSCT route system is meant to simulate the operation of HSCTs as a mature fleet in a global airline network. The "Universal" system can be considered the sum of several global airlines, although it it scheduled as if it is a single airline. This approach can be justified by making the assumption that in the future, airline alliances and code-sharing will be more extensive than today (particularly among international airlines).

A "Universal" HSCT route system was originally developed as part of the 1993 AESA HSCT assessment (Baughcum, et. al., 1994). The route system used in this study is based on the original system, but has been enlarged and refined to add many more city-pairs and to provide more efficient land-avoiding flight tracks. Gateway cities were established in the countries of each of the regions included in the regional traffic flow forecasts and assumed to be the focus of HSCT flights in year 2015. Thus HSCT flights from Britain are assumed to operate from London, flights from France operate from Paris, etc. Some countries were given more than one gateway city, due to the size of the market and/or the size of the country. (For example, the United States has 18 gateways, Japan 2 gateways, Australia and Germany 3 gateways each)

A list of the assumed gateway cities for HSCT operations is shown in Appendix B.

The total year 2015 world passenger demand (measured as passengers) was distributed among the gateway city-pairs in each region by using the share of the total passenger available seat miles (ASM) that each city pair included in the regional flows generated in 1993 (as derived from the Official Airline Guide schedules). For each city-pair in each region, total passenger demand in 2015 was forecast as follows:

Passenger Demand CITY-PAIR, 2015 =

(RPM REGIONAL FLOW, 2015 x (ASM_{CITY-PAIR}/ASM_{REGION})₁₉₉₃)/Distance CITY-PAIR

2.3 HSCT Passenger Traffic Demand - Market Penetration

Due to the operating characteristics of the HSCT (sonic boom restrictions and high operating costs, particularly on short routes), only a certain subset of the total regional passenger demands are candidates for HSCT service. (U.S. Domestic, Intra Europe, and the domestic demand of other regions are excluded, for example). The suitability of the HSCT for the remaining passenger demand must be determined according to some logical assessment criteria.

In the previous 1993 AESA HSCT emission database study (Baughcum, et. al., 1994), routes for HSCT service were selected according to a set of "static" criteria mutually agreed upon between Boeing and McDonnell Douglas. Routes were selected using the following ground rules:

- No supersonic flight over land
- Flight distance must be greater than 2000 nautical miles
- No more than 50% over land routing
- No more than 20% diversion from great circle routing
- Passenger demand must be sufficient to support at least one flight/day at 70% load factor

Once the routes that satisfied these criteria were selected, equal market penetration of the HSCT was assumed on all markets. The penetration level was adjusted to produce the 500 Mach 2.4 airplane fleet size used in that study.

One of the goals of the current fleet growth study is to determine how an increasing fleet of HSCT's would change the global distribution of emissions. Therefore, this study does <u>not</u> use a "static" set of criteria for determining the proportion of city-pair demand likely to be captured by the HSCT. Instead, demand captured by the HSCT is assumed to depend <u>only</u> on travel time saved and the fare differential over a subsonic airplane serving the same city-pair. (The travel time saved is in turn determined by the routing required to minimize flight over land, see Section 2.4.) HSCT demand capture in this study was determined by a proprietary market penetration model developed within Boeing. The proportion of each city-pair market captured by the HSCT was found by:

$P = f(R, T, F, Z, L_{min})$

where

P = percent of total passenger demand carried by the HSCT,

R =range of the HSCT,

T = Trip time saved versus a subsonic airplane,

F = Fare premium over the subsonic airplane,

Z = stop factor (whether the HSCT flight is non-stop or not), and

 L_{min} = the minimum load factor allowed on a flight.

The only explicit constraint operating in the penetration model is the prohibition of supersonic flight over land.

As the amount of time saved increased or the fare premium decreased, or the number of stops decreased, the proportion of the passenger demand carried by the HSCT increased. If the application of the penetration model lowered the HSCT passenger demand on a city-pair to less than 180 passengers per day, that city-pair was dropped from the HSCT system. The fare premium parameter (*F*) of the model was first adjusted so that the passenger demand carried by the HSCT in 2015 required approximately 500 Mach 2.4 airplanes, forming the baseline case for the calculation of HSCT emissions distribution. The fare premium parameter was then reduced so that the increased passenger demand required approximately 1000 Mach 2.4 airplanes, creating the alternate case. The average load factor was 65%.

The higher demand carried by the 1000 airplane fleet came from both an increased penetration on the same markets served by the 500 airplane fleet and an increase in the number of city-pairs served. The city-pairs, number of departures and other system data are listed in Appendix C for the 500 and 1000 unit HSCT fleets. The route system maps for fleets of 500 and 1000 HSCTs are shown in Figures 2-1 and 2-2, respectively. The routes added as the fleet grew from 500 to 1000 are shown in Figure 2-3.

Emission inventories of HSCT airplanes designed with cruise speeds of Mach 2.0 using the same route systems defined by the Mach 2.4 airplanes were also calculated. Passenger demand levels and route systems which required nominally 500 (actually 499) and nominally 1000 (actually 991) Mach 2.4 airplanes required 528 and 1062 Mach 2.0 airplanes, respectively.

1994 EMISSIONS ROUTE SYSTEM 500 AIRPLANE HSCT FLEET

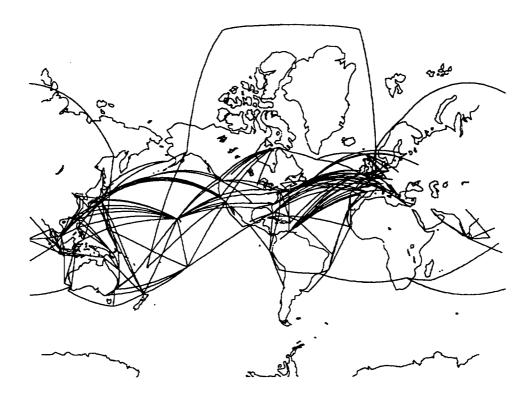


Figure 2-1. Universal Network Route System, 500 HSCT fleet

1994 EMISSIONS ROUTE SYSTEM 1000 AIRPLANE HSCT FLEET

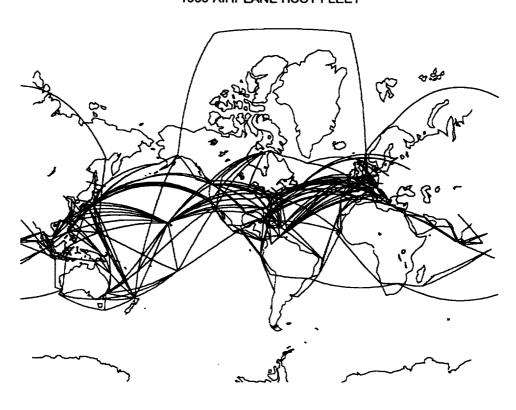


Figure 2-2. Universal Network Route System, 1000 HSCT fleet

1994 EMISSIONS ROUTE SYSTEM ROUTES ADDED BY INCREASING FLEET TO 1000



Figure 2-3. Universal Network Route System, New Routes added when increasing fleet to 1000 HSCTs.

2.4 HSCT Flight Paths - Waypoint Routing

As was noted previously, the amount of trip time saved by the HSCT versus a subsonic airplane serving the same city-pair is one of the determinants of HSCT market penetration. Since it is assumed that the HSCT must fly at subsonic speeds over land masses, each potential HSCT city-pair route was examined to find the reasonable routing which minimized (or at least reduced) the percentage of the flight spent over land. The flight routing was accomplished by establishing "waypoints", a set of specific latitude-longitude positions which defined the HSCT flight path. (The HSCT flight path between waypoints was flown as a great circle.)

As an example, consider HSCT flights from Frankfurt (FRA) to Bangkok (BKK) (See Figure 2-4). The shortest (great circle) flight path is 4841 nautical miles, all over land and therefore flown subsonically. The flight path between BKK and FRA can be altered by requiring the HSCT to fly between "waypoints". established at defined latitude-longitude positions designed to minimize the amount of overland flight. As shown in Figure 2-4, waypoints can be used to route the HSCT subsonically from Frankfurt to near Venice, then supersonically down the Adriatic, across the Mediterranean to the Sinai, subsonically across the Arabian peninsula, then supersonically again around India to Bangkok. This new path reduces the amount of flight overland to only 1993 nautical miles. but increases the total flight path to 6130 nautical miles, a distance greater than the 5000 nautical design range of the study airplane. Flying this path requires a stop at Bahrain (BAH) to refuel (and pick up passengers). After the Bahrain stop, the HSCT resumes the flight as defined above. The new path (with a stop) adds 28% to total miles flown, but reduces the subsonic flight portion of the path by 62%. (See Table 2-2)

Table 2-2. Example of waypoint routing - Frankfurt to Bangkok

Route Segment	Great Circle Distance (nmi)	Flight Path Distance (nmi)	Supersonic Distance (nmi)	Subsonic Distance (nmi)
Frankfurt - Bangkok (Great Circle Path)	4,841	4,841	0	4,841
Frankfurt - Bangkok (Direct, HSCT Waypoints)	4,841	6,130	4,137	1,993
Frankfurt - Bahrain - Bangkok (Stop at Bahrain, HSCT W	5,292 /aypoints)	6,181	4,319	1,862
Percent Change in Flight Path from direct Great Circle		28%		-62%

FRANKFURT - BANGKOK HSCT FLIGHT PATHS EXAMPLE OF WAYPOINT ROUTING

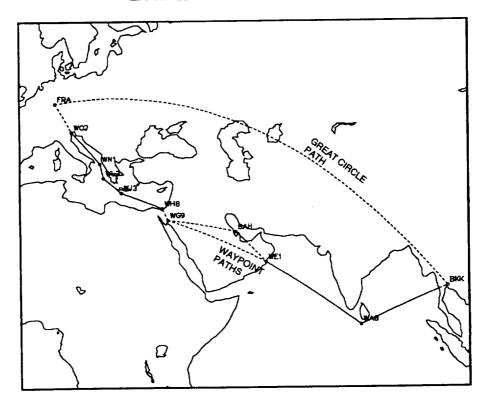


Figure 2-4. Example of Waypoint Routing

The above example shows a somewhat extreme change in flight path. Using the new waypoint routing and the market penetration model, the HSCT route system used in this study is very efficient - adding only about 5% to total route miles flown. 90% of HSCT trips are penalized less than 10% in flight path distance over the minimum Great Circle distance (Figure 2-5). 90% of HSCT trips also operate at 60% or less of subsonic block time (Block time is the total time for the flight including roll back, taxi-out, flying, and taxi-in. Subsonic block time is the block time that a subsonic aircraft would require.) Almost 60% of HSCT trips operate at less than half of subsonic block time (These statistics for for the 500 airplane fleet) (Figure 2-6). The 1000 airplane fleet, with its greater market penetration, includes more routes which are less desirable from an HSCT efficiency standpoint - lowering the overall waypoint routing efficiency and fleet time savings by a small amount. Waypoints and their positions for all HSCT routes flown are compiled as part of the flight path listing in Appendix D.

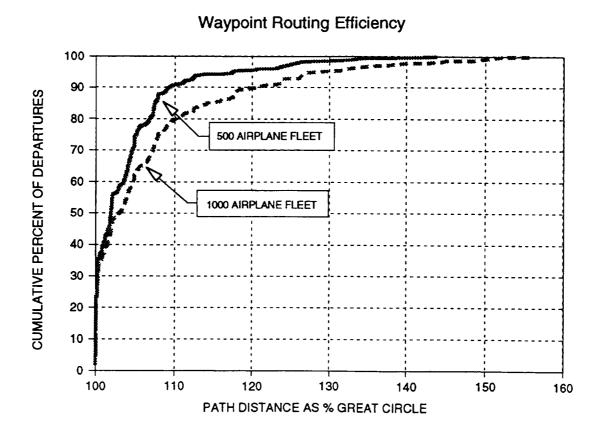


Figure 2-5 Waypoint Routing Efficiency

Trip Time Savings - HSCT Fleets

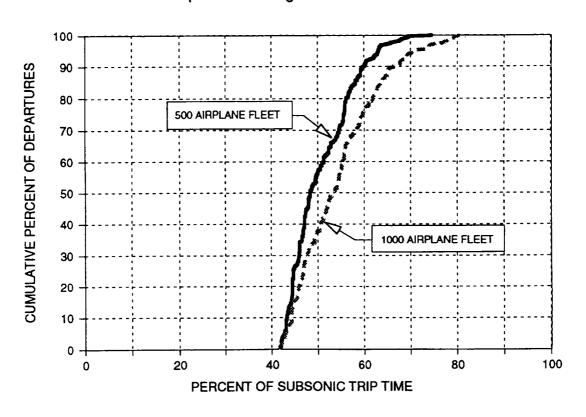


Figure 2-6 Trip Time Savings - HSCT Fleets

2.5 HSCT Scheduling

A description of the method of scheduling the HSCT fleet is provided in Appendix E. The resulting utilization statistics are summarized below. The nonlinear nature of both the penetration model and the scheduling model made it difficult to exactly achieve the goal of 500 and 1000 airplane HSCT fleets. The fleet size was adjusted by varying the fare premium in the penetration model so that the nominal "500" unit Mach 2.4 fleet was actually 499 units and the nominal "1000" unit fleet was actually 991 units. These were felt to be close enough to the target fleet sizes for these parametric studies and additional iterations were not performed.

Table 2-3. Utilization statistics for the universal airline HSCT network.

	Mach 2.4		Mach 2.0	
Units	499	991	528	106
Average Stage Length - n.m.	3555	3026	3555	302
Average Daily Use (hours)	21.95	22.24	21.87	22.1
Average Hours/Segment	3.67	3.30	4.07	3.6
Average Hours/Trip	4.26	3.78	4.71	4.1
Average Block Hours/Day	16.00	16.10	16.75	16.4
Percent of Subsonic Trip Time	49.97	53.25	55.21	58.2
Network Flight Path % of GCD	103.98	106.16	103.98	106.1
% of Trip in Supersonic Cruise	75.16	71.18	78.66	74.9
% of Trip in Subsonic Cruise	12.52	15.46	12.54	15.4
Percent Nonstop Trips	87.88	89.39	87.88	89.3
Average Trip Load Factor	65.16	65.09	65.16	65.0
Annual RPMs (Billion)	551	1,043	551	1,04
Annual ASMs (Billion)	846	1,602	846	1,60
Annual Departures	793,510	1,765,140	793,510	1,765,140
Annual RAMs (GCD - Million)	2,713	5,031	2,713	5,03
Annual RAMs (Path - Million)	2,821	5,341	2,821	5,34

Because of its speed, the HSCT has the ability to serve a large set of cities and still remain within the preference/curfew time "windows", which are always defined in local time.

2.6 2015 Subsonic Traffic

Subsonic air traffic for the year 2015 was projected using the passenger demand forecasts used in NASA Contractor Report 4592 (Baughcum, et. al., 1994). Displacement of subsonic traffic by the HSCT passenger demand was included as described in the earlier study.

3.0 Emissions Calculation Procedure

3.1 Overview of Emissions Calculation

The primary emissions from aircraft engines are water vapor (H₂O) and carbon dioxide (CO₂) produced by the combustion of jet fuel. Nitrogen oxides (NO_X), carbon monoxide (CO) and hydrocarbons are also produced in the combustors and vary in quantity according to the temperature, pressure, and other combustor conditions. Nitrogen oxides consist of both nitric oxide (NO) and nitrogen dioxides (NO₂). Sulfur dioxide (SO₂) may also be produced due to sulfur impurities in jet fuel. Soot is also produced, particularly at high power settings, but its characterization is beyond the scope of the current work.

Emission indices of water, carbon monoxide, and sulfur dioxide are determined by the jet fuel properties. These were discussed in our previous contractor report (Baughcum, et. al., 1994) and are summarized below.

Table 3-1. Recommended emission indices in units of grams emission/kilogram fuel for 1990 and 2015.

	Emission Index	
Emission	1990	2015
Carbon Dioxide (CO ₂)	3155	3155
Water (H ₂ O)	1237	1237
Sulfur dioxide (SO ₂)	0.8	0.4

The emission levels from aircraft engines are discussed by Miake-Lye (Miake-Lye, et. al., 1992). The emissions are characterized in terms of an emission index in units of grams of emission per kilogram of fuel burned. For NOx, the emission index [EI(NOx)] is given as gram equivalent NO2 to avoid ambiguity. Although hydrocarbon measurements of aircraft emissions by species have been made (Spicer, et. al., 1992), only total hydrocarbon emissions are considered in this work, with the hydrocarbon emission index [EI(HC)] given as equivalent methane (CH4).

Nitrogen oxides are produced in the high temperature regions of the combustor primarily through the thermal dissociation of oxygen followed by oxygen atom reactions with molecular nitrogen. Thus, the NOx produced by an aircraft engine is sensitive to the length of the combustor, the pressure, and the temperature within the combustor. The emissions vary with the power setting of the engine (highest at high thrust conditions). By contrast, carbon monoxide and hydrocarbon emissions are highest at low power settings when the temperature of the engine is low and incomplete combustion occurs.

Once a schedule of city-pairs and departures was determined, the next step in the development of the scenario data set was to use aircraft/engine performance and emissions data to calculate the fuel use and emissions as a function of altitude and location. For each mission, fuel consumption and emissions are calculated including all the flight segments (taxi-out, takeoff, climb, cruise, descent, landing, taxi-in), distributing the emissions in space along the route between city-pairs. The emissions were then combined for all flights into the resulting three-dimensional database.

3.2 HSCT Description

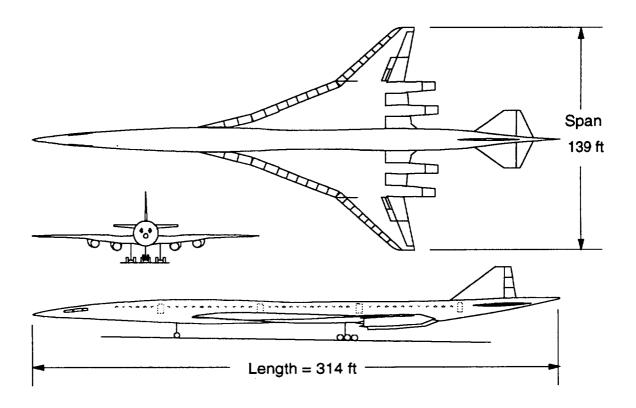
The Mach 2.4 HSCT scenarios were calculated using the Boeing preliminary design model 1080-924 with four Pratt & Whitney STJ989 turbine bypass engines (TBE) with mixed compression translating center body (MCTCB2) inlets and two-dimensional semi-stowable (SS2D) nozzles. The aircraft has a cranked-arrow wing planform (see Figure 3-1) and a mostly composite structure. Overall body length is approximately 314 feet with a wing span of 139 feet. It was designed to carry 309 passengers for a range of 5000 nautical miles.

The Mach 2.0 HSCT scenarios were developed based on the preliminary design model 1080-938 with four P&W STJ1016 turbine bypass engines with MCTCB2 inlets and SS2D nozzles. The characteristics of both these aircraft are summarized in Table 3-2.

Table 3-2. Summary of HSCT aircraft characteristics used in the development of the Mach 2.0 and Mach 2.4 HSCT emission scenarios.

	Mach 2.4	Mach 2.0
Model Number	1080-924	1080-938
Engine	PW STJ989	PW STJ1016
Range (nautical miles)	5000	5000
Passengers	309	309
Design Payload (lbs)	64,890	64,890
Max. Takeoff Weight (lbs)	784,608	802,872
Wing Span (ft)	139	140
Wing Area (sq. ft.)	8180	8260

Model 1080-924



Configuration Description:

Maximum takeoff weight

Wing Area Engine

Payload

Range

784,600 pounds 8,180 square feet

STJ989

309 passengers, tri-class

5,000 nmi - supersonic cruise

Figure 3-1. HSCT General Characteristics

The performance and emission characteristics for both Mach 2.0 and 2.4 were the same as those used as in the previous NASA contract work. (Baughcum, et. al., 1994) However, it was found that the operating empty weights used in the previous emission scenario calculations had been incorrectly entered into the analysis data file and were not consistent with the performance data for the baseline model used in the study. This was corrected and revised emission inventories for Mach 2.0 and Mach 2.4 HSCTs on the 1993 AESA assessment network were calculated and delivered to NASA Langley. In this report, these revised 1993 AESA assessment scenarios are summarized and compared to the present universal airline results.

Emissions data for NOx, CO, and hydrocarbons were provided by GE/P&W for a generic HSCT combustor with a nominal NO $_{\rm X}$ emission index at supersonic cruise of approximately 5 gm NO $_{\rm X}$ (as NO $_{\rm 2}$)/kg fuel. Nitrogen oxides, carbon monoxide, and hydrocarbon emission levels were calculated from these data as a function of power setting and altitude. A similar calculation was completed to scale to a nominal cruise EI (NO $_{\rm X}$)=15 scenario. For this scaling, the combustor was assumed to operate as a conventional combustor at low power settings and as an advanced low-NO $_{\rm X}$ combustor at higher settings. Based on discussions with both engine companies, the EI(NO $_{\rm X}$) for this case was unchanged at low power settings and increased by a factor of 3 at higher thrust settings.

3.3 Mission Profiles

The mission profile procedures were described in detail in our previous NASA contractor report (Baughcum, *et. al.*, 1994). The basic HSCT mission profile was assumed as follows:

- 10 minute taxi-out
- all engine takeoff ground-roll and liftoff
- climbout to 1500 feet and accelerate
- climb to optimum cruise altitude (subsonic or supersonic, depending on whether over land or water)
- climbing supersonic cruise at constant Mach
- descent to 1500 feet
- approach and land
- 5 minute taxi-in

For a given HSCT model, fuel burned and emissions data were calculated for parametric mission cases: various takeoff weights (in increments of 50,000 pounds), two passenger-loading factors (100% and 65%), and with two cruise speeds (Mach 2.4 and Mach 0.9). These subsonic and supersonic mission profiles of varying range were used with a regression analysis to develop generalized performance for each HSCT mission segment as a function of weight. The details of this analysis were described in our previous NASA contractor report. (Baughcum, *et. al.*, 1994)

HSCT flight profiles of fuel burn and emissions were calculated from these performance and emissions data for each HSCT mission. These profiles combined with projected HSCT flight frequencies were then used to calculate the three-dimensional database, as described in our previous contractor report. (Baughcum, *et. al.*, 1994)

When calculating the flight profiles, all aircraft were assumed to fly according to design performance. For subsonic aircraft, cruise altitudes were calculated as a climbing cruise with the optimum altitude determined by the weight of the aircraft. For the HSCT, supersonic flight was allowed only over water and thus the mission profiles were more complicated than for subsonic aircraft.

Design optimum flight profiles between city-pairs were used to distribute emissions during takeoff, subsonic and supersonic climb and cruise, and descent. Based on these mission profiles, the calculated fuel burned and emissions were then transformed onto the database grid. Two missions, which are representative of the way in which an actual HSCT would be flown, are shown in Figures 3-2 and 3-3.

The simplest mission (Figure 3-2) is a flight almost exclusively over water, such as Seattle to Tokyo. The HSCT would take off and climb subsonically and then supersonically to a supersonic cruise altitude. It would then fly at supersonic cruise at the optimum altitude determined by its gross weight. As it approached Tokyo, it would descend and land. The cumulative fraction of the total NO_X emissions is plotted on the right axis. The plot illustrates that approximately 40% of the NO_X emissions would occur during takeoff, subsonic climb, and supersonic climb prior to supersonic cruise.

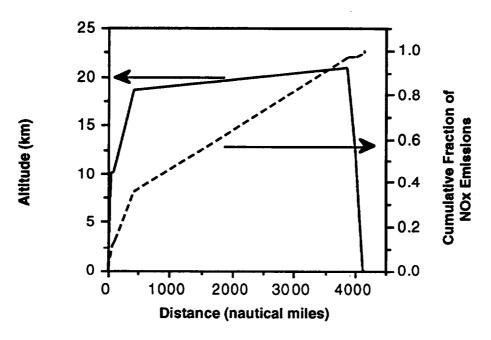


Figure 3-2. Mission profile for Mach 2.4 HSCT from Seattle to Tokyo.

A more complicated but still common mission is a flight in which one leg would be flown subsonically over land. This is illustrated in Figure 3-3 for a flight from Seattle to London. The HSCT would take off and climb to subsonic cruise altitudes. It would then cruise at subsonic speeds until it reached Hudson Bay where it would begin to climb supersonically. The HSCT would then cruise at supersonic speeds (altitude determined by the optimum performance) until descending near London. An even larger fraction (approximately 60%) of the NO_X emissions would occur during the subsonic climb, subsonic cruise, and supersonic climb prior to supersonic cruise.

A still more complicated mission, which was included in the calculations but not shown graphically, is a flight in which the aircraft might descend and climb several times to avoid flying supersonically over land. An example would be the Frankfurt to Bangkok route. In this case, the HSCT would fly subsonically over Europe, supersonically over the Mediterranean, subsonically over Arabia (stopping in Bahrain) supersonically over the Indian Ocean, and then subsonically inland over the Malay peninsula. Because of the high fuel consumption of supersonic climbs, such flight profiles were kept to a minimum in the scenario development.

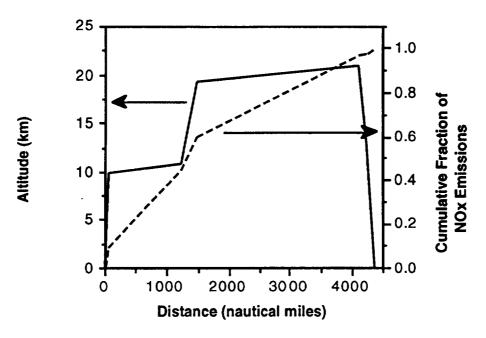


Figure 3-3. Mission profile for Mach 2.4 HSCT from Seattle to London.

3.4 Emission Calculation Procedures

All aircraft were assumed to fly according to design optimum performance. Altitudes and mission profiles were calculated based on the performance of the aircraft for its mission weight. Air traffic control constraints on routings were not considered. For each aircraft type considered, a separate three-dimensional data set of fuel burned and emissions was calculated. Subsonic aircraft were flown along great circle routes between cities. For the HSCT, routing between waypoints to avoid supersonic flight over land was used for many of the citypairs. The HSCT was flown along great circle routes between these waypoints. For all flights, prevailing winds were not considered, based on the assumption that wind effects would largely be canceled out for round trips.

To calculate the global inventory of aircraft emissions, a computer model was developed which basically combines scheduling data (city pairs, departures, aircraft type) with aircraft performance and emissions data. The Global Atmospheric Emissions Code (GAEC) computer model was used to calculate fuel burned and emissions from files of airplane performance and engine emissions data. The aircraft performance file contains detailed performance input data for a wide range of operating conditions. Each engine emission input file contains emission indices tabulated as a function of the fuel flow rate. The GAEC model was described in more detail in the earlier report (Baughcum, et. al., 1994).

For each route flown by the airplane/engine type, the takeoff gross weight required was calculated as a function of the city-pair route distance. The fuel burned was calculated for the following flight segments:

- Taxi-out
- Takeoff
- Climbout
- Subsonic Climb
- Subsonic Cruise
- Supersonic Climbout
- Supersonic Cruise
- Supersonic Descent
- Descent
- Approach and Land
- Taxi-in

For year 2015 subsonic aircraft, emissions of nitrogen oxides (NOx), hydrocarbons (HC) and carbon monoxide (CO) were projected from the ground level emission indices reported to the International Civil Aviation Organization (ICAO) for current aircraft. These measurements are reported at four thrust settings. The Boeing fuel flow correlation methodology was used to calculate emission indices for different flight phases, corrected for ambient temperature, pressure, and humidity. (Baughcum, et. al., 1994; R. L. Martin, C. A. Oncina, and J. Zeeben, private communication). This methodology will be described in more detail in a future NASA contractor report describing the development of subsonic aircraft emission inventories for each month of 1992. (S. L. Baughcum, T. G. Tritz, and S. C. Henderson, private communication)

Subsonic aircraft emission inventories were calculated using the same technology improvements as reported in NASA CR-4592 (Baughcum, et. al., 1994) except that a small error for the largest airplane type (P900) was discovered. The technology improvement factor for fuel flow given in Table 6-4 of NASA CR-4592 for the P900 aircraft had not been correctly used in the previous calculation. This was corrected so that the calculations are now consistent with the improvement factors shown in NASA CR-4592. As described later in this report, this makes only an approximately 2% change in the fuel use projected for the 2015 all subsonic fleet. Emission inventories for scheduled subsonic air traffic were calculated for the cases of fleets of 0, approximately 500, and approximately 1000 HSCTs on the universal airline network. Displacement of subsonic air traffic by HSCTs on individual routes was explicitly taken into account. The results are described in Sections 4 and 5 of this report.

Distributions of fuel usage and emissions were calculated for 1° latitude x 1° longitude x 1 km altitude cells. The altitudes used are pressure altitudes, not geometrical altitudes. The altitude corresponds to the geopotential altitudes of the U.S. Standard Atmosphere temperature and pressure profile and is thus pressure-gridded data. (U. S. Standard Atmosphere, 1976) Commercial aircraft measure their altitudes using pressure altimeters. For each city-pair, the total

route distance was calculated. The fuel burn rate and airplane gross weight were then calculated at discrete distances along the route path which corresponded to points where the airplane entered or left a cell (crossed any of the cells boundaries) or points where a transition in flight conditions occurred (climbout/climb, climb/cruise, cruise/descent, descent/approach and land, taxiout/climbout, approach and land/taxi-in). The fuel burn rate would change dramatically at these transition points.

The emissions were calculated for each flight segment between the above described discrete points using the fuel burn rate within the segment. The total fuel burned in the segment was calculated as the difference in airplane gross weight at the segment end-points. The emissions were then assigned to a cell based on the coordinates of the endpoints.

4.0 Emission Inventory Results

A summary of the network statistics is shown in Table 4-1. An increase in the size of the HSCT fleet results in a greater number of city pairs included in the network. To satisfy the same passenger demand, a Mach 2.0 HSCT fleet requires about 6% more aircraft than needed for Mach 2.4 and flies at supersonic cruise about 4000 feet lower.

Doubling the size of the fleet results in an approximate doubling of the number of departures and an approximate doubling in the global fuel burn for the fleet. Comparison of the departure frequencies shown in Appendix C indicates that doubling the fleet size increases the flight frequencies on some routes but not on others, since it is sensitive to the market penetration analyses. Thus, changes in the geographical distribution of emissions may occur upon fleet growth. This will be discussed in more depth in Section 5.

The minimum altitudes shown in Table 4-1 correspond to the lowest altitudes at which supersonic cruise is reached. Because the Mach 2.4 HSCT must climb to higher altitudes which takes both time and distance, the Mach 2.0 is able to supersonically cruise on some segments for which the Mach 2.4 aircraft cannot.

Table 4-1. Summary of departure statistics for HSCT networks.

	1993 AESA Assessment Network (revised)	New Universal Network "500"	New Universal Network "1000"
Mach 2.4	4		
Number of Aircraft	500	499	991
Number of city pairs	193	243	392
Total daily departures	2,192	2,174	4,836
Total distance (miles/day)	7,458,802	7,728,939	14,632,996
Total Fuel (million lbs/day)	493.03	509.46	961.33
Maximum flight altitude (feet)	67,904	67,854	67,865
Minimum cruise altitude (feet)	57,722	57,547	57,547
Mach 2.0	_		
Number of Aircraft	532	528	1062
Number of city pairs	193	243	392
Total daily departures	2,192	2,174	4,836
Total distance (miles/day)	7,458,802	7,728,939	14,632,996
Total Fuel (million lbs/day)	504.79	524.27	979.92
Maximum flight altitude (feet)	63,956	63,907	63,920
Minimum cruise altitude (feet)	52,881	53,674	53,674

The fuel use and emissions for the different scenarios considered are summarized in Table 4-2 below. As shown below, the change from the simple ground rules to the market-driven universal airline network has only a small effect on the global fuel usage and NOx emissions for a fleet of 500 HSCTs. The biggest changes occurred in the geographical distribution of the emissions.

Table 4-2. Summary of fuel use and emissions for the different scenarios.

Mach	EI(NOx)	Number		Fuel	NOx	НС	CO
Number		of HSCTs	Network	(kg/yr)	(kg/yr)	(kg/yr)	(kg/yr)
Mach 2.4	fleet						
2.4	5	500	1993 AESA	8.16E+10	5.37E+08	2.99E+07	2.42E+08
2.4	5	499	universal	8.21E+10	5.35E+08	2.97E+07	2.41E+08
2.4	5	991	universal	1.57E+11	1.04E+09	5.88E+07	4.76E+08
2.4	15	500	1993 AESA	8.16E+10	1.46E+09	2.99E+07	2.42E+08
2.4	15	499	universal	8.21E+10	1.48E+09	2.97E+07	2.41E+08
2.4	15	991	universal	1.57E+11	2.82E+09	5.88E+07	4.76E+08
Mach 2.0	Fleet						
2.0	5	532	1993 AESA	8.36E+10	5.02E+08	2.89E+07	2.45E+08
2.0	5	528	universal	8.45E+10	5.04E+08	2.90E+07	2.47E+08
2.0	5	1062	universal	1.60E+11	9.65E+08	5.66E+07	4.78E+08
2.0	15	532	1993 AESA	8.36E+10	1.47E+09	2.89E+07	2.45E+08
2.0	15	528	universal	8.45E+10	1.48E+09	2.90E+07	2.47E+08
2.0	15	1062	universal	1.60E+11	2.82E+09	5.66E+07	4.78E+08
2015 Sche	eduled Subs	sonic Air T	raffic				
Subsonic pa	ssenger aircr	aft (no HSCT t	fleet)	2.50E+11	2.32E+09	9.93E+07	1.11E+09
	ssenger aircra			2.22E+11	2.05E+09	9.34E+07	1.05E+09
			M2.4 HSCTs)	1.97E+11	1.75E+09	1.95E+08	1.32E+09
2015 Cargo		•	•	5.64E+09	4.91E+07	3.56E+06	2.77E+07

The fuel burned and emissions for the network used in the 1993 AESA assessment (Baughcum, et. al., 1994) differ somewhat from those reported earlier. An error in the weight of the aircraft used in the performance calculations was discovered upon later analysis. Using the corrected weights, the emission inventories for the 1993 AESA assessment network were rerun. The total fleet fuel burn for the 500 aircraft fleet increased by about 7% from that reported earlier (Baughcum, et. al., 1994) for the Mach 2.4 HSCT fleet. In addition, with the correct (heavier) weight, the supersonic cruise altitudes were slightly lower than those used in the earlier study. In the earlier report

(Baughcum, et. al., 1994), the Mach 2.4 HSCT cruise altitudes were in the range of 59,639-69,098 feet. The corrections in the aircraft weight result in cruise altitudes about 1100 feet lower for the new scenarios. Similar problems were discovered and corrected for the Mach 2.0 emission inventories.

In this section, the results for the individual component inventories will be presented and discussed. In the next section, the overall results and changes between the different scenarios will be analyzed.

4.1 Mach 2.4 HSCT Fleet Results

Details of the results of HSCT fleet operations for different flight segments for the Mach 2.4 HSCT fleets are summarized in Tables 4-3 and 4-4. Table 4-5 shows the revised results for the 1993 AESA study. For all cases considered, the majority of the miles flown, fuel used and NOx emissions occur during supersonic cruise, where the actual EI at cruise is 5.42 (close to the nominal value of 5). The nominal EI=15 case was calculated by scaling the EI(NOx) at cruise by a factor of 3 as described in CR 4592 (Baughcum, et. al., 1994). The calculated EI(NOx) at cruise for the nominal EI=15 case is 16.4 (see Appendix F).

The calculated fuel burned, emissions, and effective emission indices as a function of altitude (summed over latitude and longitude) for the Mach 2.4 HSCTs (both EI(NOx)=5 and 15) are tabulated in Appendix F. Also included in Appendix F are the revised results for the 1993 AESA assessment network.

Table 4-3. Daily mileage, fuel consumption, NOx emissions, and NOx emission index for the Mach 2.4 HSCT, nominal EI=5 flight segments. (Universal Network, 500 HSCTs)

		Daily	Daily Fuel	Daily NOx	
Flight Segment		Mileage (nmi)	(1000 lbs)	(1000 lbs)	EI(NOx)
Taxi out		0	6,376	42	6.56
Initial Climb		96,929	40,780	353	8.65
Supersonic Climb		688,696	91,822	795	8.65
Supersonic Cruise		5,808,829	318,909	1,728	5.42
Supersonic Descent		264,008	1,714	11	6.56
Subsonic Cruise		555,250	34,864	289	8.30
Final Descent		315,230	12,559	82	6.56
Taxi in		0	2,435	16	6.56
1	Total	7,728,942	509,460	3,316	6.51

Table 4-4. Daily mileage, fuel consumption, NOx emissions, and NOx emission index for the Mach 2.4 HSCT, nominal EI=5 flight segments. (Universal Network, 1000 HSCTs)

Flight Segment		Daily Mileage	Daily Fuel (1000 lbs)	Daily NOx (1000 lbs)	EI(NOx)
Tilgik Geginerik		wineage	(1000 ibs)	(1000 lb3)	LI(I4OX)
Taxi out		0	14,184	93	6.56
Initial Climb		208,556	85,784	742	8.65
Supersonic Climb		1,369,248	180,857	1,565	8.65
Supersonic Cruise		10,415,248	561,414	3,041	5.42
Supersonic Descent		585,600	3,802	25	6.56
Subsonic Cruise		1,353,126	81,939	680	8.30
Final Descent		701,220	27,938	183	6.56
Taxi in		0	5,416	36	6.56
	Total	14,632,998	961,333	6,365	6.62

Table 4-5. Daily mileage, fuel consumption, NOx emissions, and NOx emission index for the Mach 2.4 HSCT, nominal El=5 flight segments. (1993 AESA assessment network(revised), 500 HSCTs)

	D-11.	Daily	Daily	
Flight Segment	Daily Mileage	Fuel (1000 lbs)	NOx (1000 lbs)	EI(NOx)
Taxi out	0	6,429	42	6.56
Initial Climb	96,929	40,599	351	8.65
Supersonic Climb	666,449	88,815	769	8.65
Supersonic Cruise	5,380,866	295,890	1,603	5.42
Supersonic Descent	256,932	1,668	11	6.56
Supersonic Cruise & Descent	22,686	2,218	19	8.65
Subsonic Cruise	717,101	42,289	351	8.30
Final Descent	317,840	12,663	83	6.56
Taxi in	0	2,455	1 6	6.56
Total	7,458,803	493,027	3,245	6.58

The three-dimensional character of the emission inventories is illustrated in Figure 4-1, which shows the daily NOx emissions from a fleet of 500 Mach 2.4 (EI(NOx)=5) HSCTs on the universal airline network. The top panel shows NOx emissions as a function of altitude and latitude (summed over longitude). This represents the input to a 2-dimensional (altitude and latitude) stratospheric chemistry model, such as those used in the AESA assessment. Peak emissions occur at supersonic cruise at northern mid-latitudes. The bottom panel illustrates the route segments occurring at altitudes above 13 kilometers, which correspond to supersonic climb and cruise.

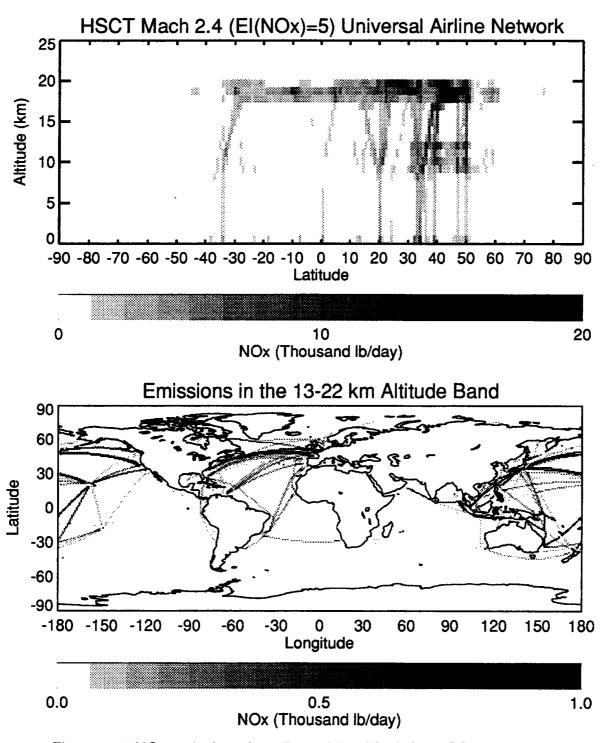


Figure 4-1. NOx emissions for a fleet of 500 Mach 2.4 HSCTs on the Universal Airline Network, as a function of altitude and latitude (summed over longitude, top panel) and as a function of latitude and longitude (summed over the 13-22 km altitude band, bottom panel). (Values greater than maximum are plotted as black.)

The fuel burned and emissions (NOx, hydrocarbons, and CO) as a function of altitude are shown in Figure 4-2 for fleets of 500 and 1000 Mach 2.4 HSCTs (EI(NOx)=5) on the present universal airline network. Not surprisingly, the larger fleet has approximately twice as much emissions and shows the same altitude distribution as the 500 HSCT fleet. Figure 4-3 shows the cumulative fraction of fuel burn and emissions plotted as a function of altitude for the two fleet sizes. The additional shorter routes for the 1000 HSCT fleet results in a larger fraction of the fuel burn and emissions occurring at lower altitudes for takeoff, climbout, and supersonic climb. Although the majority of the fuel use and NOx emissions will occur in the 18-21 kilometer altitude band, a significant fraction of the emissions occurs below 10 kilometers and between 10 and 18 kilometers.

The emission indices as a function of altitude are shown in Figure 4-4. The variation in emissions as a function of altitude reflect the changes in fuel burn rate at different stages of the flights and changes in power setting (with resulting changes in emission indices). Changes in HSCT fleet size have relatively little impact on the emission indices averaged over all missions.

The geographical distribution of the emissions for the universal airline network is displayed in Figure 4-5 for fleets of 500 and 1000 Mach 2.4 HSCTs. For these plots, the emissions for the entire fleet have been been summed over longitude and then plotted as a function of latitude. The plots show that most of the HSCT flights will occur at northern midlatitudes. Figure 4-6 shows the cumulative fraction as a function of latitude for each of the emissions, summing over the entire altitude range (0-22 km). For both fleet sizes, approximately 20% of the emissions occur in the Southern hemisphere, but the majority occur north of 30° North latitude.

The emissions injected above 13 kilometers in altitude, which will have the greatest impact on the stratospheric ozone layer, are shown in Figure 4-7 as a function of latitude for fleets of 500 and 1000 Mach 2.4 HSCTs. Figure 4-8 shows the cumulative fraction as a function of latitude for each of the emissions, summing over the 13 to 22 kilometer altitude band. Approximately 60% of the stratospheric NOx from the HSCT fleets will be injected north of 30° North latitude.

Growth of the fleet to 1000 active HSCTs causes only small changes in the geographical distribution. A more detailed discussion of the changes in emissions as the fleet grows from 500 to 1000 HSCTs will be presented in Section 5.

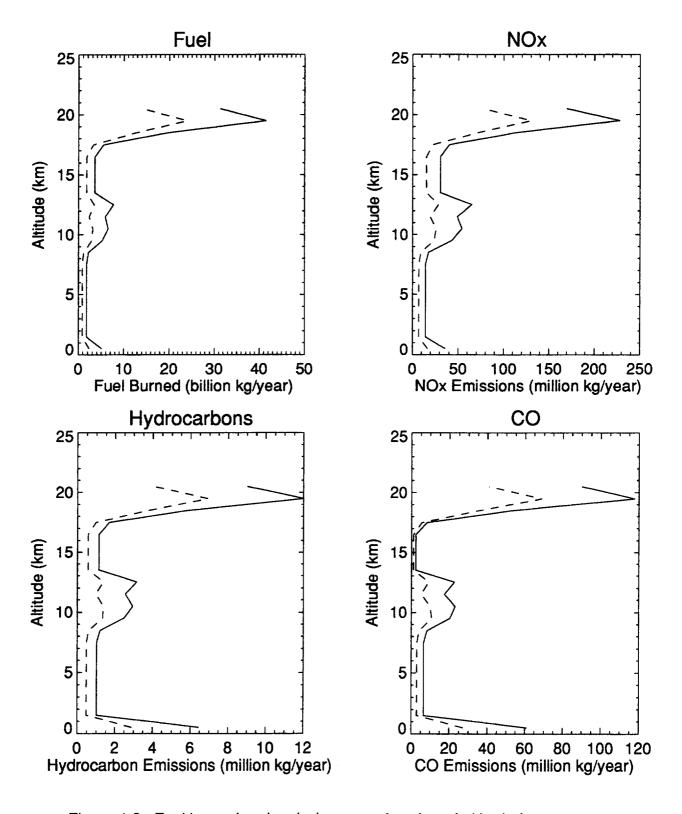


Figure 4-2. Fuel burned and emissions as a function of altitude for the universal airline HSCT network for a fleet of 500 (dashed line) and 1000 (solid line) Mach 2.4 HSCTs with EI(NOx) of approximately 5 at supersonic cruise (summed over latitude and longitude).

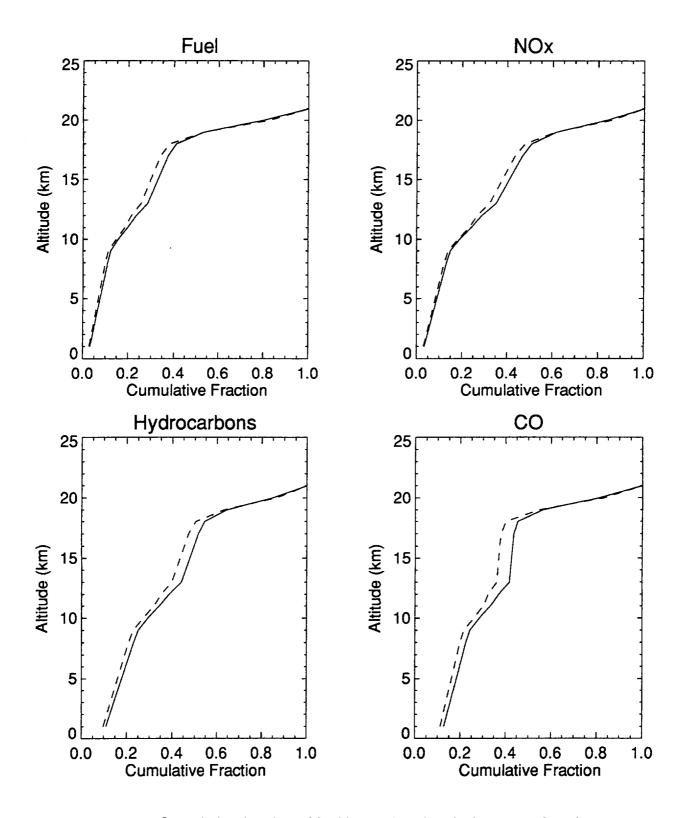


Figure 4-3. Cumulative fraction of fuel burned and emissions as a function of altitude for the universal airline HSCT network for a fleet of 500 (dashed line) and 1000 (solid line) Mach 2.4 HSCTs with EI(NOx) of approximately 5 at supersonic cruise (summed over latitude and longitude).

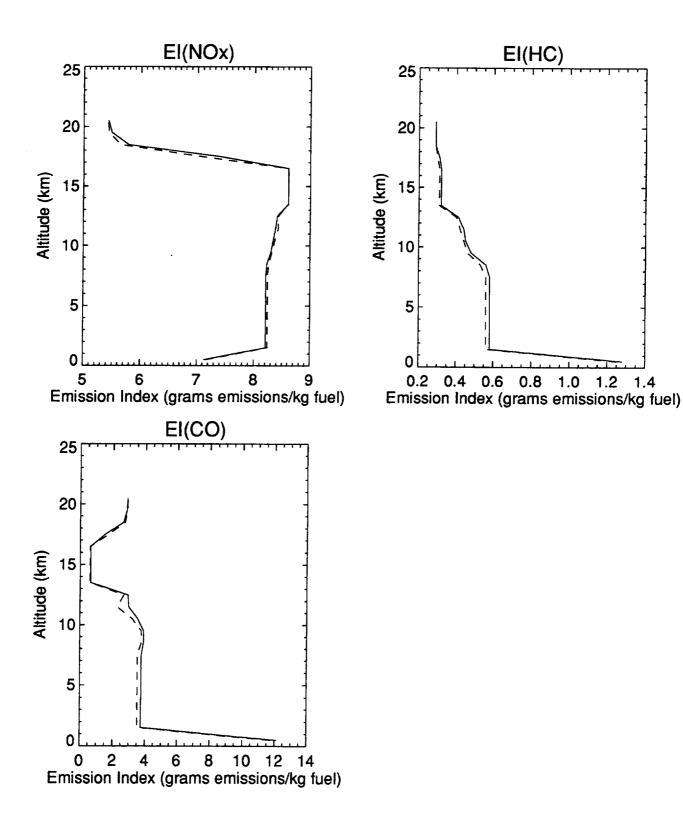


Figure 4-4. Emission indices as a function of altitude for the universal HSCT network for a fleet of 500 (dashed line) and 1000 (solid line) Mach 2.4 HSCTs with EI(NOx) of approximately 5 at supersonic cruise (summed over latitude and longitude).

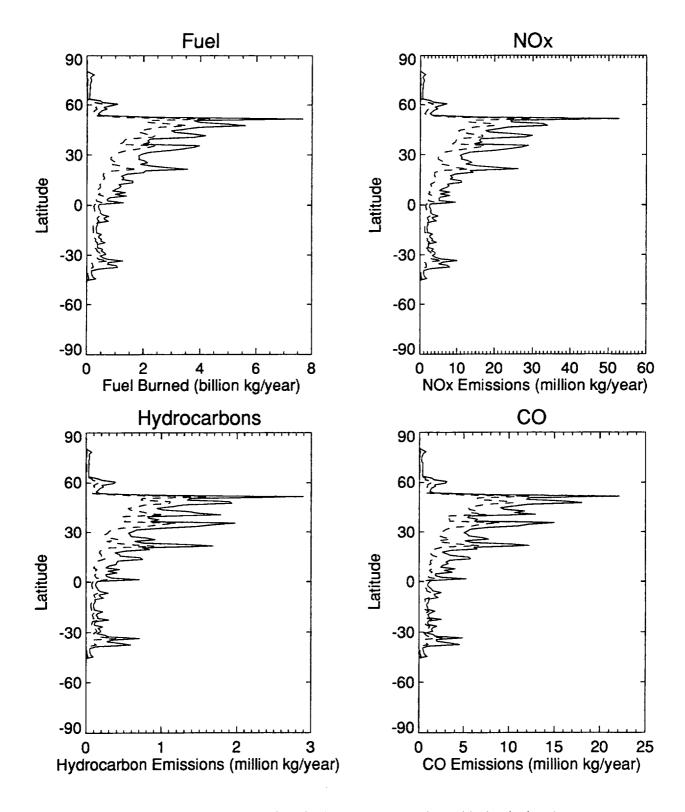


Figure 4-5. Fuel burned and emissions as a function of latitude for the universal airline HSCT network for fleets of 500 (dashed line) and 1000 (solid line) Mach 2.4 HSCTs with an EI(NOx) of approximately 5 at supersonic cruise (summed over altitude and longitude).

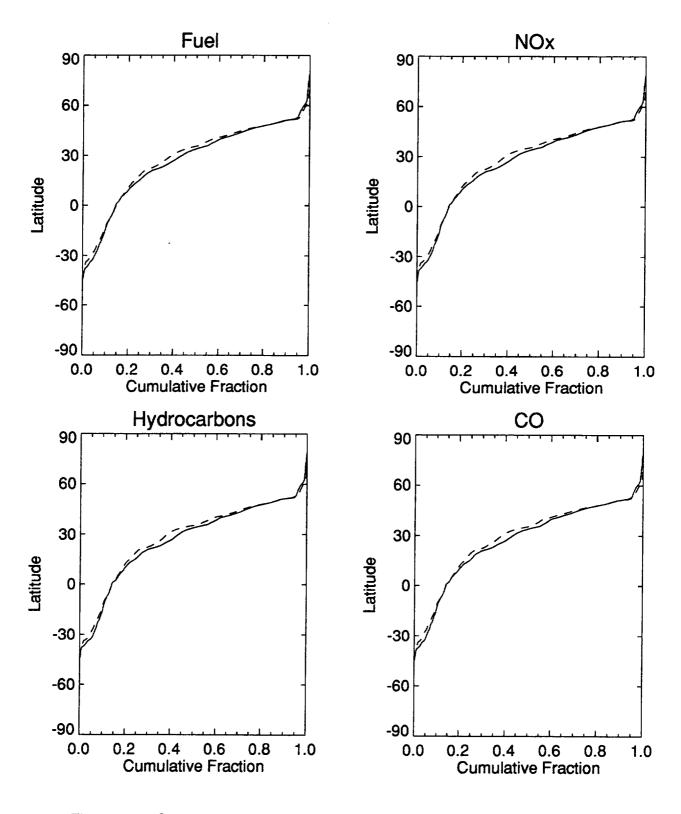


Figure 4-6. Cumulative fraction of fuel burned and emissions as a function of latitude for the universal airline HSCT network for fleets of 500 (dashed line) and 1000 (solid line) Mach 2.4 HSCTs with an EI(NOx) of approximately 5 at supersonic cruise (summed over altitude and longitude).

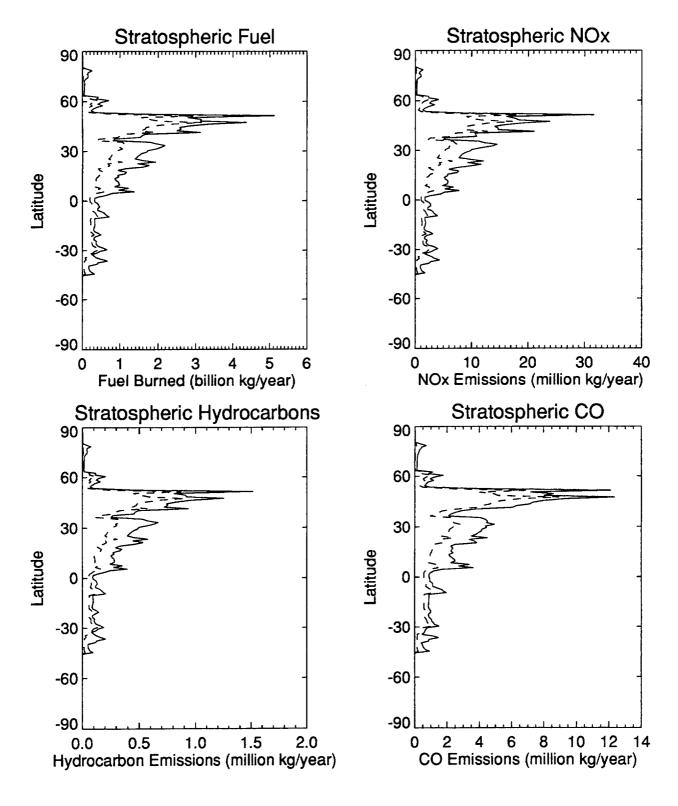


Figure 4-7. Fuel burned and emissions above 13 kilometers altitude as a function of latitude for the universal airline HSCT network for fleets of 500 (dashed line) and 1000 (solid line) Mach 2.4 HSCTs with an EI(NOx) of approximately 5 at supersonic cruise (summed over altitude and longitude).

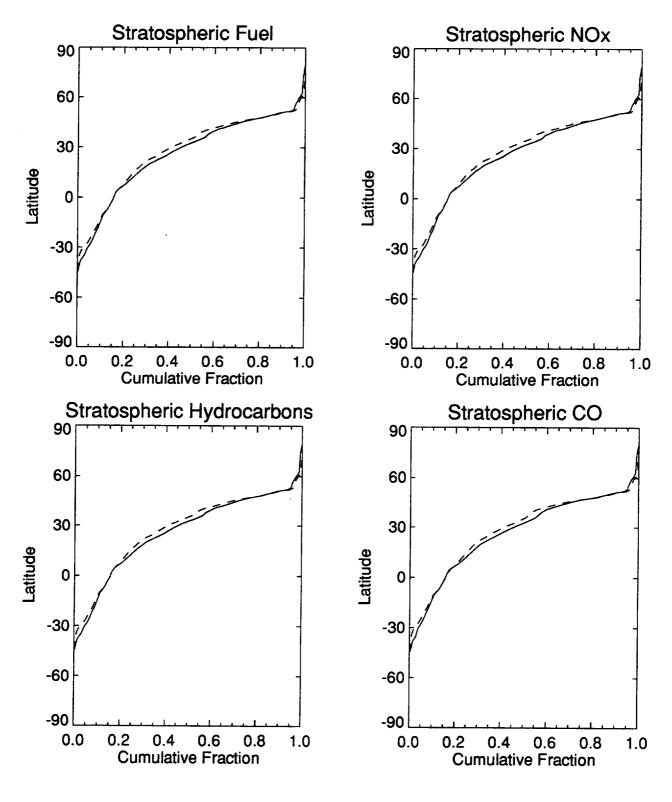


Figure 4-8. Cumulative fraction of fuel burned and emissions above 13 kilometers altitude as a function of latitude for the universal airline HSCT network for fleets of 500 (dashed line) and 1000 (solid line) Mach 2.4 HSCTs with an EI(NOx) of approximately 5 at supersonic cruise (summed over altitude and longitude).

4.2 Mach 2.0 HSCT fleet Results

Details of the results for different flight segments for the Mach 2.0 HSCT fleets are summarized in Tables 4-6 and 4-7. Table 4-8 shows the revised results for the 1993 AESA study. For all cases considered, the majority of the miles flown, fuel used and NOx emissions occur during supersonic cruise, where the calculated EI is 5.24.

The calculated fuel burned, emissions, and effective emission indices as a function of altitude (summed over latitude and longitude) for the M2.0 HSCTs (both EI(NOx)=5 and 15) are tabulated in Appendix G. Also included in Appendix G are the revised results for the 1993 AESA assessment network for Mach 2.0 HSCTs.

Since the same passenger demand was used for the Mach 2.0 fleet as was used for the Mach 2.4 fleet, the geographical distribution of emissions for the Mach 2.0 case is the same as for Mach 2.4. The altitude distributions are similar except that the supersonic cruise emissions occur approximately 4000 feet lower.

Table 4-6. Daily mileage, fuel consumption, NOx emissions, and NOx emission index for the Mach 2.0 HSCT, nominal El=5 flight segments. (Universal Network, passenger demand corresponding to 500 Mach 2.4 HSCTs)

		Daily	Daily Fuel	Daily NOx	
Flight Segment		Mileage (nmi)	(1000 lbs)	(1000 lbs)	EI(NOx)
Taxi out		0	5,752	40	7.00
Initial Climb		87,860	36,689	297	8.10
Supersonic Climb		482,933	66,765	541	8.10
Supersonic Cruise		6,079,332	367,116	1,925	5.24
Supersonic Descent		197,106	1,375	10	6.99
Subsonic Cruise		562,131	32,536	214	6.57
Final Descent		319,578	11,818	83	6.99
Taxi in		0	2,222	16	6.99
-	Total	7,728,940	524,273	3,125	5.96

Table 4-7. Daily mileage, fuel consumption, NOx emissions, and NOx emission index for the Mach 2.0 HSCT, nominal El=5 flight segments. (Universal Network, passenger demand corresponding to 1000 Mach 2.4 HSCTs)

Flight Segment	Daily Mileage (nmi)	Daily Fuel (1000 lbs)	Daily NOx (1000 lbs)	EI(NOx)
Taxi out	0	12,796	90	7.00
Initial Climb	188,134	76,870	623	8.10
Supersonic Climb	965,212	131,653	1,067	8.10
Supersonic Cruise	10,963,144	648,318	3,400	5.24
Supersonic Descent	437,346	3,052	21	6.99
Subsonic Cruise	1,368,262	76,000	499	6.57
Final Descent	710,892	26,288	184	6.99
Taxi in	0	4,942	35	6.99
To	tal 14,632,990	979,919	5,918	6.04

Table 4-8. Daily mileage, fuel consumption, NOx emissions, and NOx emission index for the Mach 2.0 HSCT, nominal El=5 flight segments. (1993 AESA assessment network (revised), passenger demand corresponding to 500 Mach 2.4 HSCTs)

	Daily	Daily Fuel	Daily NOx	
Flight Segment	Mileage (nmi)	(1000 lbs)	(1000 lbs)	EI(NOx)
Taxi out	0	5,800	4 1	7.00
Initial Climb	87,777	36,453	295	8.10
Supersonic Climb	472,821	65,351	529	8.10
Supersonic Cruise	5,649,821	341,743	1,792	5.24
Supersonic Descent	194,285	1,356	9	6.99
Supersonic Cruise & Descent	11,777	1,146	9	8.10
Subsonic Cruise	720,099	38,788	255	6.57
Final Descent	322,224	11,916	83	6.99
Taxi in	0	2,240	16	6.99
Total	7,458,804	504,792	3,030	6.00

Since the Mach 2.0 and Mach 2.4 HSCT fleets are flown on the same passenger demand network in this study, the primary difference between the two fleets is that the Mach 2.0 fleet requires about 6% more aircraft to satisfy the same passenger demand and the aircraft cruise supersonically about 4000 feet

lower. Tables of the emissions as a function of altitude for Mach 2.0 are included as Appendix G.

4.3 Year 2015 Subsonic Fleet Results

For year 2015 subsonic passenger aircraft, 10 jet categories and one generic turboprop were considered. These are summarized in Table 4-9. These are the same categories as used in our previous study (Baughcum, *et. al.*, 1994). Aircraft performance and emissions characteristics were the same as used in the previous study except that an error in the performance data used for the P900 aircraft type (> 900 passengers) was corrected, as described in Section 3. This increased the total projected fuel burn for the all subsonic 2015 scheduled passenger fleet by about 2%.

Results are presented here for the subsonic passenger fleet in use for the cases where there are 0, 500, and 1000 Mach 2.4 HSCTs in use on the universal network. Subsonic cargo aircraft data was not updated from that presented earlier (Baughcum, et. al., 1994) but is included in the summaries.

Table 4-9. Classes of "Generic" Subsonic Passenger Aircraft Used in the 2015 Scenario Construction

Class	Seating Capacity	Average Seats
TBP (turboprop)	0 - 49	30
P060	50 - 69	60
P080	70 - 109	85
P120	110 - 139	120
P180	140 - 199	170
P250	200 - 299	250
P350	300 - 399	350
P500	400 - 599	500
P700	600 - 799	700
P900	> 800	900

The results for the three subsonic passenger fleets are summarized by aircraft type in Tables 4-10, 4-11, and 4-12. Fuel use by subsonic passenger jets was projected to drop by approximately 11% because of the displacement caused by 500 HSCTs in operation and 21% in the presence of 1000 HSCTs. As discussed in Section 5, total fuel usage for the combined fleet of subsonic and HSCT fleets would increase as HSCTs displace subsonic aircraft.

The calculated fuel burn, emissions, and effective emission indices as a function of altitude (summed over latitude and longitude) for the year 2015 subsonic passenger fleets are tabulated in Appendix G.

Table 4-10 Globally Computed Fuel Burned, Emissions, and Emission Indices by Aircraft Type for 2015 Scheduled Subsonic Airliners if 500 Mach 2.4 HSCTs are in operation on the universal network.

					Globally Averaged Emission Indices		
	Fuei	NO_{x}	HC	CO	EI	EI	ΕI
File	(kg/yr)	(kg/yr)	(kg/yr)	(kg/yr)	(NO_x)	(HC)	(CO)
P060	2.63E+09	1.49E+07	1.47E+06	1.44E+07	5.66	0.56	5.50
P080	8.67E+09	6.84E+07	2.91E+06	6.59E+07	7.88	0.34	7.60
P120	1.42E+10	1.04E+08	8.02E+06	1.25E+08	7.37	0.57	8.85
P180	2.34E+10	1.73E+08	5.80E+06	1.23E+08	7.39	0.25	5.26
P250A	2.49E+10	2.15E+08	1.64E+07	1.63E+08	8.64	0.66	6.56
P250B	1.65E+10	1.21E+08	1.16E+07	6.23E+07	7.33	0.70	3.77
P350	4.09E+10	4.29E+08	1.48E+07	1.56E+08	10.50	0.36	3.82
P500	5.07E+10	4.74E+08	1.80E+07	2.15E+08	9.33	0.35	4.25
P700	2.24E+10	2.61E+08	4.18E+06	5.46E+07	11.66	0.19	2.44
P900	1.37E+10	1.45E+08	3.02E+06	4.22E+07	10.59	0.22	3.07
TBP	4.13E+09	4.40E+07	7.29E+06	2.41E+07	10.65	1.76	5.83
Total	2.22E+11	2.05E+09	9.34E+07	1.05E+09	9.23	0.42	4.71

Table 4-11 Globally computed fuel burned, emissions, and emission Indices by Aircraft Type for 2015 Scheduled Subsonic Airliners if 1000 Mach 2.4 HSCTs are in operation on the universal network.

					Globally Averaged Emission Indices		
	Fuel	NO_{x}	HC	CO	EI	EI	ΕI
File	(kg/yr)	(kg/yr)	(kg/yr)	(kg/yr)	(NO_x)	(HC)	(CO)
P060	2.63E+09	1.49E+07	1.47E+06	1.44E+07	5.66	0.56	5.50
P080	8.67E+09	6.84E+07	2.91E+06	6.59E+07	7.88	0.34	7.60
P120	1.41E+10	1.04E+08	8.01E+06	1.25E+08	7.37	0.57	8.86
P180	2.34E+10	1.73E+08	5.81E+06	1.23E+08	7.39	0.25	5.26
P250A	2.46E+10	2.13E+08	1.63E+07	1.62E+08	8.65	0.66	6.58
P250B	1.31E+10	9.59E+07	9.54E+06	5.11E+07	7.32	0.73	3.90
P350	3.65E+10	3.85E+08	1.38E+07	1.45E+08	10.56	0.38	3.97
P500	4.79E+10	4.49E+08	1.69E+07	2.02E+08	9.36	0.35	4.22
P700	1.64E+10	1.95E+08	3.61E+06	4.60E+07	11.92	0.22	2.80
P900	5.41E+09	6.10E+07	1.42E+06	1.91E+07	11.28	0.26	3.53
TBP	4.13E+09	4.40E+07	7.29E+06	2.41E+07	10.65	1.76	5.83
Total	1.97E+11	1.80E+09	8.71E+07	9.78E+08	9.16	0.44	4.97

Table 4-12 Globally Computed Fuel Burned, Emissions, and Emission Indices by Aircraft Type for 2015 Scheduled Subsonic Airliners if no HSCT Fleet Exists (revised from NASA CR 4592)

					Globally Averaged Emission Indices		
	Fuel	NO_x	HC	CO	Εi	El	ΕI
File	(kg/yr)	(kg/yr)	(kg/yr)	(kg/yr)	(NO_x)	(HC)	(CO)
P060	2.63E+09	1.49E+07	1.47E+06	1.44E+07	5.66	0.56	5.50
P080	8.67E+09	6.84E+07	2.91E+06	6.59E+07	7.88	0.34	7.60
P120	1.42E+10	1.04E+08	8.02E+06	1.25E+08	7.37	0.57	8.85
P180	2.35E+10	1.73E+08	5.81E+06	1.23E+08	7.39	0.25	5.25
P250A	2.49E+10	2.15E+08	1.64E+07	1.63E+08	8.64	0.66	6.56
P250B	2.10E+10	1.54E+08	1.39E+07	7.59E+07	7.33	0.66	3.61
P350	4.31E+10	4.51E+08	1.52E+07	1.61E+08	10.48	0.35	3.74
P500	5.25E+10	4.88E+08	1.86E+07	2.23E+08	9.31	0.35	4.26
P700	3.15E+10	3.61E+08	5.11E+06	6.84E+07	11.48	0.16	2.17
P900	2.40E+10	2.46E+08	4.63E+06	6.66E+07	10.22	0.19	2.77
TBP	4.13E+09	4.40E+07	7.29E+06	2.41E+07	10.65	1.76	5.83
Total	2.50E+11	2.32E+09	9.94E+07	1.11E+09	9.28	0.40	4.44

5.0 Analysis and Discussion

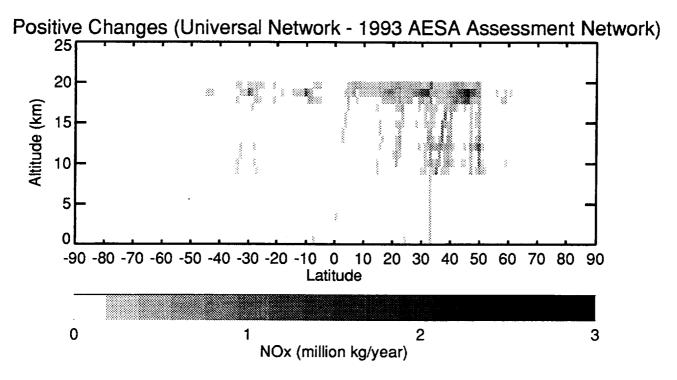
5.1 Comparison of HSCT Universal Fleet Emissions with Old Network Results

The weight corrections discussed earlier resulted in an increase in global fuel use of 7% by the HSCT fleet and cruise altitudes about 1100 feet lower than those described earlier ((Baughcum, et. al., 1994) and used in the 1993 AESA assessment. Changing from the 1993 AESA assessment network to the new universal airline network for the same number of active HSCTs in-service has little effect (less than 1%) on the global fuel burn or emissions for the HSCT fleet, when the correct OEW is used, as shown in Table 5-1.

Table 5-1. Comparison of the new universal network fuel use and emissions with the revised 1993 AESA assessment network results.

Mach 2.4 HSCT EI(NOx)=5	Fuel (kg/year)	NOx (kg/year)	HC (kg/year)	CO (kg/year)
1993 AESA assessment network (500 HSCTs) (Baughcum, et. al., 1994)	7.64E+10	5.00E+08	2.83E+07	2.33E+08
1993 AESA assessment network (500 HSCTs)(revised)	8.16E+10	5.37E+08	2.99E+07	2.42E+08
new universal network (500 HSCTs)	8.21E+10	5.35E+08	2.97E+07	2.41E+08
difference relative to the 1993 AESA network (revised)	5.02E+08	-2.63E+06	-2.09E+05	-1.15E+06
Percent change	0.61%	-0.49%	-0.70%	-0.47%

The change in ground rules has a much larger effect on the geographical distribution of the emissions. This is shown in Figure 5-1 where the 3-dimensional inventory of emissions calculated for the universal airline network is compared with the 1993 AESA assessment network (revised to account for the correct OEW). The top panel shows the increases in NOx emissions as a function of latitude and altitude when the universal airline network is compared with the 1993 AESA assessment network results (revised). The bottom panel shows the decreases in NOx emissions when the universal airline network is compared with the 1993 AESA assessment network results (revised). In general, the new universal airline network has the HSCT flying at subsonic cruise less than in the 1993 AESA assessment network. There are also fewer emissions at high northern latitudes and more in the Southern hemisphere for the new network.



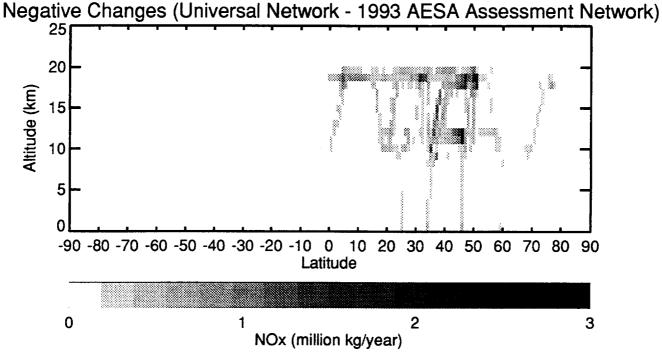


Figure 5-1. Comparison of NOx emissions from the universal airline network with the revised 1993 AESA assessment network for 500 Mach 2.4 [EI(NOx)=5] HSCTs. The top panel shows positive changes, while the bottom panel shows negative changes. (summed over longitude)

Since the changes in the high altitude emissions are expected to have the largest effects on ozone impact, the discussion will focus on changes in stratospheric NOx emissions. Figure 5-2 shows a comparison of the NOx emissions above 13 kilometers altitude for the 1993 AESA assessment network (revised) and the new 500 HSCT universal airline network. High altitude NOx emissions are greater in the southern hemisphere for each of the 10 degree latitude bands shown here. NOx emissions at extremely high northern latitudes (>70N) are less than with the old network. The analysis shows a net increase in the tropics of high altitude NOx emissions compared with the old network. At northern mid-latitudes the results are approximately the same.

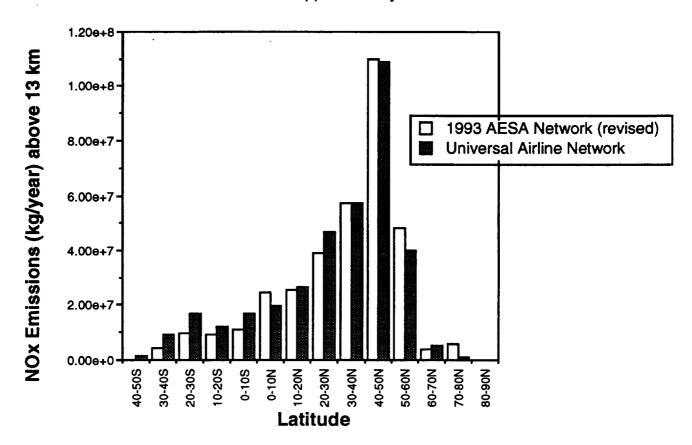


Figure 5-2. NOx emissions above 13 kilometers as a function of latitude, comparing the new universal airline scenario with the 1993 AESA assessment network scenario (revised) for 500 Mach 2.4 HSCTs.

Figure 5-3 shows the differences in fuel burned and NOx emissions at high resolution (1 degree latitude) as a function of latitude (summed over longitude). For these cases, the results are shown summed over all altitudes (the two top figures) and summed over altitudes above 13 km (bottom two figures). The high resolution plots illustrate that although there are systematic differences between the two networks in some latitude bands (e.g., the

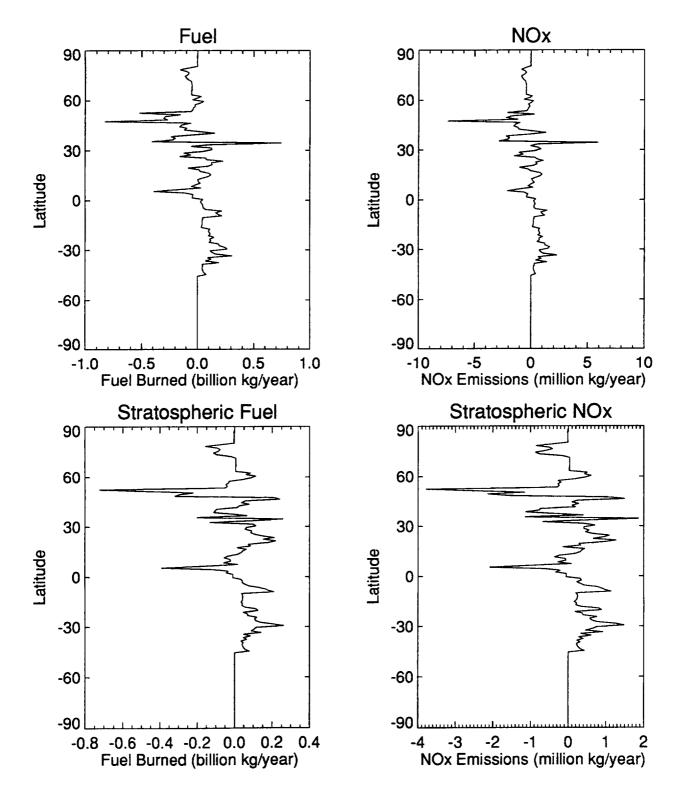


Figure 5-3. Differences in fuel burn and emissions between the new universal HSCT network and the 1993 AESA assessment network (revised) for a fleet of 500 Mach 2.4 HSCTs with EI(NOx) at cruise of approximately 5, plotted as a function of latitude. Stratospheric emissions here refer to emissions above 13 km.

Southern hemisphere), in other bands the differences are much more complicated (e.g., 30-40 North latitude).

Figure 5-4 shows the cumulative fraction of NOx emissions above 13 kilometers, emphasizing that in the new network about 15% of the stratospheric NOx emissions will occur in the southern hemisphere, compared to 10% for the old network. Most of the changes are an increase in stratospheric cruise occurring in the tropics. Since 2-D modeling calculations have indicated that HSCT emissions in the tropics may have greater impact on stratospheric ozone than for similar injections at mid-latitudes, these changes are worth noting for the AESA assessment calculations.

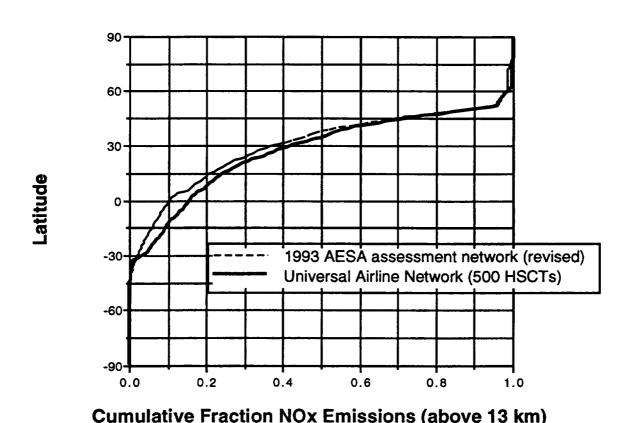


Figure 5-4. Cumulative fraction of NOx emissions above 13 km plotted as a function of latitude, comparing the results for the universal airline network with the revised 1993 AESA assessment network for the Mach 2.4 HSCT (EI(NOx)=5)).

5.2 Fleet Growth Effects

The effect of doubling the HSCT fleet from 500 to 1000 HSCTs on the universal airline network is summarized in Table 5-2. The global fuel use and emissions are projected to almost double with the fleet size.

Table 5-2. Comparison of the fuel use and emissions between the 500 and 1000 aircraft HSCT fleets.

Mach 2.4 HSCT EI(NOx)=5	Fuel (kg/year)	NOx (kg/year)	HC (kg/year)	CO (kg/year)
universal network (500 HSCTs)	8.21E+10	5.35E+08	2.97E+07	2.41E+08
universal network (1000 HSCTs)	1.57E+11	1.04E+09	5.88E+07	4.76E+08
difference (1000-2 x 500)	-7.52E+09	-3.11E+07	-5.25E+05	-7.09E+06
% difference (1000-2 x 500)	-4.58%	-2.91%	-0.88%	-1.47%

If we compare the NOx emissions injected at altitudes above 13 kilometers (Figure 5-5), it is clear that emissions in some latitude bands increase at different rates as the HSCT fleet is doubled.

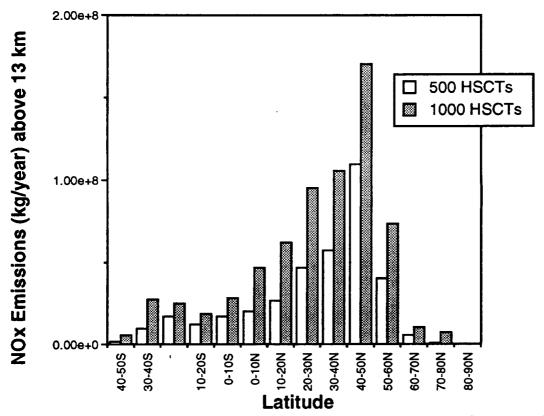


Figure 5-5. NOx emissions above 13 kilometers altitude as a function of latitude for 500 and 1000 Mach 2.4 HSCTs on the universal airline network.

To illustrate more clearly how the geographical distribution is modified as the fleet grows, Figure 5-6 shows the NOx emissions as a function of latitude for a fleet of 1000 Mach 2.4 HSCTs and compares them with the doubled emissions of the 500 HSCT fleet. In some regions (e.g., southern mid-latitudes, northern hemisphere tropics), the emissions have more than doubled compared with the 500 aircraft fleet; while in other regions (e.g., northern midlatitudes), the emissions have not grown linearly with the fleet size.

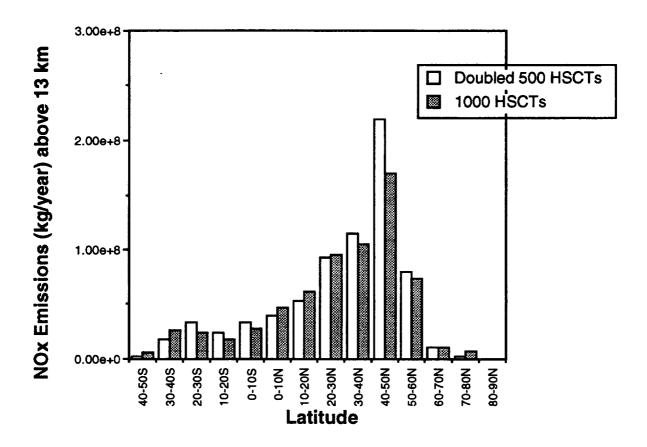


Figure 5-6. NOx emissions above 13 kilometers, comparing a fleet of 1000 HSCTs with doubling the results for a 500 HSCT fleet on the universal airline network.

Although the emission in all latitude bands do not exactly double when the fleet size doubles, the differences are relatively small in most regions. To first order, for 2-dimensional model calculations, treating the fleet size as a scalar appears to be justified. Subtle effects due to transport processes in the tropics or 3-dimensional effects will need to be evaluated for their sensitivity. The scenarios developed here should be useful for that purpose.

As shown, simply doubling the number of airplanes flown may not accurately reflect the distribution of emissions. A higher resolution comparison of the 1000 and doubled 500 HSCT fleet is shown in Figure 5-7. The top panel

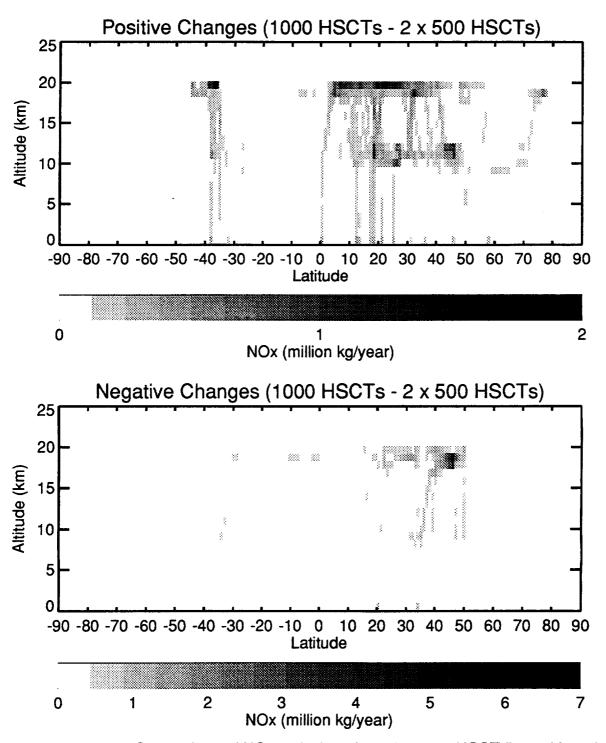


Figure 5-7. Comparison of NOx emissions from the 1000 HSCT fleet with emissions from doubling the 500 HSCT fleet on the universal airline network for Mach 2.4 [EI(NOx)=5] HSCTs. The top panel shows positive changes, while the bottom panel shows negative changes. (summed over longitude)

of Figure 5-7 shows the regions where the 1000 HSCT fleet has more than twice the emission levels of the 500 HSCT fleet. The bottom panel shows the locations where the emissions from the larger fleet are less than twice those of the smaller fleet. The bottom panel illustrates that flights in northern midlatitudes are projected to saturate and not increase linearly with fleet size. By contrast, emissions in the Southern hemisphere (particularly between 30-45° S latitude) and in the northern tropics (0-30° N latitude) are projected to increase faster than linear. In addition, emissions for the larger fleet at subsonic cruise altitudes would increase as new routes are added.

An increase of the fleet size from 500 to 1000 HSCTs would essentially double the total emissions from the HSCT fleet. However, as illustrated in Figure 5-7, the increase in fleet size shows growth in different geographical regions. As the fleet size increases, routes between new city pairs are introduced (see Appendix C).

Figure 5-8 shows the differences in fuel burned and NOx emissions as a function of latitude (summed over longitude) between the 1000 HSCT fleet and doubling the 500 HSCT fleet. The top two figures show the results considering all altitudes, while the bottom two figures consider only altitudes above 13 kilometers. For stratospheric NOx, emissions at southern mid-latitudes and the northern hemisphere tropics have grown faster than linear when the fleet increases from 500 to 1000 HSCTs, while northern mid-latitude emissions have increased at less than a linear rate.

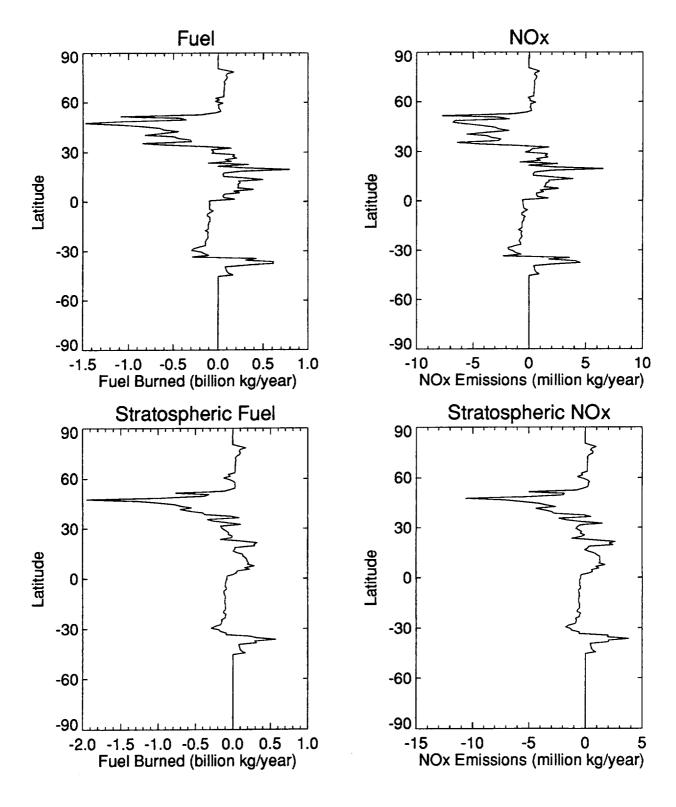


Figure 5-8. Differences in fuel burn and NOx emissions between 1000 HSCTs and simply doubling the 500 HSCT fleet, plotted as a function of latitude for the new universal HSCT network (Mach 2.4 HSCTs with EI(NOx) at cruise of approximately 5). Stratospheric emissions here refer to emissions above 13 km.

As shown in Figure 5-9, the relative partitioning of emissions between the northern and southern hemisphere is unchanged as the fleet doubles in size.

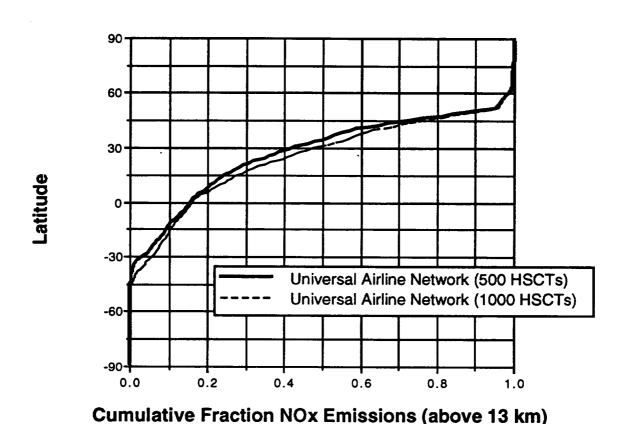


Figure 5-9. Cumulative fraction of stratospheric NOx emissions as a function of latitude for the 500 and 1000 HSCT fleets on the universal airline network.

5.3 Comparison of Fleet Growth Effects on 2015 Subsonic Emissions Inventory

The effect of a fleet of HSCTs on the subsonic fleet is summarized in Table 5-3. As discussed earlier, the corrections made to the P900 subsonic aircraft performance data files changed the global emissions by about 2%.

Not surprisingly, the fuel burn and emissions from the subsonic fleet decrease as more HSCTs are introduced into service. A fleet of HSCTs results in a drop of about 11% and 21% in total subsonic fleet fuel use for fleets of 500 and 1000 HSCTs, respectively, as HSCTs displace subsonic aircraft. The combined fuel use of subsonic and HSCT fleets will be discussed in Section 5.4.

Table 5-3. Comparison of the fuel use and emissions for the subsonic scheduled passenger fleets with and without the HSCT fleets

Year 2015 Subsonic Passenger fleet	Fuel (kg/year)	NOx (kg/year)	HC (kg/year)	CO (kg/year)
No HSCT fleet exists (Baughcum, et. al., 1994)	2.45E+11	2.24E+09	9.20E+07	1.09E+09
No HSCT fleet exists (revised)	2.50E+11	2.32E+09	9.94E+07	1.11E+09
In the presence of 500 M2.4 HSCTs (universal network)	2.22E+11	2.05E+09	9.34E+07	1.05E+09
In the presence of 1000 M2.4 HSCTs (universal network)	1.97E+11	1.80E+09	8.71E+07	9.78E+08

5.4 Total 2015 Scheduled Aircraft Emissions for Fleets of 0, 500, and 1000 HSCTs

The total global emissions for all projected scheduled air traffic scenarios for 2015 are summarized in Table 5-4. Since the HSCT uses more fuel on a per passenger mile basis than do subsonic aircraft, global jet fuel use is greater for the scenarios in which HSCTs are included in the projections. Fuel usage by scheduled passenger traffic in 2015 with a fleet of 500 HSCTs or 1000 HSCTs is projected to be 21% and 40% higher, respectively, compared to an all subsonic fleet.

These numbers shown in Table 5-4 include only air traffic due to scheduled subsonic passenger jets, cargo jets, turboprop aircraft, and HSCTs. They do not include charter traffic, military, or most of the projected air traffic in the former Soviet Union. As discussed in Chapter 2, the traffic forecasts for year 2015 are projected based on current air traffic schedules which do not include much of the internal air traffic within the former Soviet Union. Projections of charter, military, and former Soviet Union traffic have been done previously by McDonnell Douglas under contract to NASA. (Landau, et. al. 1994).

Comparisons of NOx emissions as a function of altitude for scheduled air traffic, with and without an HSCT fleet, were made in our previous work (Baughcum, et. al., 1994) and will not be repeated here. The data necessary for such calculations is included in Appendices F, G, and H of this report.

Table 5-4. Summary of fuel use, NOx, hydrocarbons, and carbon monoxide for the total scheduled air traffic scenarios for 2015.

	Fuel	NOx	HC	CO
	(kg/year)	(kg/year)	(kg/year)	(kg/year)
Total 2015 Scheduled Air Traffic without an HSCT fleet	2.56E+11	2.37E+09	1.03E+08	1.14E+09
Total 2015 Scheduled Air Traffic with a 500 Mach 2.4 HSCT fleet (EI(NOx)=5) (universal network)	3.10E+11	2.63E+09	1.27E+08	1.32E+09
Total 2015 Scheduled Air Traffic with a 500 Mach 2.4 HSCT fleet (EI(NOx)=15) (universal network)	3.10E+11	3.58E+09	1.27E+08	1.32E+09
Total 2015 Scheduled Air Traffic with a 1000 Mach 2.4 HSCT fleet (EI(NOx)=5) (universal network)	3.59E+11	2.89E+09	1.49E+08	1.48E+09
Total 2015 Scheduled Air Traffic with a 1000 Mach 2.4 HSCT fleet (EI(NOx)=15) (universal network)	3.59E+11	4.67E+09	1.49E+08	1.48E+09
Total 2015 Scheduled Air Traffic with a 500 Mach 2.0 HSCT fleet (EI(NOx)=5) (universal network)	3.12E+11	2.60E+09	1.26E+08	1.32E+09
Total 2015 Scheduled Air Traffic with a 500 Mach 2.0 HSCT fleet (EI(NOx)=15) (universal network)	3.12E+11	3.57E+09	1.26E+08	1.32E+09
Total 2015 Scheduled Air Traffic with a 1000 Mach 2.0 HSCT fleet (EI(NOx)=5) (universal network)	3.62E+11	2.82E+09	1.47E+08	1.48E+09
Total 2015 Scheduled Air Traffic with a 1000 Mach 2.0 HSCT fleet (EI(NOx)=15) (universal network)	3.62E+11	4.67E+09	1.47E+08	1.48E+09

Note: NOx is given as gram equivalent NO2

An evaluation of the effects of aircraft on the upper troposphere is one aspect of the NASA Atmospheric Effects of Aviation Project (AEAP). Based on these scenarios, the introduction of a fleet of Mach 2.4 (EI(NOx)=5) HSCTs would, change the NOx emissions due to aircraft at altitudes below 13 kilometers from 2.37 x 10^{10} kilograms/year to 2.27 x 10^{10} kilograms/year (-4%) for 500 HSCTs or to 2.15 x 10^{10} kilograms/year (-9%) for 1000 HSCTs. It is clear that the emissions of NOx above 13 kilometers (into the stratosphere) would be much higher with an HSCT fleet than without. As shown in Figure 5-10, the introduction of a fleet of HSCTs would be expected to decrease the NOx emissions in the upper troposphere.

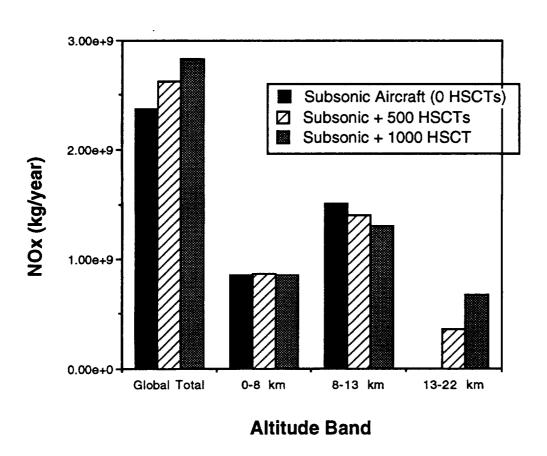


Figure 5-10. Total projected NOx emissions from 2015 scheduled air traffic for different altitude bands for fleets of 0, 500, and 1000 Mach 2.4 HSCTs with EI(NOx) at supersonic cruise of approximately 5.

5.5 Conclusions

A detailed database of projected 2015 subsonic and HSCT (both Mach 2.0 and 2.4) operational scenarios was developed using a universal airline network with HSCT fleet sizes of 0, 500, and 1000 active HSCTs. Three-dimensional data files of fuel burned and emissions (NOx, hydrocarbons, and carbon monoxide) on a 1° latitude x 1° longitude x 1 km altitude grid were calculated and delivered electronically to the Upper Atmospheric Data Program (UADP) system at the NASA Langley Research Center.

The work presented here shows that although the total global fuel burned and emissions from a fleet of 500 HSCTs is not very sensitive to whether the universal airline or the 1993 AESA assessment network is used, the geographical distribution of emissions at stratospheric cruise is sensitive to the market penetration assumptions used to distribute projected HSCT passenger demand.

An increase in HSCT fleet size from 500 to 1000 units has been shown to approximately double emissions at stratospheric cruise. However, as the fleet grows, emissions in different geographical regions grow at different rates. Consequently, stratospheric emissions in northern mid-latitudes are not projected to double as the fleet size doubles, while emissions in the northern tropics and southern hemisphere mid-latitudes are expected to more than double.

For an HSCT combustor with a NOx emission index of 5, the analyses show that the total NOx emissions below 13 kilometers altitude are not very sensitive to the presence or absence of an HSCT fleet. This suggests that to first-order the assessment of the effects of an HSCT fleet are largely decoupled from the assessment of subsonic aircraft effects. In some geographical regions, however, the changes may be greater (e.g., the North Atlantic).

The aircraft emissions inventories for scheduled air traffic developed in this study have been combined at NASA Langley with results for non-OAG scheduled operations (charter, military, and internal former Soviet Union) to create inventories of total aircraft emissions in the year 2015. These inventories are being used by the NASA Atmospheric Effects of Aviation Project (AEAP) in the 1995 AESA assessment of HSCT ozone impact.

5.6 Database Availability

The inventories of jet fuel burned and emissions (NOx, CO, total hydrocarbons) have been calculated for projected subsonic and HSCT fleets for the year 2015. These data will be available on a 1 degree latitude x 1 degree longitude x 1 km altitude grid by contacting Karen H. Sage (sage@uadp2.larc.nasa.gov) at NASA Langley Research Center or by sending a request to the Atmospheric Sciences Division, NASA Langley Research Center, Hampton, VA 23681-0001.

6. References

- Albritton, D. L., W. H. Brune, A. R. Douglass, F. L. Dryer, M. K. W. Ko, C. E. Kolb, R. C. Miake-Lye, M. J. Prather, A. R. Ravishankara, R. B. Rood, R. S. Stolarski, R. T. Watson, and D. J. Wuebbles, *The Atmospheric Effects of Stratospheric Aircraft: Interim Assessment Report of the NASA High-Speed Research Program*, NASA Reference Publication 1333, 1993.
- Baughcum, S. L., S. C. Henderson, P. S. Hertel, D. R. Maggiora, and C. A. Oncina, *Stratospheric Emissions Effects Database Development*, NASA CR-4592, 1994.
- Boeing Commercial Airplane Group, 1993 Current Market Outlook, 1993.
- Considine, D. B., A. R. Douglass, and C. H. Jackman, "Sensitivity of two-dimensional model predictions of ozone response to stratospheric aircraft: An update", *J. Geophys. Res.*, **100**, pp. 3075-3090 (1995).
- Landau, Z. H., M. Metwally, R. Van Alstyne, and C. A. Ward, "Jet Aircraft Engine Exhaust Emissions Database Development -- Year 1990 and 2015 Scenarios," NASA CR-4613, 1994.
- Miake-Lye, R. C., J. A. Matulaitis, F. H. Krause, W. J. Dodds, M. Albers, J, Hurmouziadis, K.L. Hasel, R. P. Lohmann, C. Stander, J. H. Gerstle, and G. L. Hamilton, "High Speed Civil Transport Aircraft Emissions," in *The Atmospheric Effects of Stratospheric Aircraft: A First Program Report*, M. J. Prather and H. L. Wesoky, Eds., 1992.
- Spicer, C. W., M. W. Holdren, D. L. Smith, D. P. Hughes, and M. D. Smith, "Chemical Composition of Exhaust from Aircraft Turbine Engines," *J. Engineering for Gas Turbines and Power*, **114**, pp. 111-117 (1992).
- Stolarski, R. S., and H. L. Wesoky (eds.), *The Atmospheric Effects of Stratospheric Aircraft: A Third Program Report*, NASA Reference Publication 1313, 1993.
- U. S. Standard Atmosphere, 1976, U.S. Government Printing Office, 1976.
- Wuebbles, D. J., D. Maiden, R. K. Seals, Jr., S. L. Baughcum, M. Metwally, and A. Mortlock, "Emissions Scenarios Development: Report of the Emissions Scenarios Committee," in *The Atmospheric Effects of Stratospheric Aircraft: A Third Program Report*, R. S. Stolarski and H. L. Wesoky, eds., NASA Reference Publication 1313, 1993.

Appendix A - World Passenger Demand Forecast

4.62% 8.05% 3.54% 5.07% 5.34% 7.92% 5.70% 4.16% 5.81% 5.01% 4.08% 5.20% 4.48% 4.75% 5.38% 7.03% 991-2015 Average Growth Rate 535,482 152,698 89,918 73,850 26,316 22,376 64,163 93,627 43,461 59,695 28,163 2015 445,013 123,092 437,999 297,690 92,463 3,925,296 4.58% 6.65% 5.37% 6.11% 3.31% 3.63% 6.24% 3.64% 4.03% 3.96% 4.43% 3.39% 4.78% 4.11% 4.09% 3.88% 4.48% Growth 2010-201 Rate 76,119 48,849 3,137,799 2010 60,816 117,570 20,839 23,276 307,900 366,412 18,713 52,652 35,534 74,275 75,387 388,063 219,963 2005-2010 4.87% 4.06% 4.15% 6.69% 3.78% 4.22% 4.32% 4.59% 7.45% 5.74% 3.78% 4.95% 4.25% 4.27% 6.54% 3.54% 4.92% 4.02% 4.63% Growth 28,858 39,627 2,473,985 860,974 252,344 299,023 159,139 15,545 49,215 60,236 270,878 88,926 63,217 16,367 76,883 19,110 241,051 42,821 5.19% 2000-2009 7.07% 4.41% 7.53% 3.74% 4.58% 4.62% 4.78% 7.93% 6.05% 4.22% 5.17% 4.46% 4.43% 3.96% 5.48% 4.28% 4.82% Growth 47,689 184,989 66,288 51,413 12,722 31,904 241,004 12,938 23,204 15,500 1,921,030 544,736 203,233 5,474 58,876 34,231 39,271 171,327 5.79% Growth 995-2000 5.38% 8.85% 7.04% 5.91% 5.04% 4.16% 4.94% 5.57% 4.40% 5.54% 4.69% 4.91% 4.39% 8.40% 4.75% 18,449 1,450,116 26,897 29,950 47,179 9,714 36,700 121,034 41,455 25,107 118,193 4,416 188,512 73,938 10,552 1995 433,867 991-1995 7.94% 5.50% 4.91% 6.20% 12.34% 2.08% 8.26% 3.79% 8.11% 8.92% 3.99% 5.26% 9.41% 6.65% 8.00% 11.33% 7.61% Growth WORLD PASSENGER TRAFFIC FORECAST 26,869 87,065 3,565 36,476 148,216 9,718 19,578 86,003 40,348 33,773 6,779 46,430 25,811 14,261 18,455 8,002 27,023 5,657 1,138,012 Year Intra & Dom Indian Sub Continent Intra & Domestic Mid East/Africa Intra & Domestic Latin America RPMs IN MILLIONS Europe-Indian Sub Continent Intra & Domestic Aisa/Pacific Intra & Domestic N. America Other Indian Subcontinent N. America-Latin America Intra & Domestic Europe N. America-Asia/Pacific Europe-Latin America Europe-Asia/Pacific N. America-Europe Other N. America Misc Long Range Europe-Mid East CIS International Regional Flow Europe-Africa Other African **A-1**

Appendix B - HSCT Route System Gateway Cities

City	City
Code	Name
Code	Name
1	
ACA	Acapulco, Mexico
AKL	Auckland, New Zealand
AMS	Amsterdam, The Netherlands
ANC	Anchorage, Alaska, USA
ATH	Athens, Greece
ATL	Atlanta, Georgia, USA
BAH	Bahrain, Bahrain
BER	Berlin, Germany
BKK	Bangkok, Thailand
BOG	Bogota, Columbia
BOM	Bombay, India
BOS	Boston, Massachusetts, USA
BRU	Brussels, Belgium
BUE	Buenos Aires, Argentina
CAI	Cairo, Egypt
CAN	Guangzhou, China
ccs	Caracas, Venezuela
CHI	Chicago, Illinois, USA
CMB	Colombo, Sri Lanka
CPH	Copenhagen, Denmark
CVG	Cincinnati, Ohio, USA
DEL	Delhi, India
DFW	
	Dallas, Texas, USA
DHA	Dharan, Saudia Arabia
DKR	Dakar, Senegal
DTW	Detroit, Michigan, USA
FDF	Fort-de-France, Martinique
FRA	Frankfurt, Germany
GUM	Guam, Guam
GVA	Geneva, Switzerland
HAV	Havana, Cuba
HEL	Helsinki, Finland
HKG	Hong Kong, Hong Kong
HNL	Honolulu, Hawaii, USA
HOU	Houston, Texas, USA
JKT	Jakarta, Indonesia
JNB	Johannesburg, South Africa
KHI	Karachi, Pakistan
KHV	Khabarovsk, Russian Federation
LAX	Los Angeles, California, USA
LIM	Lima, Peru
LIS	Losbon, Portugal
LON	London, England, UK
MAD	5
	Madrid, Spain
MEL	Melbourne, Australia
MEX	Mexico City, Mexico

C 211	Tair
City	City
Code	Name
	l.,
MIA	Miami, Florida, USA
MIL	Milan, Italy
MNL	Manila, Philippines
MOW	Moscow, Russian Republic
MRU	Mauritius, Mauritius
MSP	Minneapolis-St, Paul, Minnesota, USA
MUC	Munich, Germany
NAN	Nandi, Fiji
NYC	New York, New York, USA
OSA	Osaka, Japan
OSL	Oslo, Norway
PAR	Paris, France
PEK	Beijing, China
PER	Perth, Autralia
PHL	Philadelphia, Pennsylvania, USA
PPT	Papeete, Tahiti, French Polynesia
PTY	Panama City, Panama
RIO	Rio de Janeiro, Brasil
ROM	Rome, Italy
SCL	Santiago, Chile
SEA	Seattle, Washington, USA
SEL	Seoul, Korea
SFO	San Francisco, California, USA
SHA	Shanghai, China
SIN	Singapore, Singapore
SJU	San Juan, Puerto Rico
SNN	Shannon, Ireland
STL	Saint Louis, Missouri, USA
STO	Stockholm, Sweden
SYD	Sydney, Australia
TLV	Tel Aviv, Israel
TPE	Taipei, Taiwan
TYO	Tokyo, Japan
VIE	Vienna, Austria
WAS	Washington, DC, USA
WAW	Warsaw, Poland
YHZ	Halifax, Nova Scotia, Canada
YMQ	Montreal, Quebec, Canada
YVR	Vancouver, British Columbia, Canada
YYC	Calgary, Alberta, Canada
YYZ	Toronto, Ontario, Canada

Appendix C. Departure Statistics

This appendix is a table of departure statistics for the universal network for a fleets of 500 and 1000 active Mach 2.4 HSCTs. For each gateway citypair, flight distances for the great circle route, supersonic flight legs, and total path length are given in nautical miles. Stops enroute are identified in the column marked via. Block time and total trip times are given in hours with the fraction of time compared to an all subsonic flight. Daily departures and load factors are shown for both fleets of 500 and 1000 HSCTs. The first section of the table shows city pairs used by the 500 unit fleet, while the second section includes flights used only by the 1000 unit fleet.

	Load	Factor	29	98	29	88	92	8	65	89	29	8	89	29	99	29	29	63	29	29	61	29	29	29	29	29	19	29	25	29	29	67	1
1000 Units	Daily	Departures	4	56	8	20	4	24	24	80	4	8	80	9	16	4	4	9	8	4	50	4	9	4	8	2	14	4	5	7	12	8	•
	Load	Factor	61	98	67	8	29	83	8	89	67	29	89	67	64	67	29	29	65	67	62	29	29	29	29	99	62	6	29	29	62	29	9
500 Units	Daily	Departures	4	22	8	16	α.	14	5	60	4	9	4	4	14	8	8	4	8	8	12	8	4	8	7	€	9	4	ဖ	8	9	8	V
	Percent	subsonic	8	43	46	22	43	49	47	26	4	43	54	51	46	61	29	29	47	56	20	22	09	28	20	48	22	23	52	51	84	49	72
rs)		Trip	6.45	3.58	4.19	96.9	4.53	3.14	2.39	6.86	4.38	4.43	7.10	4.31	4.26	4.85	5.53	4.46	4.13	4.50	3.52	3.78	5.45	4.14	4.77	4.26	5.31	4.73	4.59	4.50	3.87	4.05	4.91
Time (hours)		Block	5.45	3.58	4.19	5.96	4.53	3.14	2.39	5.86	4.38	4.43	6.10	4.31	4.26	4.85	5.53	4.46	4.13	4.50	3.52	3.78	5.45	4.14	4.77	4.26	5.31	4.73	4.59	4.50	3.87	4.05	4.91
		Path	5085	3825	4530	6042	4833	3236	2210	2907	4833	4766	6174	4001	4232	3876	4630	3672	4038	4017	3247	3347	4483	3517	4892	4234	4317	4415	4214	4135	3806	3848	4340
(n.m.)		Cruise	3757	3165	3751	4817	3936	2614	1635	4691	4055	3918	4913	2844	3239	2214	2819	2218	3048	2716	2325	2267	2661	2238	3835	3244	2520	3141	2948	2898	2906	2826	2879
Distance (n.m.)		CC	4937	3826	4123	2659	4834	2879	2209	5671	4541	4768	6130	3812	4230	3567	4262	3412	4015	3607	3155	2972	4160	3232	4397	4057	4273	4089	3997	4005	3648	3756	4155
		Via																															
		Via	POM			Ä				H			Ĭ																				
		Dest	HKG	ĭ	봇	Γ¥	OSA	PER	PPT	SFO	SIS	TYO	YVR	ATL	SCS	풍	DFW	DTW	MIA	MSP	N	Y W	YVR	λΥZ	HKG	TPE	N	BER	FRA	GVA	PON	MAD	MOC
		Origin	AKL	AKL	AKL	AKL	AKL	AKL	AKL	AKL	AKL	AKL	AKL	AMS	AMS	AMS	AMS	AMS	AMS	AMS	AMS	AMS	AMS	AMS	ANC	ANC	ATH	ATL	ATL	ATL	ATL	ATL	ATL

		Factor	29	29		9		99	19 1	63			29	19		19					99			29		62	29	29	19	62	29	99)
1000 Units	Daily	Departures	8	7	16	22	9	9	80	26	7	9	7	4	16	4	2	24	9	22	50	2	12	2	4	24	80	4	4	18	a	4	
	Load	Factor	67	29	29	29	29	67	67	62	65	29	29	29	61	29	62	67	29	29	65	62	29	67	29	62	29	29	29	29	29	29	
500 Units	Daily	Departures	2	7	4	2	2	4	9	16	7	8	8	4	10	2	8	9	7	7	20	2	7	8	8	14	4	2	8	10	8	2	
	Percent	subsonic	22	48	62	62	8	53	26	24	22	65	62	48	54	55	61	29	58	62	54	50	54	52	5	47	49	47	9	48	49	55	
ırs)		Trip	4.18	3.55	4.03	2.93	4.92	4.46	4.89	4.10	4.04	5.46	6.15	4.54	4.13	4.41	5.78	3.05	3.79	2.87	3.10	4.79	2.62	3.66	3.62	2.99	3.31	2.67	4.74	3.41	3.69	3 67	;
Time (hours)		Block	4.18	3.55	4.03	2.93	4.92	4.46	4.89	4.10	4.04	5.46	6.15	4.54	4.13	4.41	5.78	3.05	3.79	2.87	3.10	4.79	2.62	3.66	3.62	2.99	3.31	2.67	4.74	3.41	3.69	3.67	
		Path	3962	3476	3460	2093	4743	3861	4671	3663	3444	4189	4943	4440	3559	3748	4670	3009	3077	2783	3111	4334	2545	3286	3270	2937	3100	2607	3868	3239	3428	3339	
(n.m.)		Cruise	2897	2656	2239	1008	3484	2515	3407	2501	2202	2202	2803	3333	2312	2379	2681	2343	1844	2137	2459	2971	1965	2270	2275	2275	2271	2021	2289	2401	2467	2343	
Distance (n.m.)		၁၅		3327	2893	2024	3449	3801	3976	3412	3274	3820	4517	4311	3436	3627	4306	2259	2889	1989	2505	4333	2110	3177	3185	2827	2985	2506	3602	3176	3370	3000	
		Via																															
		Via																															
		Dest	PAR	SNN	BKK	CMB	HKG	JK1	N N N	SIN	BOS	풄	DFW	MIA	NAC	WAS	YVR	OSA	PER	SEL	TYO	MAD	SIN	FRA	GVA	LON	PAR	SNN	동	NYC	WAS	YMO	
		Origin	ATL	ATL	BAH	BAH	BAH	BAH	BAH	BAH	BER	BKK	BKK	BKK	BKK	BOG	BOM	BOS	BOS	BOS	BOS	BOS	BRU	BRU	BRU	BRU							

	Load	Factor	क्र	29	29	29	29	67	65	29	62	61	29	63	67	62	99	65	29	29	29	29	29	29	61	29	29	67	65	6 2	29	89	29
1000 Units	Daily	Departures F	20	ω	4	4	4	8	14	8	20	9	8	12	9	5	56	9	12	80	8	24	∞	8	4	8	8	မှ	12	4	9	6	4
	Load	Factor	67	67	29	67	29	67	29	29	67	29	29	67	9	29	29	8	67	29	B	29	29	S	29	29	29	29	29	29	29	88	29
500 Units	Dally	Departures	12	&	4	8	a	2	10	7	4	4	8	9	4	4	14	4	4	4	8	€	9	8	7	8	7	8	€	8	4	12	7
	Percent	subsonic	61	28	22	47	43	43	46	46	49	45	53	61	8	99	28	29	20	29	9	69	45	9	22	23	29	29	29	26	28	29	23
ırs)		Trip	7.14	7.55	7.65	4.48	3.34	3.82	3.80	4.41	2.13	4.06	5.17	5.08	5.04	5.34	4.41	5.13	8.45	4.72	5.53	8.18	3.32	5.56	4.71	4.04	5.76	4.32	5.09	5.27	5.40	10.69	4.49
Time (hours)		Block	6.14	6.55	6.65	4.48	3.34	3.82	3.80	4.41	2.13	4.06	5.17	5.08	5.04	5.34	4.41	5.13	7.45	4.72	5.53	7.18	3.32	5.56	4.71	4.04	5.76	4.32	5.09	5.27	5.40	8.69	4.49
		Path	5870	6549	6652	4359	3509	4073	3781	4348	1897	4109	4498	4030	4014	3680	3681	4178	5959	3844	4364	5636	3480	4592	3911	3562	4784	3282	4435	447	4594	6772	3880
(n.m.)		Cruise	4401	5126	5180	3262	2878	3354	2925	3297	1359	3213	2906	2269	2274	1508	2274	2456	3667	2271	2415	3397	2849	2738	2384	2389	2871	1725	2880	2803	2871	4058	2514
Distance (n.m.)		၁ဗ	5441	2989	6282	4357	3508	4031	3780	4347	1837	4118	4497	3761	3806	3678	3423	3922	5614	3595	4176	5435	3339	4214	3777	3432	4455	3280	4115	4303	4286	6691	3824
		Via																														140	
		Via	DKR	DKR	7														SEA			SEA										SEA	
		Dest	MAD	PAR	LAX	FRA	LIS	LON	MAD	Z	N	PAR	ROM	FRA	GVA	Ä	LON	MUC	OSA	PAR	ROM	1 ¥0	N	SEA	FRA	NO TO	FRA	Ä	LON	MAD	PAR	TPE	JKT
		Origin	BUE	BUE	CAN	SSS	SSS	SSS	SSS	SSS	SSS	SSS	SSS	픙	ᇙ	돐	풍	ᇙ	ᇙ	ᇙ	돐	ᇙ	CPH	ᅜ	CVG	CVG D	DFW	DFW	DFW	DFW	DFW	DFW	DHA

				Distance (n.m.)	(n.m.)		Time (hours)	īŠ		500 Units		1000 Units	
									Percent	Daily	Load	Daily	Load
Origin	Dest	Via	Via	ည္ဗ	Cruise	Path	Block	Trip	subsonic	Departures	Factor	Departures	Factor
DHA	MNL			4001	3406	4690	4.92	4.92	56	9	29	10	61
DHA	SIN			3436	2500	3682	4.13	4.13	54	8	67	8	29
DKR	HAV			3691	3043	3692	3.48	3.48	43	8	67	4	9
DTW	FRA			3603	2273	3826	4.68	4.68	29	8	63	2	29
DTW	PAR			3430	2396	3615	4.13	4.13	54	a	29	2	29
FDF	FRA			3909	2878	3948	4.17	4.17	49	8	67	4	29
FDF	LON			3590	2922	3635	3.52	3.52	4	10	62	12	4
FDF	MAD			3313	2523	3359	3.49	3.49	47	00	29	4	9
FDF	PAR			3668	2826	3699	3.76	3.76	46	22	63	28	65
FRA	HOE			4545	2949	4786	5.67	5.67	22	8	29	4	29
FRA	MIA			4188	3140	4239	4.40	4.40	48	9	67	€	65
FRA	NAC			3339	2380	3401	3.74	3.74	20	20	99	32	63
FRA	표			3420	2427	3476	3.83	3.83	20	8	67	8	67
FRA	WAS			3534	2447	3590	4.02	4.02	51	9	67	80	67
FRA	ΥMQ			3161	2323	3502	4.01	4.01	57	R	64	4	62
FRA	YVR			4351	2719	4675	5.74	5.74	9	4	99	9	65
FRA	YYC			4062	2776	4345	5.05	5.05	22	8	62	7	99
FRA	YYZ			3422	2293	3671	4.37	4.37	22	8	. 29	9	62
BUM	Ä			3296	2679	3298	3.18	3.18	43	14	62	18	64
BUM	SYD			2869	2461	3058	2.99	2.99	46	8	99	4	23
BUM	TYO			1358	829	1356	1.74	1.74	52	8	99	36	63
GVA	NYC			3346	2385	3385	3.71	3.71	20	10	5	16	61
GVA	YMQ			3191	2314	3483	3.98	3.98	26	4	29	80	65
出	NAC			3565	2590	3742	4.13	4.13	52	8	29	9	9
HKG	Ĭ			4812	4075	4842	4.37	4.37	42	4	29	9	64
HKG	JKT			1761	1245	1782	2.04	2.04	49	4	29	20	61
HKG	LAX	7		6283	5175	6591	6.54	7.54	26	09	88	89	89
HKG	MEL			3992	3857	4912	4.78	4.78	54	8	29	4	29
HKG	PER			3256	2908	3545	3.37	3.37	46	4	.	4	29
HKG	SEA	TYO		5625	4713	6010	6.02	7.02	28	4	88	4	89
HKG	SFO	TYO		5994	5022	9069	6.20	7.20	56	24	88	28	68

	Load	Factor	29	65	2	89	29	89	99	65	62	65	63	29	99	64	61	63	61	99	61	99	67	67	29	62	67	64	65	29	67	64	
1000 Units	Daily	Departures F	94	14	8	40	4	80	84	9	22	89	16	12	16	36	9	24	4	124	1	∞	4	9	4	18	12	12	24	8	4	78	
	Load	Factor	9	5	49	29	29	29	83	83	61	8	62	29	29	64	29	7 9	29	99	98	29	29	67	29	65	67	29	65	29	29	99	1
500 Units	Daily	Departures	9	12	9	32	8	4	36	9	20	52	€	4	12	14	7	20	8	6	4	9	8	4	8	€	4	∞	8	8	4	18	!!
	Percent	subsonic	52	47	26	29	28	52	47	45	42	4	46	47	48	47	65	42	42	4	47	35	22	48	46	93	23	45	51	47	83	3	í
urs)		Trip 8	1.75	4.12	2.12	7.08	4.37	6.93	2.38	4.68	4.20	3.49	2.49	2.50	4.15	2.28	5.12	4.03	4.04	3.26	2.52	4.95	5.26	3.13	2.95	3.76	2.37	3.18	4.35	4.71	8.08	6.55	((
Time (hours)		Block	1.75	4.12	2.12	90.9	4.37	5.93	2.38	4.68	4.20	3.49	2.49	2.50	4.15	2.28	5.12	4.03	4.04	3.26	2.52	4.95	5.26	3.13	2.95	3.76	2.37	3.18	4.35	4.77	7.08	6.55	
		Path	1397	4532	1865	5935	3391	0009	2217	4799	4599	3567	2383	2325	4440	2082	3581	4419	4395	3312	2349	4377	4536	3183	2957	3997	2126	3285	3859	4729	7173	4945	
(n.m.)		Cruise	879	3810	1316	4548	1852	4786	1652	3764	3845	2846	1822	1723	3651	1525	1530	3707	3670	2634	1747	2908	2898	2541	2337	3291	1516	2657	2599	3585	2659	2468	5446
Distance (n.m.)		၁ဗ	1392	3981	1585	5533	3396	5825	2216	4789	4597	3557	2383	2324	3950	2080	3579	4409	4394	3311	2347	4200	4365	2940	2849	2968	2053	3145	3859	4666	5948	4727	F007
		Via																															
		Via				TYO		BUM																							PER		
		Dest	N N	SYD	170	YVR	HOU	농	LAX	MEL	Z Z	OSA	PPT	SEA	SEL	SFO	STL	SYD	TPE	1 40	Y	LON LON	PAR	OSA	SEL	SYD	TPE	170	8	SIN	SYD	NO NO	
		Origin	HKG	HKG	HKG	HKG	Ĭ	Ĭ	¥	¥	Ĭ	ĭ	¥	¥	Ĭ	¥	¥	¥	¥	¥	Ĭ	HOH	10	KT	-X	¥	Ϋ́	JKT	S N N	S S S	S S	LAX	XV -

			Distance (n.m.)	(n.m.)		Time (hours)	ırs)		500 Units		1000 Units	
								Percent	Daily	Load	Daily	Load
Dest	Via	Via	CC	Cruise	Path	Block	Trip	subsonic	Departures	Factor	Departures	Factor
يـا	TYO		6335	4942	6372	6.41	7.41	54	4	88	4	89
z			4798	4019	4799	4.36	4.36	42	8	67	2	67
4			4956	3790	4957	4.95	4.95	46	40	2	4	99
¥	TYO		5416	4929	6373	6.43	7.43	63	4	67	4	29
_			3566	2929	3567	3.39	3.39	43	9	65	€	62
_	ΙΛΟ		5178	3859	5390	6.10	7.10	63	32	67	52	67
_	0 Y		7612	6159	7626	7.32	8.32	47	4	89	€	89
۵	Ħ		6508	5359	9699	6.41	7.41	48	48	89	48	89
ш	TYO		5894	4520	5913	6.04	7.04	52	40	98	4	29
0			4724	3859	4726	4.43	4.43	43	58	2	99	63
Ø			2276	1167	2402	3.03	3.03	58	8	9	18	64
NYC			3164	1710	3379	3.87	3.87	55	8	29	4	29
ပ			2915	2291	2916	2.93	2.93	45	9	67	9	99
0			4163	3594	4336	4.02	4.02	44	10	62	12	9
d			3835	3111	3843	3.69	3.69	44	22	6	26	64
۵.			3476	2511	3857	4.45	4.45	28	8	67	ဖ	61
ပ			2989	2386	3052	3.08	3.08	46	20	99	80	65
ے			3070	2432	3127	3.16	3.16	46	9	99	10	9
_	DKR		4993	4127	5376	5.55	6.55	09	4	67	€	67
⋖			4156	2479	4376	5.47	5.47	09	4	29	9	29
0			4649	2468	4851	6.38	6.38	63	9	67	10	67
_			3633	2930	3634	3.51	3.51	44	8	67	4	67
_			3638	2343	3824	4.59	4.59	22	4	62	9	29
Δ	ZQ5	BUM	9184	7181	9860	10.53	12.53	09	9	67	12	63
0	ZQ5		5175	3519	5560	6.63	7.63	89	12	29	40	62
Ş			3184	2452	3241	3.35	3.35	47	18	62	26	64
₫			2817	2327	3153	3.34	3.34	53	4	29	80	29
œ			4090	2458	4323	5.40	5.40	09	4	29	80	61
ပ			3786	2513	3994	4.71	4.71	26	4	29	80	8
Z			3079	2298	3322	3.70	3.70	54	14	29	28	62
×			4892	3203	4893	5.17	5.17	49	∞	29	10	62

A108 3835 3108 3108 3108 3108 3108 3108 3108 3108		\\ \	ć			2		SUO ODE		1000 Units	
MIA MIA MIA NYC NYC NYC NYC NAS OSA PPT SFO HNL S258 A412 MUC NYC NYC NYC NYC NYC NYC NYC N							Percent	Daily	Load	Dally	Load
MIA NYC NYC NYC NAS NAS NAS NAS NAS NAC NYC NYC NAS NYC NYC NYC NYC NYC NYC NYC NY		1	Cruise	Path	Block	Trip	subsonic	Departures	Factor	Departures	Factor
NYC RIO NAS OSA OSA PPT SFO HNL SFO HNL SFO HNL SFO NYC		3835	2993	3836	3.82	3.82	45	4	67	9	29
HIO 4396 WAS 3306 OSA 4378 PPT 3614 SFO HNL 6828 SIN 3258 TYO 4412 MUC 4339 PAR 3976 RIO 3624 RIO 3624 RIO 3624 ROM 3626 NYC 3459 NYC 3459 NYC 3496 NYC 4036 NYC 3496 NYC 3496 OSA SEA 5996 OSL 3192 PAR ANC 8908 OSL 3192 PAR ANC 8908 OSL 3192 PAR ANC 8908 OSL 3192			2327	3124	3.28	3.28	47	10	67	8	8
WAS 3306 OSA 4378 PPT 3614 SFO HNL 6828 SIN 3258 TYO 4412 RIO 4433 PAR 3624 RIO 3624 ROM 4493 SCL 3459 NYC 3459 NYC 3496 VYR 4501 YYC 4216 PAR ANC 8908 OSA SEA 5996 OSL 3147 ROM 3704			3594	4592	4.50	4.50	47	10	67	12	92
OSA 4378 PPT 3614 SFO HNL 6828 SIN 3258 TYO 4412 MUC 4339 PAR 836 NYC 3459 NYC 3459 NYC 3456 OSA SEA 5696 OSA SEA 5906			2394	3313	3.56	3.56	48	2	29	2	29
PPT 3614 SFO HNL 6628 SIN 3258 TYO 4412 MUC 4339 PAR 3976 RIO 3624 RIO 3459 NYC 3459 NYC 3496 NYC 4036 NYC 3496 VYR 4501 YYC 4216 PAR ANC 8908 OSL 3192 PAR SEA 5996 OSL 3704 SIN 5704			3733	4808	4.74	4.74	49	2	29		29
SFO HNL 6828 SIN 3258 TYO 4412 MUC 4339 PAR 3976 RIO 3624 ROM 4493 SCL 3692 NYC 3459 NYC 3496 NYC 4036 NYC 4036 NYC 3496 NYC 3496 NYC 3496 OSA SEA 5996 OSL 3192 PAR ANC 8908 OSA SEA 5996 OSL 3192			2788	3614	3.65	3.65	46	9	99	8	65
SIN TYO MUC MUC MUC MUC A339 PAR RIO ROM SCL NYC WAS SYD TYO NYC WAS SYD YVR YVR YVR YVR OSA SEA S192 A216 S192 SOB OSA SEA S192 SOB SOB SOB SOB SOB SOB SOB SO			5289	6881	96.9	7.96	49	4	89	4	89
TYO			3652	4679	4.59	4.59	63	9	61	14	92
MUC 4339 PAR 3976 RIO 3624 ROM 4493 SCL 3459 NYC 3459 NYC 4036 NYC 4036 NYC 3496 NYC 4216 YYC 4501 YYC 4216 PAR ANC 8908 OSL 3192 PAR 3147 ROM 3704			3717	4763	4.67	4.67	48	4	29	9	99
PAR 3976 RIO 3624 ROM 4493 SCL 3624 NYC 3459 NYC 4036 NYC 3496 NYC 3496 VYC 4216 YYC 4216 PAR ANC 8908 OSA SEA 5996 OSL 3192 PAR TVO 3147 ROM 3704			3071	4364	4.72	4.72	20	4	99	4	29
RIO 3624 ROM 4493 SCL 3592 NYC 3459 NYC 3459 TYO 1645 NYC 4036 NYC 3496 NYC 4216 YYC 4216 YYC 8908 OSA SEA 5996 OSL 7VC 3192 ROM 3704 ROM 370			3090	3989	3.99	3.99	46	9	64	9	99
ROM 4493 SCL 3592 NYC 3459 WAS 3656 SYD 1645 NYC 4036 NYC 3496 VVR 4501 YYC 4216 PAR ANC 8908 OSL 3192 PAR 3192 PAR 3704 SIN SEA 3704			3983	4781	4.38	4.38	22	12	29	20	65
SCL NYC NYC NYS SYD TYO TYO NYC NYC NYC NYC NYC NYC NYC NYC NAS NYC			3232	4495	4.77	4.77	49	4	62	4	29
NYC WAS SYD TYO TYO TYO NYC			2983	3689	3.55	3.55	45	4	29	9	29
WAS 3656 SYD 3380 TYO 1645 NYC 4036 WAS 3496 WAS 3691 YYC 4216 PAR ANC 8908 OSA SEA 5996 OSL 3192 PAR ROM 3704			2542	3529	3.79	3.79	49	14	65	20	99
SYD TYO TYO NYC NYC NYC NYC NAS			2607	3718	4.07	4.07	20	8	61	8	29
TYO 1645 NYC 4036 NYC 3496 WAS 3691 YVR 4216 PAR ANC 8908 OSA SEA 5996 OSL 3192 PAR ROM 3704			3196	3920	3.73	3.73	20	8	. 67	4	8
NYC NYC NYC NYC NAS NAS 3496 NYC YVR YVC PAR ANC 0SA SEA 0SL PAR ROM 3704			1083	1646	1.98	1.98	51	4	99	24	99
NYC 3496 WAS 3691 YVR 4501 YYC 4216 PAR ANC 8908 OSA SEA 5996 OSL 3192 PAR 80M 3704			2573	4207	5.03	5.03	. 57	4	62	9	61
WAS 3691 YVR YYC 4216 PAR ANC 8908 OSA SEA 5996 OSL 3192 PAR 3147 ROM 3704			2569	3549	3.79	3.79	49	12	61	16	65
YVR YYC YYC A216 PAR ANC 8908 OSA SEA 5996 OSL PAR 3192 ROM 3704			2635	3738	4.07	4.07	20	8	29	4	67
YYC YYC PAR ANC 8908 OSA SEA 5996 OSL PAR 3192 PAR 3147 ROM 3704	•		2679	4828	9 0.9	6.08	62	8	92	8	29
PAR ANC 8908 OSA SEA 5996 OSL 3192 PAR 3147 ROM 3704			2736	4499	5.39	5.39	28	2	62	8	29
OSA SEA 5996 OSL 3192 PAR 3147 ROM 3704			7057	9143	9.08	10.08	49	4	29	4	29
OSL 3192 PAR 3147 ROM 3704			3667	9959	8.62	9.62	74	4	29	20	29
PAR 3147 ROM 3704			2610	3340	3.35	3.35	47	8	29	4	67
ROM 3704			2382	3215	3.39	3.39	48	28	ß	42	99
OLVO CTA TO MIS			2548	3739	4.18	4.18	51	14	29	20	67
31N 3EA 110 82/6	170	8276	2697	9143	11.24	13.24	69	9	88	9	8
Ors		1386	870	1391	1.75	1.75	25	4	29	28	65
SNN		2668	2132	2722	2.76	2.76	46	9	29	10	29

Distance (n.m.) Time (hours) 50	Time (hours) Percent	Time (hours) Percent	Time (hours) Percent	Time (hours) Percent	Percent	Percent	Percent		20	500 Units Daily	Load	1000 Units Daily	Load
Via Via GC Cruise Path Block Trip S	Via GC Cruise Path Block Trip	GC Cruise Path Block Trip	Cruise Path Block Trip	Path Block Trip	Block Trip	Trip		subsonic		Departures	Factor		Factor
3395 2600 3548 3.75	3395 2600 3548 3.75 3.75	2600 3548 3.75 3.75	2600 3548 3.75 3.75	3548 3.75 3.75	3.75 3.75	3.75		20		4	29	9	29
LON 4920 3331 5113	4920 3331 5113 6.02 7.02	3331 5113 6.02 7.02	3331 5113 6.02 7.02	5113 6.02 7.02	6.02 7.02	7.02		99		4	29	12	99
SEA 5844 3397 6243 8.35	5844 3397 6243 8.35 9.35	3397 6243 8.35 9.35	3397 6243 8.35 9.35	6243 8.35 9.35	8.35 9.35	9.35		7	₹	4	29	3 6	65
3671 2359 3779 4.49 4.49	2359 3779 4.49 4.49	2359 3779 4.49 4.49	2359 3779 4.49 4.49	3779 4.49 4.49	4.49 4.49	4.49		40	22	4	6 7	∞	99
3694 3032 3840 3.78 3.78	3032 3840 3.78 3.78	3032 3840 3.78 3.78	3032 3840 3.78 3.78	3840 3.78 3.78	3.78 3.78	3.78		4	46	2	67	8	67
4344 3667	3667 4468 4.18	3667 4468 4.18	3667 4468 4.18	4468 4.18	4.18		4.18	7	7	12	65	14	63
4670 3965 4756 4.35 4.35	3965 4756 4.35 4.35	3965 4756 4.35 4.35	3965 4756 4.35 4.35	4756 4.35 4.35	4.35 4.35	4.35		•	43	16	62	8	62
2668 2183	2183 2797 2.84	2183 2797 2.84	2183 2797 2.84	2797 2.84	2.84		2.84		47	26	64	46	29
4217	3684 4428 4.08	3684 4428 4.08	3684 4428 4.08	4428 4.08	4.08		4.08		44	5	29	12	99
4260	3503 4393 4.24	3503 4393 4.24	3503 4393 4.24	4393 4.24	4.24		4.24		45	6	29	80	29
3228	2550 3264 3.28	2550 3264 3.28	2550 3264 3.28	3264 3.28	3.28		3.28		46	8	29	8	29
MIA 8478	8478 6360 8795 8.91	6360 8795 8.91	6360 8795 8.91	8795 8.91	8.91		9.91		51	4	6 7	4	67
DKR 4956 4046 5400 5.70	4956 4046 5400 5.70	4046 5400 5.70	4046 5400 5.70	5400 5.70	5.70		6.70		62	80	29	16	67
4835 2583 4988 6.50	4835 2583 4988 6.50	2583 4988 6.50	2583 4988 6.50	4988 6.50	6.50		6.50		62	8	67	4	63
GDX 5239	5239 3669 5716 6.74	3669 5716 6.74	3669 5716 6.74	5716 6.74	6.74		7.74		89	4	67	16	29
3343	3343 2448 3404 3.67	2448 3404 3.67	2448 3404 3.67	3404 3.67	3.67		3.67		49	∞	67	12	29
2984 2323	2323 3316 3.65	2323 3316 3.65	2323 3316 3.65	3316 3.65	3.65		3.65		22	10	61	18	99
3248 2417	2417 3459 3.81	2417 3459 3.81	2417 3459 3.81	3459 3.81	3.81		3.81		23	4	29	80	29
2422 2290	2290 2919 2.94	2290 2919 2.94	2290 2919 2.94	2919 2.94	2.94		2.94		53	8	29	9	63
4287	2869 4287 4.82	2869 4287 4.82	2869 4287 4.82	4287 4.82	4.82		4.82		51	4	64	4	29
3301	3301 2689 3303 3.18	2689 3303 3.18	2689 3303 3.18	3303 3.18	3.18		3.18		43	24	64	32	65
GUM 5096	5096 4439 5664 5.68	4439 5664 5.68	4439 5664 5.68	5664 5.68	5.68		6.68		9	4	29	80	29
ACA LAX 10000	LAX 10000 7361 10879 12.20	10000 7361 10879 12.20	7361 10879 12.20	10879 12.20	12.20		14.20		62	9	29	12	65
3901	3901 2592 3924 4.48	2592 3924 4.48	2592 3924 4.48	3924 4.48	4.48		4.48		25	7	62	8	29
3823	2461 4010 4.80	2461 4010 4.80	2461 4010 4.80	4010 4.80	4.80		4.80		21	8	67	4	64
4503 3774 4602 4.30	3774 4602 4.30	3774 4602 4.30	3774 4602 4.30	4602 4.30	4.30		4.30		4	2	99	10	67
TYO 5264 4058 5332 5.52	5264 4058 5332 5.52	4058 5332 5.52	4058 5332 5.52	5332 5.52	5.52		6.52		24	4	29	4	29
4131	4131 3397 4145 3.90	3397 4145 3.90	3397 4145 3.90	4145 3.90	3.90		3.90		43	16	65	18	9
SFO 4887 4080 4904 4.48 4.48	4080 4904 4.48	4080 4904 4.48	4080 4904 4.48	4904 4.48	4.48		4.48		42	4	29	80	67
2511 1976 2571	2511 1976 2571 2.66 2	1976 2571 2.66 2	1976 2571 2.66 2	2571 2.66 2	2.66 2	~	2.66		47	9	29	12	29
HNL 6448	6448 5233 6501 6.31 7	5233 6501 6.31 7	5233 6501 6.31 7	6501 6.31 7	6.31 7	7	7.31		23	16	89	20	89

	Load	Factor	88	65	99	92	92	29	99	29	9	22	9	92	99	99	99	29	29	29	89	29	29	29	29	29	3	67	67	29	29	62
1000 Units	Daily	Departures	8	28	46	99	88	2	24	16	16	œ	φ.	32	4	100	2	7	2	4	4	4	4	8	8	8	32	7	7	8	8	14
	Load	Factor	88	62	65	99	99	29	62	29	3																					
500 Units	Daily	Departures	16	26	8	14	26	8	22	12	12																					
	Percent	subsonic	22	42	52	5	45	46	43	29	45	22	28	55	22	22	79	51	65	63	79	65	69	SS	26	69	28	5	21	65	88	5
ırs)		Trip 9	6.70	4.08	3.94	2.08	2.89	3.97	4.02	6.58	3.97	2.00	13.00	1.90	1.60	1.59	4.63	3.44	2.70	7.03	9.73	2.72	7.49	3.91	4.76	3.95	1.83	3.40	2.27	5.60	3.65	1.98
Time (hours)		Block	5.70	4.08	3.94	2.08	2.89	3.97	4.02	5.58	3.97	2.00	11.00	1.90	1.60	1.59	4.63	3.44	2.70	6.03	8.73	2.72	6.49	3.91	4.76	3.95	1.83	3.40	2.27	5.60	3.65	1.98
		Path	5628	4441	4300	1741	2900	4314	4383	5257	4070	1720	10273	1424	1164	1166	2914	3132	1836	5603	6577	1946	5503	3418	4154	3614	1362	3079	1788	3904	3085	1385
(n.m.)		Cruise	4367	3706	3603	1151	2300	3597	3668	3893	3233	1183	7442	800	638	648	930	2215	791	4090	3431	948	3543	2272	2718	2548	761	2166	1066	1642	1715	929
Distance (n.m.)		CC.	2607	4439	3400	1740	2893	3931	4226	5176	4050	1439	6066	1423	1163	1164	2576	2993	1772	5158	2669	1787	5028	3349	3868	2536	1254	2975	1683	3902	2771	1339
		Via											GDX																			
		Via	TYO							TYO			BUM							DKR	BAH		ZQ5									
		Dest	TPE	ΤΛΟ	SYD	TPE	1 40	TPE	TYO	Y	Y	LAX	LON	MEL	NAN	SYD	BAH	BOS	CAI	잂	NIS SI	7[\	7	WAS	YYC	X X	SEA	<u>1</u>	SCS	Ĭ	≥	SJU
		Origin	SFO	SFO	NIS SIS	NIS.	SIN	SYD	SYD	TPE	Τ¥ο	ACA	AKL	AKL	AKL	AKL	AMS	AMS	AMS	AMS	AMS	AMS	AMS	AMS	AMS	ANC	ANC	ANC	ATL	ATL	ATL	ATL

	Load	Factor	67	67	99	65	64	61	67	67	29	29	29	29	29	29	29	29	99	29	62	29	29	29	29	67	29	29	29	8	29	29	ţ
1000 Units	Daily	Departures	4	2	4	22	7	9	2	4	8	2	9	2	2	2	9	10	24	12	8	80	4	8	2	9	10	7	2	26	8	4	
	Load	Factor																															
500 Units	Daily	Departures					٠																										
	Percent	subsonic	2	99	75	78	75	11	89	3	69	61	99	69	28	62	55	8	65	7	51	7	22	79	92	65	79	78	49	29	25	52	,
ırs)	•	Trip	8.95	4.99	4.16	4.85	3.95	4.53	2.55	7.54	2.56	4.75	2.56	5.98	1.83	4.07	1.72	2.90	1.92	6.34	5.47	2.05	2.73	6.21	6.11	3.44	6.81	6.48	3.33	1.63	4.11	1.83	
Time (hours)	•	Block	7.95	4.99	4.16	4.85	3.95	4.53	2.55	6.54	2.56	4.75	2.56	5.98	1.83	4.07	1.72	2.90	1.92	5.34	5.47	2.05	2.73	6.21	6.11	3.44	6.81	6.48	3.33	1.63	4.11	1.83	1
		Path	6037	4772	2672	3029	2676	2860	1756	5866	1866	3830	2342	4461	1286	3479	1282	2755	1536	5160	4931	1314	2168	4093	4045	3625	4402	4232	3124	1163	3620	1458	
(n.m.)	•	Cruise	3397	3476	936	928	1118	932	793	4087	950	2225	1698	2191	642	2238	724	2067	959	3958	3328	206	1290	1151	1155	2976	1124	1140	2291	610	2418	911	4004
Distance (n.m.)		ည္	5935	3382	2422	2748	2307	2602	1563	5396	1549	3496	1623	3915	1287	2918	1259	1998	1186	4070	4902	1314	2156	3545	3623	2320	3892	3774	3014	1094	3544	1454	0770
		Via																															
		Via	SEA							DKR										POM													
		Dest	TYO	CAN	GVA	LON	Z Z	PAR	CAI	잂	TLV	λλΣ	BOM	CAI	CMB	DHA	JKT	Ξ	MNL	SYD	FRA	MIA	NAC	FRA	GVA	HKG	NO NO	PAR	BRU	MIA	ROM	SJU	5
		Origin	ATL	ВАН	ВАН	ВАН	BAH	BAH	BER	BER	BER	BER	BKK	BOG	BOG	BOG	BOM	BOM	BOM	BOM	BOM	BOS	BOS	BOS	Bos								

				Distance (n.m.)	(n.m.)		Time (hours)	rs)		500 Units		1000 Units	
									Percent	Daily	Load	Daily	Load
Origin	Dest	Via	Via		Cruise	Path	Block	Trip	subsonic	Departures	Factor	Departures	Factor
BRU	TLV			1754	949	1891	2.61	2.61	63			2	65
BRU	1	CDX		5103	3592	5586	6.59	7.59	89			4	67
BUE	ROM	DKR		6019	4468	6555	7.06	8.06	62			4	67
CAI	FRA			1575	795	1642	2.33	2.33	62			8	29
CAI	GVA			1522	296	1594	2.23	2.23	61			7	8
CAI	LON			190 4	788	1951	2.93	2.92	99			4	67
CAI	MAD			1806	1116	1816	2.27	2.27	53			2	67
CAI	PAR			1731	792	1782	2.60	2.60	64			9	29
CAI	ROM			1159	780	1348	1.78	1.78	61			4	67
CAN	농 노			1799	1237	1811	2.11	2.11	20			2	67
CAN	N S			1416	871	1426	1.82	1.82	53			8	29
SOO	풍			2180	1048	2206	3.09	3.09	62			2	29
SOO	LAX			3139	2464	3952	4.69	4.69	29			7	67
SCS	MIA			1183	663	1184	1.61	1.61	55			20	99
돐	CPH			3697	2734	4110	4.65	4.65	22			7	67
표	M			3916	2271	4125	5.25	5.25	61			7	6 7
동	SJU			1795	655	1801	2.80	2.80	99			9	29
띥	STO			3698	2487	4177	5.09	5.09	62			2	29
품	WAW			4056	2915	4469	5.11	5.11	57			8	29
CMB	DHA			2046	1008	2112	2.96	2.96	63			4	29
CMB	FRA			4352	1758	4760	6.70	6.70	2			8	29
CMB	NIS SIN			1479	926	1537	1.93	1.93	54			9	65
ᇤ	NIS SIN			2240	1077	2271	3.18	3.18	62			∞	99
뎚	<u>2</u>			3188	3464	4854	5.16	5.16	73			8	29
DFW	SJU			1872	1252	2001	2.45	2.45	26			~	29
DFW	1 0	SEA		2269	3397	5585	7.08	8.08	29			4	29
DHA	FRA			2379	936	2696	4.17	4.17	11			8	29
DHA	LON			2731	858	3002	4.76	4.76	11			∞	8
DHA	X	ris Lis		5715	3538	2962	7.40	8.40	89			4	92
DHA	PAR			2584	933	2835	4.44	4.44	92			8	67
DKR	GVA			2231	1878	2700	3.03	3.03	29			8	62

Distance (n.m.)	Distance (n.m.)	Distance (n.m.)				Time	(hou	ırs)	Percent	500 Units Daily	Load	1000 Units Daily	Load
Ö	Via GC Cruise	GC Cruise	Cruise		Pat	_	Block	Trip	subsonic	Departures	Factor	Departures	Factor
1508 1129	1129	1129	1129	•	1660		1.95	1.95	54			2	29
	1851	1851	1851	-	2583		2.83	2.83	24			4	64
3261 2278	3261 2278	2278	2278	60	3477		4.02	4.02	22			2	29
SEA 5712 3667	5712 3667	3667	3667		6138	_	7.80	8.80	71			4	6 7
SEA 5542 3397	5542 3397	3397	3397		581	2	7.52	8.52	71			80	29
2014 1245	1245	1245	1245		220	ଧ	2.85	2.85	61			8	67
BAH 6001 3450	6001 3450	3450	3450		658	Ξ	8.71	9.71	75			4	29
YYC 5030 2776	5030 2776	2776	2776		53	ဗ္ဗ	7.46	8.46	77			4	89
MIA 5153 3631	5153 3631	3631	3631		534	ဖွ	6.07	7.07	63			4	68
DKR 5163 4035	5163 4035	4035	4035		565	ល	6.20	7.20	64			4	67
BAH 5543 3435	5543 3435	3435	3435		638	<u>ლ</u>	8.35	9.35	78			4	67
3970 2909	3970 2909	2909	2909		397	4	4.18	4.18	48			8	64
GDX GUM 8901 7255	GUM 8901 7255	8901 7255	7255	•	100	8	10.70	12.70	62			9	63
1594 953	1594 953	953	953		175	2	2.34	2.34	62			9	65
GDX 5054 3592	5054 3592	3592	3592		570	o	6.81	7.81	71			4	29
2549 2107	2549 2107	2107	2107		270	2	2.75	2.75	48			8	29
1385 849	849	849	849		138	32	1.7	1.71	53			12	99
1375 820	820	820	820		13.	7	1.78	1.78	53			18	64
1734 1388	1734 1388	1388	1388		19	54	2.20	2.20	54			4	29
BAH 5663 3437	5663 3437	3437	3437		633	ស	8.26	9.26	76			4	68
1575 954	954	954	954		17	2	2.25	2.25	9			9	99
GDX 5295 3566	5295 3566	3566	3566		58	7	7.16	8.16	71			4	67
3455 2386	2386	2386	2386		36	င္ဟ	4.24	4.24	55			2	. 67
4027 3179	3179	3179	3179		402	7	3.95	3.95	45			2	67
GDX 5205 5419	5205 5419	5419	5419		127	6	8.10	9.10	81			16	9
1341	1096	1096	1096		166	LO	2.00	2.00	61			36	65
GDX 5183 5569	5183 5569	5569	5569		120	ιΣ	8.21	9.21	82			4	67
1122 870	870	870	870		14	77	1.81	1.81	64			24	.
NAN 2756 2161 27	2161	2161	2161		27	26	2.79	2.79	45			7	6 7
4320 1473	1473	1473	1473		432	Σ.	6.59	6.59	20			8	29
4029 1482	1482	1482	1482		4	32	6.04	6.04	89			2	29

	y Load	s Factor	16 61	29 9	2 67	2 67	2 67	29 9	2 67	8 67	4 67	4 68	2 67	4 67	29 9		4 67	2 67	2 67	4 68	2 67	4 64	4 67	4 68	4 67	4 A7
1000 Units	Daily	Departures	•	_										-		54						**				
	Load	Factor																								
500 Units	Daily	Departures																								
	Percent	subsonic	09	53	48	09	26	49	48	74	7	11	26	63	26	65	29	28	45	46	52	26	99	47	72	1
rs)		Trip	2.05	1.69	3.21	2.07	4.45	2.00	2.17	6.76	8.03	9.62	4.71	2.61	2.73	2.72	7.21	4.59	4.36	7.97	2.44	1.86	2.59	7.55	9.15	
Time (hours)		Block	2.05	1.69	3.21	2.07	4.42	2.00	2.17	5.76	7.03	8.62	4.71	2.61	2.73	2.72	6.21	4.59	4.36	6.97	2.44	1.86	2.59	6.55	8.15	
		Path	1432	1282	3018	1613	3820	1711	1928	5196	6072	6523	3961	1891	2298	2688	5406	3861	4527	7341	2298	1368	1942	6768	6142	
(n.m.)		Cruise	692	754	2219	926	2481	1172	1374	3663	3992	3432	2461	949	1492	2106	3388	2407	3610	9009	1728	744	1051	5455	3397	0000
Distance (n.m.)		ပ္ပ	1415	1284	3013	1433	3583	1710	1924	4170	5179	5783	3808	1773	2112	1768	4949	3557	4411	7331	2044	1362	1659	6745	5851	
		Via																								
		Via								SJU	SDX	BAH				:	DKR		٠	TYO				H	SEA	
		Dest	SEL	NIS.	SIN	TLV	XXZ	SYD	PΤΥ	띪	PAR	NIS.	STL	7[SIN	SYD	ROM	YMO	YVR	NIS.	SIN	WAS	λλΣ	YVR	WAS	
		Origin	MNL	NW WN	MRO	MUC	MUC	NAN	NAC	NAC	OSA	PAR	PAR	PAR	PER	PER	띪	ROM	SEL	SFO	SHA	SJU	SJU	SYD	TYO	?

Appendix D. HSCT Routing Table

The following table provides a list of the city paris which make up the universal HSCT route system. It also includes the waypoints (latitude, longitude) between each city-pair used to avoid supersonic flight over land. Great circle routes were flown between city pairs unless waypoint routing was necessary. If waypoints were used, great circle routes were flown between the waypoints.

Origin Deet Waypoint 1 Waypoint 2 Waypoint 3 Lat Long. Lat Long. Lat	Waypoint 1 Waypoint 2 Lat Long. Lat Long.	Waypoint 2 Long. Lat. Long.	Long.	Long.	Wayı	등교	t3 Long	Waypoint 4 Lat.	r4 Long.	Waypoint 5	15 Long.	Waypoint 6	Long	Waypoint 7	Long
									À		Ž.		Cong		Long.
LAX 1500N 10500W 2500N 11500W 3000N	10500W 2500N 11500W	2500N 11500W	11500W		3000N		11800W								
1100000 P	2002	2007		4 000 to											
2000S 15500E 10008 14200E 0700S	15500E 1000S 14200E 0700S	10008 14200E 0700S	14200E 0700S	07008			12000E								
NAN OSA															
25000	20001	9000													
2000\$ 15500E	15500E 3500S	20002		11300E											
SIN 20008 15500E 1000S 14200E 0700S	15500E 1000\$ 14200E	1000\$ 14200E	14200E		07008		12000F	27050	100001						
) ! !										
OYT															
ATL 5100N 00900W 3226N 07823W	00900W 3226N	3226N	_	07823W											
4530N 01221E 4000N 01900E 3720N	01221E 4000N 01900E 3720N	4000N 01900E 3720N	01900E 3720N	3720N		0	01947E	3425N	02400E	31 10N	03325E	2845N	34405		
1 5100N 00900W 4700N 05000W 4108N	00900W 4700N 05000W 4108N	4700N 05000W 4108N	05000W 4108N	4108N	-	0	W00790								
3720N	01221E 4000N 01900E 3720N	4000N 01900E 3720N	01900E 3720N	3720N	_	Ö	01947E	3425N	02400F						
1 6100N 00900W	W00600						1								
5100N 00900W 4700N 05000W 4108N	00900W 4700N 05000W 4108N	4700N 05000W 4108N	05000W 4108N	4108N		8	W00790								
5100N 00900W 3226N 07623W	00900W 3226N 07823W	3226N 07823W	07823W												
5100N	00900W 4200N	4200N		01700W											
5100N 00900W	00900W 4700N 05000W	4700N 05000W	05000W		4108N		06700W								
_	00300E 7200N 02500E	7200N 02500E	02500E		7200N		13230E								
	_	W00800													
6000N 00500W	00500W 5800N 04500W	5800N 04500W	04500W		6100N		06500W	6200N	W00070	6300N	07500W	8230N	Wood of		
5100N 00900W	00900W 4700N 05000W	4700N 05000W	05000W		4108N		06700W						***************************************		
4530N 01221E	01221E 4000N 01900E	4000N 01900E	01900E		3720N		01947E	3425N	02400E						
5100N 00900W	N0044 W00600	4700N		05000W											
_	00900W 4700N 05000W	4700N 05000W	W00050		4108N		W00780								
YVR 6000N 00500W 5800N 04500W 6100N	00500W 5800N 04500W	5800N 04500W	04500W		6100N		06500W	6200N	W00070	6300N	07500W	ROSCA	77,000,00		
6000N 00500W 5800N 04500W 6100N	00500W 5800N 04500W 6100N	5800N 04500W 6100N	04500W 6100N	6100N	_	_	06500W	8200N	W00070	A300N	07500W		M00000		
5100N 00900W 4700N 05000W 4108N	00900W 4700N 05000W 4108N	4700N 05000W 4106N	05000W 4108N	4108N		_	06700W				40067		Moooo		
16500W 3500N 14200E 2000N	16500W 3500N 14200E 2000N	SECON 14200E SOOM	14200E 2000M	Noon		•	SEONE								
5730N 16500W 3700N 14700F	16500W 3700N 14700F	3700N 14700F	14700E												
8500N 01000W 6230M	01000W 6230W 00300F	ADSON ODSON	ON SOOF		K700M		100000								
5000N 13500W	13500W	10000				•	10000								
5730N	16500W 3330N	3330N		14000F											
				*											

	Long.																																						
Waypoint 7	Let.																																						
	Long.																			01221E			01221E			01221E											W00080		
Waypoint 6	Lat																			4530N			4530N			4530N											6230N		
	Long.																			01900E			01900E			01900E											07500W		
Waypoint 5	Lat																			4000N			4000N			4000N											6300N		
-	Long.		W00790													•		10800E		01947E	10800E		01947E	01200E	10800E	01947E	10200E		02400E						02400E		M00070		
Waypoint 4	Lat.		4106N															N0080		3720N	N0080		3720N	3700N	N0080	3720N	0200N		3425N						3425N		6200N		
13	Long.		0500W															09700E		02400E	09700E		02400E	02400E	09700E	02400E	09700E	06700W	01947E	06700W				W00780	01947E	W00780	06500W	06700W	07200E
Waypoint 3	בּ		4600N															0610N		3425N	0610N		3425N	3425N	0610N	3425N	0610N	4108N	3720N	4108N				4106N	3720N	4106N	6100N	4106N	1730N
12	Long.	14700E	W00800	W00900	W00890	W00900	W00900		W00680	M00600		W00900	W00800			05000W	08000E	08000E	07500E	03325E	08000E	08000E	03325E	03325E	08000E	03325E	300080	05000W	01900E	05000W	07823W	02000W		05000W	01900E	05000W	04500W	05000W	07500E
Waypoint 2	Lat	3700N	4600N	4800N	1730N	4800N	4800N		0500S	5100N		4800N	4800N			4700N	0500N	0500N	0730N	3110N	0500N	0500N	3110N	3110N	0500N	3110N	0500N	4700N	4000N	4700N	3226N	2000N		4700N	4000N	4700N	P800N	4700N	1000T
=	Long.	16500W	00043W	07823W	07823W	07823W	07823W		W00870	07823W	07823W	07823W	07823W		07623W	07823W	05740E	05740E	05740E	03440E	05740E	06740E	03440E	03440E	05740E	03440E	05740E	W00900	01221E	M00600	M00600	01700W	W00800	W00600	01221E	M00600	M00500	W00000	0000E
Waypoint 1	3	5730N	4450N	3226N	3226N	3226N	3226N		2800N	3226N	3226N	3226N	3226N		3226N	3226N	1930N	1930N	1930N	2845N	1930N	1930N	2845N	2845N	1930N	2845N	1930N	5100N	4530N	5100N	5100N	4200N	4800N	5100N	4530N	5100N	N0009	5100N	0500N
Dest		70	N	BER	SCS	FRA	QVA	Ħ	Z	LON	MAD	MUC	PAR	SEA	S	SNR	BKK	CAN	CMB	٩٨	HKG	JKT	PO	1	Z Z	PAR	Z S	BOS	₹ S	ᇙ	DFW	DKR	M	NYC	7	WAS	Χ	XX	BOM
Origin		ANC	ATH	AП	AП	ATL	ATL	ATL	ATL	AП	AH	ATL	ATL	ATL	ATL	AП	ВАН	D BAH	ا BAH	ВАН	ВАН	BAH	ВАН	ВАН	ВАН	ВАН	ВАН	BER	BEH	BER	BER	BER	BER	BER	BER	BEA	BER	BER	BKK

Long- Lat. Lat. Long- Lat. La	•	;											:			
CAM GROWN GROONE 1930M G5746E 7130M G720E 1730M G730E 1730M G730M HALE 1730M G730E 1730M G730E 1730M G730E 1730M G730E 1730M G			1	Long.	3	Long.	Ę	Long.	Let		3		Lat.	Long.	, i	Long.
CAM 0500M 06000E 193M 05740E 2445M 02440E 193M 05740E 193M 05740E 193M 05740E 193M 05740E 193M 05740E 193M 19500E 0600M 0600E 0610M 06740E 0705M 19500E 0600M 07050E 0705M 19500E 0705M 19500E 0705M 19500E 0705M 19500E 0705M 19500E 0705M 19500E 0705M 0705M 19500E 0705M 07																
MAIL 0700H 10500E	8 K	₹ 8	200Y	08000E	1930N	05740E	2845N	03440E								
Milk	۲ ا															
KH G600M 19800E 1000M 19800E 1730M	8	¥	0000 0000	0000E	1930N	05740E										
MAL 0700M 19500E 0900M 19500E 1730M 0720E 1730M 0720E 1730M 0720E 1730M 0720E 1730M 19500E 19000B 19000E 19000B	EK X	벌	N0070	10500E												
Mile 0700H 10500E 0000H 10000E 3300H 13700E 3300H 13700H 137	BKK	Ī	N0050	0000E	1000F	07500E	1730N	07200E								
PGR GATON 10800E 10900 11900E 3300N 12500E 3100NE 310NE 3100NE	BKK	Z	0700N	10500E	N0090	10900E								•		
PCM 1900te 1900	BKK	VSO	M0010	10500E	N0090	10800E	3300N	13700								
SEL 1700M 10800E 0000M 10800E 3000M 12600E 3500M 12600E 3720M 01847E 4000M 018447E 4000M 0184447E 4000M 0184447E 4000M 0184447E 4000M 0184447E 4000M 0184447E 4000M 0184447E 4000M 4000M 4000M 4000M 4000M 4000M 4000M 4000M 4000M	BKK	E	N00%	1040E	10008	11000E	30008	11000E								
SEL 0700M 10800E 0800M 10800E 3000M 12500E 3800M 12500E 3800M 12500E 3800M 12500E 3800M 12500E 3800M 12500E 3700M 13700E 3800M 12500E 3700M 01947E 4000M 01900E MAD MAD 1700M 01700M 01700M 1000M 01900E 3110M 03325E 345M 02400E 3720M 01947E 4000M 01900E MAD 1730M 05720E 2348M 0340E 3110M 03325E 342M 02400E 3720M 01947E 4000M 01900E MAD 1730M 05720E 2348M 0340E 3110M 03325E 342M 02400E 3720M 01900E MAD 1730M 05720E 2346B 0340E 3110M 03325E 342M 02400E 3720M 01947E 4000M 01900E BRI 1730M 05700W 4100M 0500W 510M 0500	BKK	<u>S</u>	82000	10900E	07008	12000F	1000	14200E								
TYO OTOON 10800E 3000N 13700E 3300N 1370N 3325E 3425N 02400E 3720N 01947E 4000N 01900E 3425N 02400E 3720N 01947E 4000N 01947E 4000N 01940E 3720N 01947E 4000N 01940E 3720N 01947E 4000N 02940M 4108N 02940M 4108N 02940M 4108N 03940M 4108N	8KK	SEL	0700N	10500E	N0090	1080E	3000N	12500F	MOORE	TORONE						
HAZ	BKK	7	0700N	10500E	N0090	1000E	3300N	13700E								
MAD	B 00	FRA	4200N	01700W												
NYC 2800N 07800W	Bog	MAD														
NYC 2900N 07500W C400E 3110N 03325E 3425N 02400E 3720N 01947E 4000N 01900E GVA 1930N 05740E 20440E 3110N 03325E 3425N 02400E 3720N 01947E 4000N 01900E HKG 1730N 0720E 1000N 0750E 2050N 00325E 3425N 02400E 3720N 01947E 4000N 01900E LCN 1930N 05740E 2040E 3110N 0332E 3425N 02400E 3720N 01947E 4000N 01900E SIN 1730N 0570W 4700N 0500W 5100N 0990W 3720N 01947E 4000N 01900E BRU 4108N 0500W 4108N 0500W 5100N 0990W 5100N 0990W 10200E 3720N 01947E 4000N 01900E BRU 4108N 0500W 4100N 0500W 5100N 0990W 5100N 0990W	Bog	¥														
FRA 1930N 06740E 2845N 0340E 3110N 03325E 3425N 02400E 3720N 01947E 4000N 01900E QVA 1930N 05740E 2845N 0340E 3110N 03325E 3425N 02400E 3720N 01947E 4000N 01900E LON 1830N 05740E 2845N 0340E 3110N 03325E 3425N 02400E 3720N 01947E 4000N 01900E RN 1730N 05700E 2845N 0340E 3110N 03325E 3425N 02400E 3720N 01947E 4000N 01900E SIN 1730N 05700W 4700N 05000W 5100N 0900W 5100N 0900W 10200E 3720N 01900E 01900E 0500N	B 00	X	2600N	07600W												
GVA 1930N 65740E 2845N 03440E 3110N 03325E 3425N 02400E 3720N 01947E 4000N 01900E HKQ 1730N 05740E 2845N 03440E 3110N 03325E 3425N 02400E 0400N 01900E LON 1930N 05740E 2845N 03440E 3110N 03325E 3425N 02400E 4000N 01900E LON 1730N 05740E 2845N 03440E 3110N 03325E 3425N 02400E 4000N 01900E BRU 4106N 05740E 2800N 5100N 05900W 4000N 10200E 4000N 01900E FRA 4106N 05700W 4700N 05000W 5100N 00900W 4000N 10200E 4000N 01900E LON 4106N 06700W 4700N 05000W 4106N 05000W 4106N 0500W 4106N 0500W 4106N 0500W 4106N 0500W 4106	BOM	FRA	1930N	05740E	2845N	03440E	3110N	03325E	3425N	02400F	3720N	01947E	NOON	300010	463081	110010
HKG 1730N 07200E 1000N 07500E 0500N 06000E 0610N 09700E 0800N 10500E 0750N 09500E 0750N 09500E 0750N 0950N 0	BOM	QVA	1930N	05740E	2845N	03440E	3110N	03325E	3425N	02400E	3720N	019476	4000N	1900	4550K	012215
LON 1930N 05740E 2845N 03440E 3110N 03325E 3425N 02400E 3720N 01947E 4000N 01900E 8N 1730N 05740E 2845N 03440E 3110N 03325E 3425N 02400E 3720N 01947E 4000N 01900E 8N 1730N 05700W 4700N 05000W 5100N 00900W	BOM	HKG	1730N	07200E	1000N	07500E	0500N	0000E	N0190	09700F	Noceo	1080F				01221E
PAR 1930N 05740E 2845N 03440E 3110N 03325E 3425N 02400E 3720N 01947E 4000N 01900E BRU 4106N 06700W 4700N 05000W 5100N 06900W 10200E 0510N 06900W 10200E 0500N 10200E 0500N 10200E 0510N 06900W 10200E 0500N	BOM	LON	1930N	05740E	2845N	03440E	3110N	03325E	3425N	02400E	3720N	01947E	4000N	1900E	ARRON	01221E
SIN 1730N 07200E 1000N 07500E 0500N 0600E 0610N 09700E 0200N 10200E BRU 4106N 06700W 4700N 65000W 5100N 00900W 10200E 0200N 10200E GVA 4106N 06700W 4700N 65000W 5100N 00900W 10200E 10200E LON 4106N 06700W 4700N 65000W 5100N 00900W 10200E 10	BOM	PAR	1930N	05740E	2845N	03440E	3110N	03325E	3425N	02400E	3720N	01947E	4000N	01900E	4530N	012216
BRU 4106N 06700W 4700N 65000W 5100N 06900W GVA 4106N 06700W 4700N 65000W 5100N 00900W GVA 4106N 06700W 4700N 65000W 5100N 00900W LON 4106N 06700W 4700N 06000W 5100N 00900W MIA 3820N 06700W 4800N 00600W 5100N 00900W PAR 4106N 06700W 4700N 06000W 4106N 06700W SJU SNN 4106N 4700N 05000W 4106N 06700W GH 5100N 01700W 4700N 05000W 4106N 06700W MX 5100N 01221E 4000N 01900E 7200N 4106N 06700W MAS 5100N 00900W 4700N 05000W 4106N 06700W MAS 5100N 00900W 4700N 05000W 4106N 06700W	BOM	NIS NIS	1730N	07200E	1000L	07500E	0500N	08000E	0610N	09700E	0200N	10200E				7 1 7 1 L
FRA 4106N 06700W 4700N 05000W 5100N 00900W GVA 4106N 06700W 4500N 06500W 5100N 00900W LON 4106N 06700W 4700N 06000W 5100N 00900W MIA 3820N 06700W 4800N 06600W 5100N 00900W PAR 4106N 06700W 4700N 06600W 4106N 06700W SJU SIN 4106N 06700W 4700N 05000W 4106N 06700W CH 5100N 00900W 4700N 02000W 4106N 06700W DKR 4200N 01720W 4700N 02000W 4106N 06700W MYC 5100N 00900W 4700N 0190E 3720N 01947E 3426N WAS 5100N 00900W 4700N 0500W 4106N 06700W VMQ 5100N 00900W 4700N 05000W 4106N 06700W	BOS	BRC	4106N	W00780	4700N	05000W	5100N	W00600								
GVA 4106N 06700W 4500N 06600W 5100N 00900W LON 4106N 06700W 4700N 66000W 5100N 00900W MIA 3620N 06700W 4800N 06600W 5100N 00900W PAR 4106N 06700W 4700N 65000W 4106N 06700W SJU SNN 4106N 06700W 4700N 65000W 4106N 06700W CH 6100N 00900W 4700N 02600W 4106N 06700W DKR 4200N 01720W 4700N 65000W 4106N 06700W TLV 4630N 01221E 4000N 0190E 720N 01947E 3426N WAS 6100N 01221E 4000N 0190E 3720N 01947E 3426N VMQ 5100N 00900W 4700N 65000W 4106N 06700W VMQ 5100N 00900W 4700N 65000W 4106N 06700W	Bos	FRA	4106N	W00780	4700N	05000W	5100N	W00900								
LON 4106N 06700W 4700N 05000W 5100N 00900W MIA 3820N 06857W 4800N 06600W PAR 4106N 06700W 4800N 05000W SJU SNN 4106N 06700W 4700N 05000W CH 5100N 00900W 4700N 02000W DKR 4200N 01700W 2000N 02000W TLV 4530N 01221E 4000N 01900E 3720N 113230E NYC 5100N 00900W 4700N 05000W TLV 4530N 01221E 4000N 01900E 3720N 01947E 3425N WAS 5100N 00900W 4700N 05000W 4106N 06700W VMA 5100N 00900W 4700N 05000W 4106N 06700W DKR 3600S 06200W 2000S 03500W	Bos	٩٨	4106N	06700W	4800N	00600W										
MIA 3820N 06957W PAR 4106N 06700W 4800N 06600W ROM 4106N 06700W 4700N 06600W SJU SU 4700N 4700N 65000W CH 6100N 00900W 4700N 62000W DKR 4200N 01700W 2000N 4106N 06700W MYC 6100N 00900W 4700N 6500W 4106N 66700W TLV 4530N 01221E 4000N 0190E 3720N 01947E 3426N WAS 6100N 00900W 4700N 65000W 4106N 66700W VMQ 6100N 00900W 4700N 65000W 4106N 66700W VMQ 6100N 00900W 4700N 65000W 4106N 66700W	BOS	NO Po	4106N	06700W	4700N	05000W	5100N	M00600					÷			
PAR 4106N 06700W 4800N 06600W ROM 4106N 06700W 4700N 06600W SJU SU 4700N 4700N 65000W 4106N 06700W CH 6100N 00900W 4700N 02000W 4106N 06700W DKR 4200N 01700W 2000N 4700N 6500W 4106N 06700W MYC 6100N 00900W 4700N 01900E 720N 13230E 720N MAS 6100N 01221E 4000N 0190E 372N 01947E 3426N VMQ 6100N 00900W 4700N 05000W 4106N 06700W VMQ 6100N 00900W 4700N 05000W 4106N 06700W DKR 3600S 06200W 4106N 06700W 06700W	B 08	¥	3820N	06957W												
ROM 410eN 06700W SJU SNN 410eN 06700W 4700N 05000W 410eN 06700W CH 6100N 09900W 4700N 05000W 410eN 06700W DKR 4200N 01700W 2000N 4700N 02000W 410eN 06700W MYC 6100N 00900W 4700N 01900E 720N 13230E MAS 6100N 01221E 4000N 01900E 3720N 01947E 3426N VMQ 6100N 00900W 4700N 05000W 410eN 06700W VMQ 6100N 00900W 4700N 05000W 410eN 06700W DKR 3600S 06200W 4700N 05000W 410eN 06700W	BOS	PAR	4106N	W00780	48 00 N	W00900										
SJU SNN 4108N 06700W 4700N 05000W CH 6100N 00900W 4700N 05000W 4108N 06700W DKR 4200N 01700W 2000N 02000W QDX 6230N 00300E 7200N 7200N 13230E NYC 6100N 00900W 4700N 05000W 4108N 06700W TLV 4530N 01221E 4000N 01900E 3720N 01947E 3425N WAS 6100N 00900W 4700N 05000W 4108N 06700W VMQ 6100N 00900W 4700N 05000W 4108N 06700W DKR 3600S 06200W 2000S 03500W	808	HOM	410ex	06700W												
SNN 4106N 06700W 4700N 06000W CHI 6100N 00900W 4700N 05000W 4106N 06700W DKR 4200N 01700W 2000N 02000W 4106N 06700W QDX 6230N 00300E 7200N 13230E 720N 13230E NYC 6100N 00900W 4700N 01900E 3720N 01947E 3426N WAS 6100N 00900W 4700N 05000W 4106N 06700W VMQ 6100N 00900W 4700N 05000W 4106N 06700W DKR 3600S 06200W 2000G 05000W 4106N 06700W	BOS	2														
CH 6100N 00900W 4700N 05000W 4106N 06700W DKR 4200N 01700W 2000N 02000W 4106N 06700W GDX 6230N 00300E 7200N 02500E 7200N 13230E NYC 5100N 00900W 4700N 01900E 3720N 01947E 3425N WAS 5100N 00900W 4700N 05000W 4106N 06700W YMQ 5100N 00900W 4700N 05000W 4106N 06700W DKR 3600S 06200W 2000S 03500W 4106N 06700W	BOS	N N N	4106N	W00780	4700N	05000W										
DKR 4200N 01700W 2000N 02000W QDX 6230N 0030GE 7200N 0250GE 7200N 13230E NYC 5100N 00900W 4700N 01900E 3720N 01947E 3425N TLV 4530N 01221E 4000N 4700N 05000W 4106N 06700W VMQ 5100N 00900W 4700N 05000W 4106N 06700W DKR 3600S 05200W 2000S 03500W		Ŧ	5100N	M00600	4700N		4108N	06700W								
QDX 6230N 00300E 7200N 02500E 7200N 13230E NYC 5100N 00900W 4700N 05000W 4108N 06700W TLV 4530N 01221E 4000N 01900E 3720N 01947E 3425N WAS 5100N 00900W 4700N 05000W 4108N 06700W VMQ 5100N 00900W 4700N 05000W 4108N 06700W DKR 3600S 05200W 2000S 03500W 4108N 06700W	BRC	DKA R	4200N	01700W	2000N											
NYC 5100N 00900W 4700N 05000W 4108N 06700W TLV 4630N 01221E 4000N 01900E 3720N 01947E 3425N WAS 5100N 00900W 4700N 05000W 4106N 06700W YMQ 5100N 00900W 4700N 05000W 4106N 06700W DKR 3600S 06200W 2000S 03500W	BRU	S	6230N	00300E	7200N		7200N	13230E								
TLV 4530N 01221E 4000N 01900E 3720N 01947E 3425N WAS 5100N 00900W 4700N 05000W 4106N 06700W YMQ 5100N 00900W 4700N 05000W 4106N 06700W DKR 3600S 05200W 2000S 03500W	BRC	X	5100N	W00900	4700N		4108N	W00290								
WAS 5100N 00900W 4700N 05000W 4106N 06700W YMQ 5100N 00900W 4700N 05000W 4106N 06700W DKR 3600S 05200W 2000S 03500W	BRC	۲	4530N	01221E	4000¥		3720N	01947E		02400E						
YMQ 5100N 00900W 4700N 05000W 4106N DKR 3600S 05200W 2000S 03500W	BRU	WAS	5100N	M00600	4700N		4108N	W00780		!						
DKR 3600S 05200W 2000S 03500W	BRU	Y.	5100N	W00000	4700N		410eN	W00290								
	BUE	DKA	36008	06200W	20008	03500W) } !								

	Ł	ŀ													
		Waypoint 1		Waypoint 2		Waypoint 3		Waypoint 4		Waypoint 5		Waypoint 6		Waypoint 7	
			Long.	ž	Long.	Lat	Long.	2	Long.	Let	Long.	Lat	Long.	Lat	Long.
;															
₹ C	FRA	3425N	02400E	3720N	01947E	4000N	01900E	4530N	01221E						
S	۵۸	3425N	02400E	3720N	01947E	4000N	01900E	4530N	01221E						
CA	NO P	3425N	02400E	3720N	01947E	4000N	01900E	4530N	01221E						
S	MAD	3425N	02400E	3700N	01200E										
S	N	3425N	02400E	4108N	W00790										
Š	PAR	3425N	02400E	3720N	01947E	4000N	01900E	4530N	01221E						
Š	ROM	3425N	02400E	3700N	01200E										
CAN	JKT	N0080	10800E												
CAN	NIS.	N0080	10800E												
CAN	<u>5</u>	2000N	12500E												
SCS	풄	1730N	W00890	3226N	07823W										
S	FRA	4200N	01700W												
SOO	ž	1130N	07000W	1036N	07928W	0847N	07934W	N0630	W00080	1500N	10500W	2500N	11500W	3000N	11800W
S	SI I														
SOO	LON	4800N	W00000												
SOO	MAD														
SOO	¥														
S	¥														
SSS	N	1730N	W00800	3820N	06957W										
SOO	PAR	4800N	W00900												
S	ROM														
품	CPH	4108N	W00780	4700N	05000W	N0009	00500W								
동	FRA	4108N	W00780	4700N	05000W	5100N	W00000								
Ξ	ΔVD	4108N	W00780	4800N	W00900										
품	Ĭ														
돐	LON	4108N	W00780	4700N	05000W	5100N	W00900								
돐	Ę	4106N	06700W												
돐	MCC	4106N	06700W	4700N	05000W	5100N	W00000								
동	PAR	4106N	06700W	4800N	M00900										
₹	ROM	4106N	W00780												
₹	SEA														
₹	S														
풄	810	4106N	W00780	4700N	05000W										
돐	WAW	4106N	W00780	4700N	05000W	N0009	00500W								
CMB	ĕ	0730N	07500E	1930N	05740E										
CMB	FRA	0730N	07500E	2845N	03440E	3110N	03325E	3425N	02400E	3720N	01947E	4000N	01900E	4530N	01221E
CMB	PAR	0730N	07500E	2845N	03440E	3110N	03325E	3425N	02400E	3720N	01947E	4000N	01900E	4530N	01221E
CMB	NIS.	06 10N	09700E	0200N	10200E										

Origin	- - - -	Waypoint 1		Waypoint 2	2	Waypoint 3	9	Waypoint 4	14	Waypoint 5	15	Waypoint 6	•	Waypoint 7	
		1	Long.	F.	Long.	3	Long.	Let	Long.	Ę	Long.	Lat	Long.	Ę	Long.
PH H	NAC	N 0009	W0000	4700N	05000W	4108N	W00Z90								
H	SEA	N0009	W00500	5800N	04500W	6100N	06500W	8200N	W0000	NOORA	07500W	MOSCA	Woode		
CVG	FRA	4106N	W00700	4700N	05000W	5100N	W00900								
CVG	LON	4106N	W00790	4700N	05000W	5100N	W00900								
떈	N N	06 10N	09700E	0200N	10200E										
DEL.	<u>2</u>	0610N	09700E	N0090	10800E	3300N	13700E								
DFW	FRA	3226N	07823W	5100N	W00600										
DFW	Ĭ														
DFW	PO	3226N	07623W	5100N	W00600										
DFW	MAD	3226N	07823W												
DFW	PAR	3226N	07623W	4800N	W00900										
DFW	SEA														
DFW	3	2900N	W00500	2400N	06230W	2350N	W00080	2350N	07500W						
DHA	FRA	2845N	03440E	3110N	03325E	3425N	02400E	3720N	01947E	4000N	01900E	4530N	01221E		
₽ H	JK1	1930N	05740E	0500N	3000 9 0										
DHA DHA	EIS	3110N	03325E	3425N	02400E	3730N	01200E	3830N	00730E						
AH DHA	NO Po	2845N	03440E	3110N	03325E	3425N	02400E	3720N	01947E	4000N	01900E	4530N	01221E		
DHA	M	1930N	05740E	0500N	3000e0	0610N	09700E	N0090	10800E						
OHA DHA	PAR	2845N	03440E	3110N	03325E	3425N	02400E	3720N	01947E	4000N	01900E	4530N	01221E		
DHA	Z S	1930N	05740E	0500N	0000E	0610N	09700E	0200N	10200E						
DKA DKA	V	2000N	02000W	4200N	01700W				•						
DKA	HAV														
DKR	왕	2000N	02000W	2700N	02000W										
DKR	NO.	2000N	02000W	4200N	01700W										
DKR	MAD	2000X	02000W	3000N	01800W	3701N	00756W								
DKA	NYC														
DKR	PAR	2000N	02000W	4200N	01700W										
DKR	잁	2000S	03500W												
DKR	ROM	2000N	02000W	3000K	01900W	3701N	00756W								
¥TQ	FRA	410eN	W00780	4700N	05000W	5100N	M00600								
₩ IQ	LON	4106N	W00780	4700N	05000W	5100N	W00600								
₩LQ	PAR	4106N	W00780	4700N	W00030	5100N	W00600								
₩ LQ	SEA		,												
70F	FRA	4000N	W00900												
흕	NO Po	5100N	M00600												
듄	MAD														
70.	PAR	4800N	W00000												
Ë	X	410en	06700W												

Origin	Dest	Waypoint 1	11	Waypoint 2	12	Wavpoint 3	E.	Wavnoint 4		Wavnoint	2	Wevnoint		Wavnoint 7	
		=	Long.	.	Long.	נ ב	Long.	Lat	Long.	Let	Long.	Lat	Long.	Let	Long.
İ	;														
FRA	BAH	4530N	01221E	4000	01900E	3720N	01947E	3425N	02400E	3110N	03325E	2845N	03440E		
FRA	DKR R	4200N	01700W	2000N	02000W					•					
FRA	QD X	6219N	00447E	6230N	00300E	7200N	02500E	7200N	13230E						
FRA	ᅙ	4800N	W00900	3226N	07823W										
FRA	¥ ¥	4800N	W00800												
FRA	A	5100N	W00600	4700N	05000W	4108N	W00790								
FRA	풀	S100N	W00600	4700N	05000W	4108N	06700W								
FRA	망	4800N	W00900												
FRA	ገ.	4530N	01221E	4000A	01900E	3720N	01947E	3425N	02400E						
FRA	WAS	5100N	W00600	4700N	05000W	4108N	06700W								
FRA	YMO	5100N	W00600	4700N	W00080	4108N	W00790								
FRA	χ	00009	W00300	200N	04500W	6100N	06500W	6200N	07000W	6300N	07500W	6230N	W0000		
FRA	¥Ç	N0009	00500W	2800N	04500W	6100N	06500W	6200N	07000W	6300N	07500W	6230N	W0000		
FRA	7,42	5100N	M00600	4700N	05000W	4108N	06700W								
αDΧ	GUM														
XQ5	N O	7200N	13230E	7200N	02500E	6230N	00300E								
OD ,	NE NE	3700N	14700E	3500N	14200E										
χQυ	OSA	3700N	14700E	3400N	14100E										
aDX	PAR	7200N	13230E	7200N	02500E	6230N	00300E								
αDX	<u>ک</u>	3700N	14700E												
₩0°	αDX														
BOB	¥	•													
BUN	JKT	0300N	12200E	N0000	11830E	0500S	11700E								
™ O	Z														
B OM	OSA														
M OD	SEL	3000K	12500E	3500N	12500E										
8 00	SYD	05008	15400E	20002	15500E	32308	15400E								
B OB	<u></u>														
۵VA	ВАН	4530N	01221E	4000N	01900E	3720N	01947E	3425N	02400E	3110N	03325E	2845N	03440E		
۵VA	XQD.	5219N	00447E	6230N	00300E	7200N	02500E	7200N	13230E						
۵VA	NAC	4800N	W00900	4106N	06700W										
۵VA	7	4530N	01221E	4000 1	01900E	3720N	01947E	3425N	02400E						
۵VA	YNO	4700N	05000W	4106N	06700W										
۵۸	λλΣ	5100N	M00600	4700N	05000W	4106N	06700W								
HAV	MAD														
표	N	4100N	05000W	4106N	W00780										
HKG	aDX	2000N	12500E	3500N	14200E	3700N	14700E								
HKG	Į,	2200N	12230E												

Origin		Waypoint 1		Waypoint 2	12	Wavpoint 3	62	Wavecint 4	1	Wesmolnt		Monte		Manager 1	
		בּ	Long.	: 3	Long.	į	Long.		Long	Let		maypom.	-	waypoint /	566
											i				i i
HKG	K	N0090	10800E												
HKG	필	2000N	12200E	80680	14700E	10005	15200E	20008	15500F	SEARS	TREATE	30202	164000		
HKG	V SO	2000N	12500E								10000	200			
HKG	E	N0080	100001	10008	11000E	30008	11000E								
HKG	SEL	2200N	12230E												
HKG	NIS S	N0090	1000E												
HKG	SYD	2000N	12200E	9308	14700E	10005	15200E	20005	15500F	25008	15 EAST	20200	164000		
HKG	<u>6</u>	2000N	12500E					}			3000	35.303	1040		
H	BON														
¥	9 9														
H	Š														
¥	MEL	2500S	16500E												
HNH	Z Z										,				
Ĭ	NAN														
HNL	N														
Ä	OSA	3400N	141005												
	<u>.</u>														
i Ž D-	SEA														
	8	3000N	13000F	ACOUNT.	12EAR										
¥	SFO														
H	SП														
¥	SYD	2500S	16500E												
Ĭ	TPE														
Ĭ	7														
ĭ	¥											-			
₹	742														
¥	NO P	3226N	07823W	5100N	W00900										
₽	PAR	3226N	07823W	4800N	W00000										
오	SEA														
POF	3	2400N	08230W	2350N	W00080	2350N	07500W								
JKT	ÆF	0700S	12000E	10008	14200E		15500E	25008	15500F	30306	15 ANDE				
JK1	Z	N0090	10800E								1016				
JKT	V80	N0090	10800E	3300N	13700E										
JKT	Æ	N0090	10000E	3000N	12300E	3800N	12300E	NOCOL	11000						
LK1	SEL	N0090	10000E	3000N	12500		125005								
K	SYD	0000	12000E	10008	14200F		15500E	25000	1000						
JK1	핕	N0080	100001	}	1		10000E		3000	32302	15400E				
JKT	0,1	0000N	10800	NOOSE	19700E										
	J •	; ; ;		•	1 2 2										

Orlain		Dest. Wavpoint 1	-	Wavpoint 2	12	Wavboint 3		Wavecint 4	Į	Wevnoint	2	Wavnoint		Wavpoint 7	
•		Let	Long.	Let	Long.	į	Long.	ž	Long.	Ę	Long.	L at	Long.	į	Long.
İ															
BNS	DKA	2600S	01500E	1400N	02100W										
a S	MRC	2800S	04800E												
e N	PER														
SNS SNS	3														
SNB	NIS.	28008	04800E												
ž	ACA	3000N	11800W	2500N	11500W	1500N	10500W								
ž	Ĭ														
ž	LON LON	6230N	W00080	6300N	07500W	6200N	W00070	6100N	W00590	S800N	04500W	5100N	W00600		
ž	MEX	3000k	11800W	2000N	11000W										
ž	X														
Š	OSA	3400N	14100E												
Š	PPT														
ž	70														
3	MEX	1500N	W00760												
3	A	05008	08300W												
	2	9666	W0000	140016	Moore										
	2 2	50550	M00690	atone v	A 200 /0										
		2000	A COSSO												
	S K K														
SI.	8	3000N	01800W	0730S	03200W	2000S	03500W								
S C	BAH	4530N	01221E	4000N	01900E	3720N	01947E	3425N	02400E	3110N	03325E	2845N	03440E		
S C	OKA	4200N	01700W	2000N	02000W										
PO	QDX	6230N	00300E	7200N	02500E	7200N	13230E								
LON	¥	5100N	M00600												
LON	MSP	5100N	M00600	2800N	04500W	6100N	06500W	6200N	W00070	8300N	07500W	6230N	W00080		
LON	NAC	5100N	W00600	4700N	05000W	4108N	W00790								
LON	롶	5100N	M00600	4700N	05000W	4108N	W00780								
PO	SEA	5100N	M00600	2800N	04500W	9100N	06500W	6200N	W000T0	8300N	07500W	6230N	W00080		
PO	SFO	5100N	M00600	2800N	04500W	6100N	06500W	6200N	W00070	9 300N	07500W	6230N	W00080		
PO	3	5100N	W00000												
LON	ST	5100N	M00600	4700N	05000W	4108N	06700W								
LON	7	4530N	01221E	4000N	01900E	3720N	01947E	3425N	02400E						
LON	WAS	5100N	M00600	4700N	05000W	4108N	06700W				٠				
LON	YHZ	5100N	M00800	4700N	W00030										
LON	YMQ	5100N	W00600	4700N	05000W	4108N	W00780								
LON	Y	5100N	M00600	2600N	04500W	6100N	06500W	6200N	W00070	8300N	07500W	6230N	W00080		
LON	X	5100N	M00600	2600N	04500W	6100N	06500W	6200N	W00070	8300N	07500W	6230N	W00080		
LON	7,42	5100N	M00600	4700N	05000W	4108N	06700W								
MAD	¥														

Origin	Deet	Waypoint 1	11.1	Wayboint 2	12	Wavpoint 3	13	Westernam	1	Weigner		A salesmon		West	
1		.	Long	-		•				waypour.		a maypoint o		waypoint /	•
			· Russ		- County		Long	L'AI.	Long.	ב ב	Long.	Lat	Long.	Į.	Long.
MAD	NAC	4108N	Worth												
MAD	2	3701N	00756W	2700N	WOODO	20008	W CO								
MAD	٦,	3700N	01200E	3425N	02400E										
MAD	WAS	4108N	W00780												
MAD	ANO.	4106N	W00290												
MEL	Ĭ	2500S	16500E												
ME	Z		!												
Ę	VS 0	3230S	15400E	25008	15500E	20003	15500F	05008	15400E						
MEL	PER	35008	11300E												
MEL	Ā														
MEL	Z	32308	15400E	25008	15500E	2000S	15500E	10005	142005	20020	10000	- ST060	10000		
MEL	<u></u>	32308	15400E	25008	15500E	20002	15500E	05005	15400F	3	3007		3000		
MEX	¥				•										
MEX	NAC	2400N	06230W	2350N	W00080	2350N	07500W								
MEX	F	1500N	W00760	N0670	08230W										
_	SFO	2000N	11000W	3356N	12200W										
_	WAS	2400N	08230W	2350N	W00080	2350N	07500W	3800N	07500W						
¥ 1(MEX														
¥ M V	MSC C	4800N	W00900												
¥	PAR	4800N	W00900												
¥	PPT														
¥	잁	2600N	07600W	2000	W00080	0730S	03200W	20008	03500W						
¥	ROM														
Y	ಶ	02003	08300W												
=	DKA	3701N	00756W	3000K	01800W	2000N	02000W								
=	N	4500N	W00800	4108N	06700W										
ĭ	WAS	4600N	W00800	4108N	06700W										
Į	VSO														
Ĭ	PEX	2000N	12200E	3000K	12300E	3800N	12300E	3900N	11800E						
Z Z	SEL	3000K	12500E	3500N	12500E										
ĭ	Z,														
Z	SYD	03308	14700E	1000S	15200E	20008	15500E	2500S	15500E	32308	15400F				
¥	₹						!								
MOM	N	N0009	00500W	4700N	05000W	4108N	W00790								
MRC	NIS														
	X	5100N	M00600	4700N	W00030	4108N	W00790								
MUC	구	4530N	01221E	4000N	01900E	3720N	01947E	3425N	02400E						
2	WAS	5100N	M00600	4700N	05000W	4106N	W00790		!						
							;;;;;;;;;;;;;;;;;;;;;;;;;;;;;;;;;;;;;;;								

Origin	Deet.	Waypoint 1	1	Waypoint 2	t2	Waypoint 3	13	Wavpoint 4	7.	Waveclet	2	Wavecint	-	Waynoint 7	
		Lat	Long.	.	Long.	Let	Long.	1	Long	1	Long.	Lat	Long.	Lat	Long.
	!														
ت 1	X	0000 0000	00500W	2800N	04500W	6100N	06500W	6200N	W00070	9 300N	07500W	6230N	W00080	٠	
MCC	χ	N0009	00500W	2800N	04500W	6100N	06500W	6200N	W00070	6300N	07500W	6230N	0800W		
MUC	X	5100N	M00600	4700N	0500W	4106N	W00790								
ZYZ	ANC														
NAN	SYD														
NAC	LON	4108N	06700W	4700N	05000W	5100N	W00900								
NAC	OSL	4108N	W00790	4700N	05000W										
NAC	PAR	4108N	W00790	4800N	W00900										
N	ΡΤ	2500N	07500W												
N	ROM	4108N	W00700	4600N	W00000							-			
NAC	SEA			:											
NAC	S S														
N	NNS SNN	4108N	W00790	4700N	05000W										
NAC	STO	4108N	W00780	4700N	05000W										
NAC	ΝE	4108N	W00790	4800N	W00900										
N	WAW	4108N	W00790	4700N	05000W	N0009	00500W								
	αDΧ	3400N	14100E	3700N	14700E										
¥80 1	SEA	3400N	14100E	2000N	17900W										
	SFO	3400N	14100E												
OSA	NIS S	3300N	13700E	N0090	10800E										
OSA	SYD	02008	15400E	2000S	15500E	2500S	15500E	3230S	15400E						
OSA	Y	3400N	14100E	2000N	17900W										
PAR	ВАН	4530N	01221E	4000N	01900E	3720N	01947E	3425N	02400E	3110N	03325E	2845N	03440F		
PAR	DKR	4200N	01700W	2000N	02000W										
PAR	αDΧ	6 230N	00300E	7200N	02500E	7200N	13230E								
PAR	¥	4800N	W00900												
PAR	됨	5100N	W00000	4700N	05000W	4108N	W00780								
PAR	SFO	5100N	M00600	2800N	04500W	6100N	06500W	6200N	07000W	8300N	07500W	6230N	W0000		
PAR	ያፗ	5100N	M00600	4700N	05000W	4108N	W00780								
PAR	7	4530N	01221E	4000N	01900E	3720N	01947E	3425N	02400E						
PAR	WAS	4800N	W00000	4108N	06700W										
PAR	VM0	4800N	W00000	4108N	W00790										
PAR	*	5100N	M00600	4700N	05000W	4106N	W00780								
PEX	몺	3900N	11800E	3800N	12300E	3000K	12300E	X0080	10800E						
PER	SYD	35008	11300E	4500S	15000E										
PER	<u>ک</u>	0100N	11930E	0500N	12600E	3000N	13500E								
P 0	HKG	03308	14700E	2000N	12200E										
X	SYD	20008	15500E	2500\$	15500E	3230S	15400E								

Waypoint 7 Lat. Long.																															
Wayi Long. L																	ע														
																16400	5														
Waypoint 6 Let																30300	20030														
5 Long.																15500E							14700E			L					
Waypoint 5 Lat.																25008							03308			140000	None				
Long.																15500E							15200E	15400E		10000	3005				
waypoint 4 Lat.																20003							10008	02008		Money			=		
Long.											10800E					14200E			03500W				15500E	15500E		10KME					
waypomt 3 Lat.											0000N					10008			2000S 0				2000\$	20008		3500N					
Long.			W00680			W00780	W00790	14100E			12500E				-10800E	12000E		13700E	03200W				15500E			13000F				10900E	
Lat			02008			4108N	4106N	3400N			3000N				N0080	0700S		3300N	0730S					2500S		3000N				N0090	
Long.			07500W	03500W	06700W	M00600	W00800	17900W	17900W		12500E				12500E	10900E	10800E	10000E	06100W		06700W	16500E	15400E	15400E		14100E	17900W			13700E	
19			20003						\$000¥		3500N				3000N	03078	N0090	N0090	1435N		4106N			32308			2000N			3300N	
	MOD	SYD	ACA	DKR	WAS	YMO	7,42	VSO	1 40	WAS	N S	<u>ک</u>	Ĭ	<u>ک</u>	N S	SYD	TPE	1 40	₽	WAS	772	Ž	1 6	2	ŠŽ	PEK	SEA	SEL	SFO	NIS	
	PPT	PPT	잁	욡	30	ROM	ROM	SEA	SEA				SFO	SFO				NIS							2 2						

Appendix E. Universal Airline System Scheduling

The passenger demand for HSCT service between city-pairs is determined by forecast growth rates and the HSCT market penetration. Once the demands between city-pairs are determined, an acceptable schedule for the HSCT fleet must be created. The schedule is built using a Boeing-developed "Sequential Itinerary" model which dynamically links the cities and demands in the HSCT route network, finding a suitable set of city-pairs for each airplane to serve. The model accounts for airport curfews and for passenger-preferred departure and arrival time "windows". The following is a brief explanation of the model operation:

(Refer to Figure E-1). At the start of the operational day at city "A", the model examines all possible routes that could be flown to carry demand from city "A", looking ahead one leg beyond the first destination. Passenger preference time windows for departure and arrival and airport curfews will likely limit the routes that can be served. In this example, flights are restricted to A-B, then B-F or B-G.

The first airplane is assigned to route A-B (Figure E-2, I). At B, the model looks ahead for the routes to serve which will minimize the time on the ground at B. The model assumes that the minimum ground time for a "turn", that is the end of a flight number, is 1.5 hours. The minimum ground time for a through stop, that is an intermediate stop in the flight required for refueling, is 1.0 hours. In this example (Figure E-2, II), serving B-F then F-P will require stopping at F until the airplane can clear the preference/curfew "window" at P. Since the ground time to serve B-F-P would be longer than that required to serve B-G and then G-K, the model assigns the airplane to the latter routes.

As the airplane "flies" the city-pairs, the model tracks accumulated time for that airplane. The operational day for the airplane (block time for the flights, ground time for "turns" and through stops) is limited to 24 hours less a set maintenance interval, since the model logic works with daily demand. The model uses the 24 hour limit as well as the preference/curfew "windows" in assigning routes. The time limit is obviously more restrictive near the end of the operational day.

As airplane number 1 reaches city P, (Figure E-2, III) its operational day ends with an accumulated time of 20+ hours. At that point airplane number 2 is assigned to serve the cities that receive demand from P. The model schedules airplane 2 in the same manner as number 1, linking together cities which have HSCT demand assigned until the end of the operational day for airplane 2, at which point airplane 3 is assigned. This process continues until all the city-pair demand is served, which takes 500 airplanes and 500 "airplane-days" in the base case. While the model links single airplanes and itineraries sequentially, the results are the same as if multiple airplanes operated together at the same time on the schedule determined by the model.

"Sequential Itinerary" Scheduling Model

City pairs and trip frequencies available for airplane starting the operational day at city "A", "looking ahead" one leg.

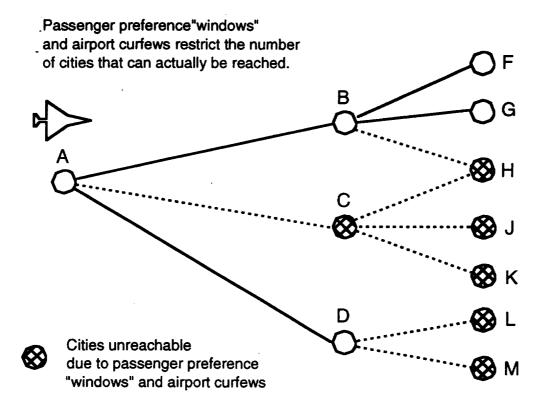


Figure E-1. Sequential Intinerary Scheduling Model Schematic, 1 airplane

"Sequential Itinerary" Scheduling Model

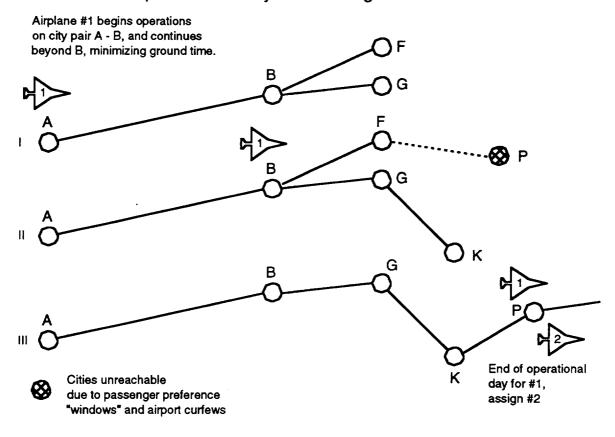


Figure E-2. Sequential Itinerary Scheduling Model Schematic, 3 airplanes.

Table E-1 shows the details of the scheduling of the first 5 airplanes in the 1994 HSCT emissions route system. Because of its speed, the HSCT has the ability to serve a large set of cities and still remain within the preference/curfew time "windows", which are always defined in local time. Thus airplane #1 in the example in Table E-1 begins the day in New York at 0800 New York time, flies to Warsaw and back, then on to Tokyo via Seattle, ending its day at 2023 local time after the short flight from Tokyo to Manila. Airplane #2 starts at Manila at 2153, and can reach Singapore at 2335, then off to Sydney, arriving at 0701 the next morning. From Sydney, the airplane can reach Tokyo at 1131, then to Washington via Seattle, arriving at 0815 local time. Airplane #3 starts from Washington, and ends its day in Guam. Airplane #4 starts in Guam and ends up in Singapore, airplane #5 starts in Singapore and ends up back in Singapore after six trips. Airplane #6 starts in Singapore, and ends its day in Los Angeles. Airplane #7 starts in Los Angeles and ends its day in Seattle and so on until all demand on all city pairs is satisfied.

Table E-1. HSCT "Sequential Itinerary" Scheduling Model

					Local Time		Block	Ground Time (Hrs)	Ground Time (Hrs)
Airplane #	Flight #	Origin	Dest.	Via	Depart	Arrive	Time (Hrs)	(Turn)	(at Via Cities)
1	1	NYC	WAW		800	1744	3.8	1.5	
1	2	WAW	NYC		1913	1703	3.8	1.5	
1	3	NYC	TYO	SEA	1832	1826	8.4	1.0	1.0
1	4	TYO	MNL		1925	2023	2.0		
					Onamtional	Totals	17.9	4.0	1.0
					Operational Hours	Uay	22.8		
2	5	MNL	SIN		2153	2335	1.7	1.5	
2	6	SIN	SYD		105	701	3.9	1.5	
2 2 2	7	SYD	TYO		831	1131	4.0	1.5	
2	8	TYO	WAS	SEA	1301	745	8.2		1.0
						Totals	17.8	4.5	1.0
					Operational	Day	23.3	•	
					Hours				
3	9	WAS	TYO	SEA	937	907	8.2	1.2	1.0
3	10	TYO	YVR		1018	2114	4.0	1.5	
3	11	YVR	TYO		2243	1943	4.0	1.5	
3	12	TYO	GUM		2113	2358	1.7		
						Totals	17.8	4.2	1.0
					Operational Hours	Day	23.0		
4	13	GUM	TYO		645	728	1.7	1.5	
4	14	TYO	SYD		858	1400	4.0	1.5	
4	15	SYD	TPE		1529	1726	4.0	1.5	
4	16	TPE	SIN		1856	2104	2.1		
						Totals	11.8	4.5	0.0
					Operational Hours	Day	16.3		
5	17	SIN	MRU		2234	2150	3.2	1.5	
5	18	MRU	SIN		2320	630	3.2	1.5	
5	19	SIN	TYO		759	1151	2.9	1.5	
5	20	TYO	SIN		1321	1515	2.9	1.5	
5	21	SIN	TPE		1645	1847	2.1	1.5	
5	22	TPE	SIN		2016	2224	2.1		
						Totals	16.4	7.5	0.0
					Operational Hours	Day	23.8		

Appendix F. Altitude Distribution of Emissions for Mach 2.4 HSCT fleets

This appendix contains the tables which summarize the different Mach 2.4 HSCT emission scenarios. For each of the scenarios considered, the fuel burned and emissions (NOx, CO, and hydrocarbons) were summed over latitude and longitude and tabulated as a function of altitude in 1 km altitude increments (the resolution of the data set).

Cumulative fractions of fuel burned and emissions were calculated from the ground up to provide a simple way to evaluate how the emissions were distributed vertically. In addition, the effective emission index for each altitude band was calculated and tabulated.

The global total of fuel burned and emissions were calculated and listed at the bottom of each table. Also, included is the effective emission index for NOx, CO, and hydrocarbons, globally averaged over all locations and altitudes.

For the charts shown, the notation 1.00E+08 is equivalent to 1.00 x 10⁸. The emissions are in units of kilograms per year and the emission indices have units of grams of emissions per kilogram of fuel burned.

US Standard Atmosphere (1976) pressures and temperatures were used in the calculations. These altitudes correspond to the geopotential altitudes of the US Standard Atmosphere grid.

Table F-1. Fuel burned, emissions, cumulative fractions of emissions, and emission indices as a function of altitude (Summed over Latitude and Longitude) for the Mach 2.4 (Nominal EI(NOx)=5) HSCT fleet only, assuming 500 HSCTs are flying on the universal network.

Altitude Band (km)	Fuel (kg/year)	cum fuel (%)	NOx (kg/year)	cum NOx (%)	HC (kg/year)	cum HC (%)	CO (kg/year)	cum CO (%)	EI(NOx)	EI(HC)	EI(CO)
	2.32E+09	2.82%	1.66E+07	3.11%	2.89E+06	9.75%	2.72E+07	11.26%	7.17	1.25	11.73
	8.34E+08	3.83%	6.88E+06	4.39%	4.67E+05	11.32%	2.94E+06	12.48%	8.24	0.56	3.53
	8.34E+08	4.85%	6.88E+06	5.68%	4.68E+05	12.90%	2.94E+06	13.70%	8.24	0.56	3.53
	8.36E+08	5.87%	6.89E+06	6.97%	4.68E+05	14.48%	2.94E+06	14.92%	8.24	0.56	3.52
	8.34E+08	6.88%	6.87E+06	8.25%	4.67E+05	16.05%	2.94E+06	16.14%	8.24	0.56	3.53
	8.34E+08	7.90%	6.88E+06	9.54%	4.68E+05	17.63%	2.95E+06	17.36%	8.24	0.56	3.53
	8.34E+08	8.92%	6.88E+06	10.82%	4.68E+05	19.20%	2.95E+06	18.58%	8.24	0.56	3.53
	8.35E+08	9.93%	6.88E+06	12.11%	4.68E+05	20.78%	2.95E+06	19.80%	8.24	0.56	3.53
	1.12E+09	11.29%	9.23E+06	13.84%	5.94E+05	22.79%	4.22E+06	21.55%	8.26	0.53	3.77
	2.87E+09	14.79%	2.39E+07	18.30%	1.33E+06	27.26%	1.08E+07	26.02%	8.32	0.46	3.76
	3.11E+09	18.58%	2.60E+07	23.17%	1.36E+06	31.86%	9.96E+06	30.15%	8.37	0.44	3.20
	2.30E+09	21.38%	1.94E+07	26.81%	9.61E+05	35.10%	5.25E+06	32.32%	8.43	0.42	2.28
	3.41E+09	25.53%	2.87E+07	32.18%	1.36E+06	39.69%	9.13E+06	36.11%	8.43	0.40	2.68
	1.77E+09	27.68%	1.52E+07	35.03%	5.55E+05	41.56%	1.08E+06	36.55%	8.61	0.31	0.61
	1.77E+09	29.84%	1.53E+07	37.88%	5.56E+05	43.43%	1.08E+06	37.00%	8.61	0.31	0.61
	1.77E+09	32.00%	1.52E+07	40.73%	5.55E+05	45.30%	1.08E+06	37.45%	8.61	0.31	0.61
	1.77E+09	34.15%	1.52E+07	43.58%	5.55E+05	47.18%	1.08E+06	37.90%	8.61	0.31	0.61
	3.19E+09	38.04%	2.25E+07	47.80%	9.63E+05	50.42%	5.49E+06	40.17%	7.06	0.30	1.72
	1.28E+10	53.61%	7.21E+07	61.28%	3.71E+06	62.94%	3.49E+07	54.65%	5.64	0.29	2.73
	2.40E+10	82.78%	1.30E+08	85.66%	6.91E+06	86.25%	6.87E+07	83.11%	5.44	0.29	2.87
	1.41E+10	100.00%	7.67E+07	100.00%	4.08E+06	100.00%	4.08E+07	100.00%	5.45	0.29	2.88
	8.21E+10		5.35E±08		2 07E±07		0.44 🖺 .00		4	90.0	6

Table F-2. Fuel burned, emissions, cumulative fractions of emissions, and emission indices as a function of altitude (Summed over Latitude and Longitude) for the Mach 2.4 (Nominal EI(NOx)=5) HSCT fleet only, assuming 1000 HSCTs are flying on the universal network.

EI(CO)	12.10	3.75	3.75	3.75	3.77	3.77	3.77	3.77	3.91	3.91	3.54	2.99	2.93	0.65	0.65	0.65	0.65	1.50	2.64	2.84	2.88	3.03
EI(HC)	1.28	0.58	0.58	0.58	0.58	0.58	0.58	0.58	0.56	0.48	0.45	0.44	0.41	0.32	0.32	0.32	0.32	0.31	0.29	0.29	0.29	0.38
EI(NOx)	7.13	8.21	8.21	8.21	8.21	8.21	8.21	8.21	8.23	8.30	8.34	8.38	8.41	8.61	8.61	8.61	8.61	7.39	5.78	5.49	5.43	6.62
cum CO (%)	12.81%	14.19%	15.56%	16.93%	18.31%	19.69%	21.07%	22.45%	24.22%	28.46%	33.28%	36.95%	41.69%	42.17%	42.65%	43.14%	43.62%	45.34%	26.30%	81.06%	100.00%	
CO (kg/year)	6.09E+07	6.53E+06	6.53E+06	6.53E+06	6.56E+06	6.56E+06	6.56E+06	6.56E+06	8.39E+06	2.02E+07	2.29E+07	1.74E+07	2.25E+07	2.29E+06	2.29E+06	2.29E+06	2.29E+06	8.21E+06	5.21E+07	1.18E+08	9.01E+07	4.76E+08
cum HC (%)	10.97%	12.68%	14.40%	16.11%	17.83%	19.55%	21.27%	22.99%	25.01%	29.22%	34.22%	38.57%	43.92%	45.84%	47.75%	49.66%	51.58%	54.42%	64.24%	84.64%	100.00%	
HC (kg/year)	6.45E+06	1.01E+06	1.19E+06	2.48E+06	2.94E+06	2.55E+06	3.15E+06	1.12E+06	1.13E+06	1.12E+06	1.12E+06	1.67E+06	5.77E+06	1.20E+07	9.03E+06	5.88E+07						
cum NOx (%)	3.46%	4.83%	6.21%	7.59%	8.96%	10.34%	11.71%	13.09%	14.79%	18.92%	24.12%	28.83%	35.05%	37.99%	40.94%	43.88%	46.82%	50.70%	61.70%	83.63%	100.00%	
NOx (kg/year)	3.59E+07	1.43E+07	1.77E+07	4.29E+07	5.40E+07	4.89E+07	6.46E+07	3.05E+07	3.06E+07	3.05E+07	3.05E+07	4.03E+07	1.14E+08	2.28E+08	1.70E+08	1.04E+09						
cum fuel (%)	3.21%	4.32%	5.43%	6.54%	7.65%	8.76%	9.87%	10.98%	12.35%	15.65%	19.78%	23.50%	28.40%	30.67%	32.93%	35.20%	37.46%	40.94%	53.55%	80.03%	100.00%	
Fuel (kg/year)	5.03E+09	1.74E+09	2.15E+09	5.17E+09	6.47E+09	5.83E+09	7.69E+09	3.55E+09	3.55E+09	3.55E+09	3.55E+09	5.45E+09	1.98E+10	4.15E+10	3.13E+10	1.57E+11						
Altitude Band (km)	0 - 1	1 - 2	2 - 3	3 - 4	4 - 5	9 - 9	2 - 9	7 - 8	6 - 8	9 - 10	10 - 11	11 - 12	12 - 13	13 - 14	14 - 15	15 - 16	16 - 17	17 - 18	18 - 19	19 - 20	20 - 21	Global Total

Table F-3. Fuel burned, emissions, cumulative fractions of emissions, and emission indices as a function of altitude assuming 500 HSCTs are flying on the 1993 AESA assessment network. (revised from NASA CR 4592) (Summed over Latitude and Longitude) for the Mach 2.4 (Nominal EI(NOx)=5) HSCT fleet only,

Table F-4. Fuel burned, emissions, cumulative fractions of emissions, and emission indices as a function of altitude (Summed over Latitude and Longitude) for the Mach 2.4 (Nominal EI(NOx)=15) HSCT fleet only, assuming 500 HSCTs are flying on the universal network.

Attitude Band (km)	Fuel (kg/year)	cum fuel (%)	NOx (kg/year)	cum NOx (%)	HC (kg/year)	cum HC (%)	CO (kg/year)	cum CO (%)	EI(NOx)	EI(HC)	EI(CO)
•	00.000	000	70.747.07	8000	L	0 750	707	7		10 1	1
-	Z.3ZE+03	6.02%	0.04E+0.0	2.33%	Z.89E+U0	8.75%	Z./ZE+0/	11.20%	15.28	CZ. L	11./3
1 - 2	8.34E+08	3.83%	1.92E+07	3.69%	4.67E+05	11.32%	2.94E+06	12.48%	22.97	0.56	3.53
2 - 3	8.34E+08	4.85%	1.92E+07	4.99%	4.68E+05	12.90%	2.94E+06	13.70%	22.97	0.56	3.53
3 - 4	8.36E+08	5.87%	1.92E+07	6.28%	4.68E+05	14.48%	2.94E+06	14.92%	22.98	0.56	3.52
4 - 5	8.34E+08	6.88%	1.92E+07	7.58%	4.67E+05	16.05%	2.94E+06	16.14%	22.97	0.56	3.53
5 - 6	8.34E+08	7.90%	1.92E+07	8.88%	4.68E+05	17.63%	2.95E+06	17.36%	22.97	0.56	3.53
2 - 9	8.34E+08	8.92%	1.92E+07	10.17%	4.68E+05	19.20%	2.95E+06	18.58%	22.96	0.56	3.53
7 - 8	8.35E+08	9.93%	1.92E+07	11.47%	4.68E+05	20.78%	2.95E+06	19.80%	22.97	0.56	3.53
6 - 8	1.12E+09	11.29%	2.15E+07	12.93%	5.94E+05	22.79%	4.22E+06	21.55%	19.24	0.53	3.77
9 - 10	2.87E+09	14.79%	4.15E+07	15.73%	1.33E+06	27.26%	1.08E+07	26.02%	14.45	0.46	3.76
10 - 11	3.11E+09	18.58%	5.16E+07	19.22%	1.36E+06	31.86%	9.96E+06	30.15%	16.57	0.44	3.20
11 - 12	2.30E+09	21.38%	4.94E+07	22.56%	9.61E+05	35.10%	5.25E+06	32.32%	21.44	0.42	2.28
12 - 13	3.41E+09	25.53%	5.94E+07	26.58%	1.36E+06	39.69%	9.13E+06	36.11%	17.44	0.40	2.68
13 - 14	1.77E+09	27.68%	4.54E+07	29.65%	5.55E+05	41.56%	1.08E+06	36.55%	25.65	0.31	0.61
14 - 15	1.77E+09	29.84%	4.54E+07	32.72%	5.56E+05	43.43%	1.08E+06	37.00%	25.65	0.31	0.61
15 - 16	1.77E+09	32.00%	4.54E+07	35.79%	5.55E+05	45.30%	1.08E+06	37.45%	25.65	0.31	0.61
16 - 17	1.77E+09	34.15%	4.54E+07	38.86%	5.55E+05	47.18%	1.08E+06	37.90%	25.65	0.31	0.61
17 - 18	3.19E+09	38.04%	6.73E+07	43.41%	9.63E+05	50.42%	5.49E+06	40.17%	21.06	0.30	1.72
18 - 19	1.28E+10	53.61%	2.16E+08	58.02%	3.71E+06	62.94%	3.49E+07	54.65%	16.88	0.29	2.73
19 - 20	2.40E+10	82.78%	3.91E+08	84.45%	6.91E+06	86.25%	6.87E+07	83.11%	16.31	0.29	2.87
20 - 21	1.41E+10	100.00%	2.30E+08	100.00%	4.08E+06	100.00%	4.08E+07	100.00%	16.25	0.29	2.88
Global Total	8.21E+10		1.48E+09		2.97E+07		2.41E+08		18.00	0.36	2 94
Global Total	8.21E+10		1.48E+09		2.97E+07		2.41E+08		4	8	3.00 0.36

Table F-5. Fuel burned, emissions, cumulative fractions of emissions, and emission indices as a function of altitude (Summed over Latitude and Longitude) for the Mach 2.4 (Nominal EI(NOx)=15) HSCT fleet only, assuming 1000 HSCTs are flying on the universal network.

Altitude Band (km)	Fuel (kg/year)	cum fuel (%)	NOx (kg/year)	cum NOX (%)	HC (kg/year)	cum HC (%)	CO (kg/year)	cum CO (%)	EI(NOx)	ЕІ(НС)	EI(CO)
•	100 U	9,00	100	7000	00 111	7010 07	0.000	, ,	0077	7	07 07
- - -	5.03E+08	3.21%	/.55E+0/	7.00%	0.40E+00	0.87%	0.09E+0/	12.81%	14.99	1.28	1Z. 52
1 - 2	1.74E+09	4.32%	3.96E+07	4.08%	1.01E+06	12.68%	6.53E+06	14.19%	22.77	0.58	3.75
2 - 3	1.74E+09	5.43%	3.96E+07	5.48%	1.01E+06	14.40%	6.53E+06	15.56%	22.77	0.58	3.75
3 - 4	1.74E+09	6.54%	3.96E+07	6.89%	1.01E+06	16.11%	6.53E+06	16.93%	22.77	0.58	3.75
4 - 5	1.74E+09	7.65%	3.96E+07	8.29%	1.01E+06	17.83%	6.56E+06	18.31%	22.75	0.58	3.77
9 - 9	1.74E+09	8.76%	3.96E+07	9.70%	1.01E+06	19.55%	6.56E+06	19.69%	22.75	0.58	3.77
2 - 9	1.74E+09	9.87%	3.96E+07	11.10%	1.01E+06	21.27%	6.56E+06	21.07%	22.74	0.58	3.77
7 - 8	1.74E+09	10.98%	3.96E+07	12.51%	1.01E+06	22.99%	6.56E+06	22.45%	22.75	0.58	3.77
6 - 8	2.15E+09	12.35%	4.30E+07	14.03%	1.19E+06	25.01%	8.39E+06	24.22%	20.00	0.56	3.91
9 - 10	5.17E+09	15.65%	7.54E+07	16.70%	2.48E+06	29.22%	2.02E+07	28.46%	14.59	0.48	3.91
10 - 11	6.47E+09	19.78%	9.95E+07	20.23%	2.94E+06	34.22%	2.29E+07	33.28%	15.36	0.45	3.54
11 - 12	5.83E+09	23.50%	1.05E+08	23.96%	2.55E+06	38.57%	1.74E+07	36.95%	18.03	0.44	2.99
12 - 13	7.69E+09	28.40%	1.26E+08	28.44%	3.15E+06	43.92%	2.25E+07	41.69%	16.42	0.41	2.93
13 - 14	3.55E+09	30.67%	9.09E+07	31.66%	1.12E+06	45.84%	2.29E+06	42.17%	25.62	0.32	0.65
14 - 15	3.55E+09	32.93%	9.10E+07	34.89%	1.13E+06	47.75%	2.29E+06	42.65%	25.62	0.32	0.65
15 - 16	3.55E+09	35.20%	9.09E+07	38.11%	1.12E+06	49.66%	2.29E+06	43.14%	25.62	0.32	0.65
16 - 17	3.55E+09	37.46%	9.09E+07	41.34%	1.12E+06	51.58%	2.29E+06	43.62%	25.62	0.32	0.65
17 - 18	5.45E+09	40.94%	1.20E+08	45.60%	1.67E+06	54.42%	8.21E+06	45.34%	22.03	0.31	1.50
18 - 19	1.98E+10	53.55%	3.42E+08	57.73%	5.77E+06	64.24%	5.21E+07	56.30%	17.30	0.29	2.64
19 - 20	4.15E+10	80.03%	6.82E+08	81.93%	1.20E+07	84.64%	1.18E+08	81.06%	16.45	0.29	2.84
20 - 21	3.13E+10	100.00%	5.09E+08	100.00%	9.03E+06	100.00%	9.01E+07	100.00%	16.27	0.29	2.88
Global Total	1 57E±11		2 R2E+00		5 RRE-107		4 76F±08		47.00	ac c	6

Table F-6. Fuel burned, emissions, cumulative fractions of emissions, and emission indices as a function of altitude assuming 500 HSCTs are flying on the 1993 AESA assessment network. (revised from NASA CR 4592) (Summed over Latitude and Longitude) for the Mach 2.4 (Nominal EI(NOx)=15) HSCT fleet only,

EI(CO)	11.98							3.57		3.28		2.94			0.61							2.97
ЕІ(НС)	1 27	0.56	0.56	0.56	0.56	0.56	0.56	0.56	0.52	0.45	0.44	0.43	0.41	0.31	0.31	0.31	0.31	0.30	0.29	0.29	0.29	0.37
EI(NOx) EI(HC)	15.22	22.93	22.93	22.93	22.93	22.93	22.93	22.93	19.28	16.92	16.50	17.65	15.61	25.65	25.65	25.65	25.65	20.73	16.86	16.33	16.26	17.91
cum CO (%)	11.45%	12.69%	13.94%	15.19%	16.43%	17.68%	18.93%	20.18%	22.01%	25.49%	29.79%	33.73%	39.25%	39.66%	40.10%	40.54%	40.98%	43.47%	57.71%	84.51%	100.00%	
CO (kg/year)	2.78F±07	3.02E+06	3.02E+06	3.02E+06	3.02E+06	3.02E+06	3.02E+06	3.02E+06	4.45E+06	8.44E+06	1.04E+07	9.55E+06	1.33E+07	1.07E+06	1.07E+06	1.07E+06	1.07E+06	6.06E+06	3.45E+07	6.50E+07	3.76E+07	2.42E+08
cum HC (%)	88.6	11.48%	13.07%	14.67%	16.27%	17.87%	19.47%	21.07%	23.18%	27.07%	31.83%	36.49%	42.48%	44.32%	46.16%	48.00%	49.84%	53.23%	65.49%	87.41%	100.00%	
HC (kg/year)	2.95E+06	4.77E+05	4.77E+05	4.77E+05	4.77E+05	4.77E+05	4.77E+05	4.77E+05	6.33E+05	1.16E+06	1.42E+06	1.39E+06	1.79E+06	5.50E+05	5.50E+05	5.50E+05	5.50E+05	1.01E+06	3.66E+06	6.55E+06	3.76E+06	2.99E+07
cum NOx (%)	2.41%	3.74%	5.07%	6.40%	7.72%	9.05%	10.38%	11.71%	13.31%	16.28%	19.96%	23.88%	28.55%	31.63%	34.71%	37.78%	40.86%	45.63%	60.17%	85.50%	100.00%	
NOx (kg/year)	3.53E+07	1.94E+07	2.34E+07	4.35E+07	5.37E+07	5.74E+07	6.83E+07	4.50E+07	4.50E+07	4.50E+07	4.50E+07	6.97E+07	2.13E+08	3.70E+08	2.12E+08	1.46E+09						
cum fuel (%)	2.84%	3.88%	4.91%	5.95%	6.99%	8.02%	9.06%	10.10%	11.59%	14.74%	18.72%	22.71%	28.07%	30.22%	32.37%	34.51%	36.66%	40.78%	56.23%	84.03%	100.00%	
Fuel (kg/year)	2.32E+09	8.47E+08	8.47E+08	8.47E+08	8.47E+08	8.47E+08	8.47E+08	8.47E+08	1.21E+09	2.57E+09	3.25E+09	3.25E+09	4.38E+09	1.75E+09	1.75E+09	1.75E+09	1.75E+09	3.36E+09	1.26E+10	2.27E+10	1.30E+10	8.16E+10
Altitude Band (km)	0 - 1	1 - 2	2 - 3	3 - 4	4 - 5	9 - 9	2 - 9	7 - 8	6 - 8	9 - 10	10 - 11	11 - 12	12 - 13	13 - 14	14 - 15	15 - 16	16 - 17	17 - 18	18 - 19	19 - 20	20 - 21	Global Total

-		

Appendix G. Altitude Distribution of Emissions for Mach 2.0 HSCT fleets

This appendix contains the tables which summarize the different Mach 2.0 HSCT emission scenarios. For each of the scenarios considered, the fuel burned and emissions (NOx, CO, and hydrocarbons) were summed over latitude and longitude and tabulated as a function of altitude in 1 km altitude increments (the resolution of the data set).

Cumulative fractions of fuel burned and emissions were calculated from the ground up to provide a simple way to evaluate how the emissions were distributed vertically. In addition, the effective emission index for each altitude band was calculated and tabulated.

The global total of fuel burned and emissions were calculated and listed at the bottom of each table. Also, included is the effective emission index for NOx, CO, and hydrocarbons, globally averaged over all locations and altitudes.

For the charts shown, the notation 1.00E+08 is equivalent to 1.00×10^8 . The emissions are in units of kilograms per year and the emission indices have units of grams of emissions per kilogram of fuel burned.

US Standard Atmosphere (1976) pressures and temperatures were used in the calculations. These altitudes correspond to the geopotential altitudes of the US Standard Atmosphere grid.

Table G-1. Fuel burned, emissions, cumulative fractions of emissions, and emission indices as a function of attitude (Summed over Latitude and Longitude) for the Mach 2.0 (Nominal EI(NOx)=5) HSCT fleet only, assuming passenger demand corresponding to 500 Mach 2.4 HSCTs flying on the universal network.

ł	Altitude Band (km)	l	Fuel (kg/year)	cum fuel (%)	NOx (kg/year)	cum NOx (%)	HC (kg/year)	cum HC (%)	CO (kg/year)	cum CO (%)	EI(NOx)	EI(HC)	EI(CO)
	0 - 1	αi	2.11E+09	2.50%	1.54E+07	3.06%	2.50E+06	8.62%	2.34E+07	9.48%	7.29	118	11.08
	1 - 2	7.	7.66E+08	3.41%	6.04E+06	4.25%	4.22E+05	10.07%	2.64E+06	10.55%	7.88	0.55	3.45
	2 - 3	7.	7.66E+08	4.31%	6.03E+06	5.45%	4.22E+05	11.53%	2.64E+06	11.62%	7.88	0.55	3.45
	3 - 4	7.	7.67E+08	5.22%	6.04E+06	6.65%	4.22E+05	12.98%	2.64E+06	12.69%	7.88	0.55	3.45
	4 - 5	7.	7.66E+08	6.13%	6.03E+06	7.85%	4.22E+05	14.44%	2.64E+06	13.76%	7.88	0.55	3.45
	9 - 9	7.	7.65E+08	7.03%	6.03E+06	9.04%	4.22E+05	15.89%	2.64E+06	14.83%	7.88	0.55	3.45
	2 - 9	7.	7.67E+08	7.94%	6.04E+06	10.24%	4.22E+05	17.35%	2.64E+06	15.90%	7.88	0.55	3.45
	7 - 8	7.	7.67E+08	8.85%	6.04E+06	11.44%	4.22E+05	18.80%	2.64E+06	16.97%	7.87	0.55	3.45
	6 - 8	- -	1.21E+09	10.29%	9.00E+06	13.23%	5.75E+05	20.79%	4.15E+06	18.65%	7.41	0.47	3.41
_	9 - 10	.2	2.78E+09	13.58%	1.97E+07	17.14%	1.10E+06	24.57%	8.66E+06	22.16%	7.09	0.40	3.12
	10 - 11	- 2	2.64E+09	16.69%	1.93E+07	20.97%	1.03E+06	28.11%	7.02E+06	25.00%	7.33	0.39	2.66
	11 - 12	ر. د	2.02E+09	19.09%	1.56E+07	24.06%	8.07E+05	30.90%	4.34E+06	26.76%	7.70	0.40	2.14
	12 - 13	3	2.97E+09	22.60%	2.18E+07	28.39%	1.04E+06	34.47%	6.56E+06	29.42%	7.35	0.35	2.21
	13 - 14	-	.51E+09	24.39%	1.22E+07	30.81%	4.75E+05	36.11%	9.40E+05	29.80%	8.07	0.31	0.62
	14 - 15	٠ <u>.</u>	.51E+09	26.18%	1.22E+07	33.23%	4.75E+05	37.75%	9.35E+05	30.18%	8.08	0.31	0.62
	15 - 16	~ :	.52E+09	27.97%	1.22E+07	35.66%	4.77E+05	39.39%	9.54E+05	30.56%	8.07	0.31	0.63
	16 - 17	, 6.	6.67E+09	35.86%	3.82E+07	43.25%	1.95E+06	46.12%	1.66E+07	37.30%	5.73	0.29	2.50
	17 - 18	~·	.82E+10	57.44%	9.70E+07	62.51%	5.27E+06	64.29%	5.15E+07	58.14%	5.32	0.29	2.85
	18 - 19	<u>ي</u> 2	2.66E+10	88.88%	1.40E+08	90.22%	7.65E+06	% 29.06	7.63E+07	89.04%	5.26	0.29	2.87
	19 - 20	6 (9.39E+09	100.00%	4.93E+07	100.00%	2.71E+06	100.00%	2.71E+07	100.00%	5.25	0.29	2.88
	Global Total		8.45E+10		5.04E+08		2.90E+07		2.47E+08		5.96	0.34	2 92
1		l			*						?	l	1

Table G-2. Fuel burned, emissions, cumulative fractions of emissions, and emission indices as a function of altitude assuming passenger demand corresponding to 1000 Mach 2.4 HSCTs flying on the universal network. (Summed over Latitude and Longitude) for the Mach 2.0 (Nominal EI(NOx)=5) HSCT fleet only,

0 - 1 4.58 1 - 2 1.59 2 - 3 1.59 3 - 4 1.59 4 - 5 1.59 5 - 6 1.59	4.58E+09 1.59E+09 1.59E+09 1.59E+09 1.59E+09	9 87%					(ng/gai)	(6/)			
1 - 2 1.591 2 - 3 1.591 3 - 4 1.591 4 - 5 1.591 5 - 6 1.591	E +09 E +09 E +09 E +09 E +09	6.5.9	3.33E+07	3.46%	5.57E+06	9.85%	5.25E+07	10.99%	7.28	1.22	11.46
2 - 3 1.591 3 - 4 1.591 4 - 5 1.591 5 - 6 1.591	E+09 E+09 E+09 E+09	3.86%	1.25E+07	4.75%	9.06E+05	11.45%	5.85E+06	12.22%	7.86	0.57	3.68
3 - 4 1.598 4 - 5 1.598 5 - 6 1.591	E+09 E+09 E+09	4.86%	1.25E+07	6.04%	9.06E+05	13.05%	5.85E+06	13.44%	7.86	0.57	3.68
4 - 5 1.59I 5 - 6 1.59I	E+09 E+09	5.85%	1.25E+07	7.34%	9.06E+05	14.66%	5.85E+06	14.67%	7.86	0.57	3.68
5 - 6 1.59	E+09	6.85%	1.25E+07	8.63%	9.09E+05	16.26%	5.88E+06	15.90%	7.86	0.57	3.70
		7.84%	1.25E+07	9.93%	9.09E+05	17.87%	5.89E+06	17.13%	7.86	0.57	3.70
6 - 7 1.59	.59E+09	8.84%	1.25E+07	11.22%	9.10E+05	19.48%	5.89E+06	18.36%	7.86	0.57	3.70
7 - 8 1.59	1.59E+09	9.84%	1.25E+07	12.52%	9.10E+05	21.09%	5.89E+06	19.59%	7.86	0.57	3.70
8 - 9 2.22	2.22E+09	11.23%	1.67E+07	14.25%	1.12E+06	23.08%	8.00E+06	21.27%	7.50	0.51	3.60
9 - 10 5.03	5.03E+09	14.37%	3.57E+07	17.94%	2.07E+06	26.74%	1.65E+07	24.72%		0.41	3.28
10 - 11 5.57	5.57E+09	17.86%	4.01E+07	22.10%	2.22E+06	30.66%	1.64E+07	28.16%		0.40	2.95
11 - 12 5.23	5.23E+09	21.14%	3.87E+07	26.11%	2.08E+06	34.33%	1.38E+07	31.04%	7.39	0.40	2.63
12 - 13 6.72	6.72E+09	25.34%	4.88E+07	31.17%	2.38E+06	38.54%	1.62E+07	34.43%	7.26	0.35	2.41
13 - 14 3.03	3.03E+09	27.24%	2.45E+07	33.70%	9.63E+05	40.24%	2.00E+06	34.84%	8.07	0.32	99.0
14 - 15 3.03	3.03E+09	29.14%	2.45E+07	36.24%	9.62E+05	41.95%	1.99E+06	35.26%	8.07	0.32	99.0
15 - 16 3.041	3.04E+09	31.04%	2.45E+07	38.78%	9.65E+05	43.65%	2.02E+06	35.68%	8.07	0.32	0.66
16 - 17 1.011	1.01E+10	37.35%	6.00E+07	45.00%	2.98E+06	48.92%	2.34E+07	40.58%	5.96	0.30	2.33
17 - 18 2.89	2.89E+10	55.44%	1.56E+08	61.14%	8.37E+06	63.72%	8.01E+07	57.34%	5.39	0.29	2.77
18 - 19 4.88	4.88E+10	85.97%	2.57E+08	87.81%	1.41E+07	88.59%	1.39E+08	86.49%	5.28	0.29	2.86
19 - 20 2.24	2.24E+10	100.00%	1.18E+08	100.00%	6.46E+06	100.00%	6.45E+07	100.00%	5.25	0.29	2.88
Global Total 1.60	1.60E+11		9.65E+08		5.66E+07		4.78E+08		6.04	0.35	2.99

assuming passenger demand corresponding to 500 Mach 2.4 HSCTs flying on the 1993 AESA assessment network. (revised from NASA CR 4592) Table G-3. Fuel burned, emissions, cumulative fractions of emissions, and emission indices as a function of altitude (Summed over Latitude and Longitude) for the Mach 2.0 (Nominal EI(NOx)=5) HSCT fleet only,

	Fuel (kg/year)	cum fuel (%)	NOx (kg/year)	cum NOx (%)	HC (kg/year)	cum HC (%)	CO (kg/year)	cum CO (%)	EI(NOx) EI(HC)	EI(HC)	EI(CO)
0 - 1	2.11E+09	2.52%	1.54E+07	3.07%	2.55E+06	8.81%	2.39E+07	9.75%	7.32	121	11.35
1 - 2	7.76E+08	3.45%	6.11E+06	4.29%	4.30E+05	10.30%	2.71E+06	10.85%	7.87	0.55	3.50
2 - 3	7.76E+08	4.38%	6.11E+06	5.51%	4.30E+05	11.79%	2.71E+06	11.96%	7.87	0.55	3.50
3 - 4	7.76E+08	5.30%	6.11E+06	6.72%	4.30E+05	13.27%	2.71E+06	13.06%	7.87	0.55	3.50
4 - 5	7.76E+08	6.23%	6.11E+06	7.94%	4.30E+05	14.76%	2.71E+06	14.17%	7.87	0.55	3.50
5 - 6	7.76E+08	7.16%	6.11E+06	9.16%	4.30E+05	16.25%	2.71E+06	15.27%		0.55	3.50
2 - 9	7.76E+08	8.09%	6.11E+06	10.38%	4.30E+05	17.74%	2.71E+06	16.38%		0.55	3.50
7 - 8	7.76E+08	9.02%	6.11E+06	11.59%	4.30E+05	19.22%	2.71E+06	17.48%		0.55	3.50
8 - 9	1.15E+09	10.39%	8.58E+06	13.30%	5.56E+05	21.15%	3.90E+06	19.07%	7.49	0.49	3.40
9 - 10	2.48E+09	13.35%	1.80E+07	16.90%	9.88E+05	24.56%	7.04E+06	21.94%	7.28	0.40	2.84
10 - 11	2.80E+09	16.70%	2.04E+07	20.97%	1.09E+06	28.32%	7.56E+06	25.03%	7.30	0.39	2.70
11 - 12	2.90E+09	20.17%	2.13E+07	25.22%	1.11E+06	32.17%	7.35E+06	28.02%	7.37	0.38	2.54
12 - 13	3.82E+09	24.74%	2.74E+07	30.69%	1.33E+06	36.78%	9.46E+06	31.88%	7.18	0.35	2.47
13 - 14	1.51E+09	26.55%	1.22E+07	33.13%	4.76E+05	38.42%	9.38E+05	32.26%	8.08	0.31	0.62
14 - 15	1.51E+09	28.37%	1.22E+07	35.57%	4.76E+05	40.07%	9.38E+05	32.65%	8.08	0.31	0.62
15 - 16	1.52E+09	30.18%	1.23E+07	38.02%	4.78E+05	41.72%	9.54E+05	33.03%	8.07	0.31	0.63
16 - 17	7.01E+09	38.57%	3.99E+07	45.97%	2.05E+06	48.81%	1.77E+07	40.25%	5.70	0.29	2.53
17 - 18	1.75E+10	59.46%	9.30E+07	64.51%	5.04E+06	66.25%	4.92E+07	60.32%	5.33	0.29	2.85
18 - 19	2.53E+10	89.76%	1.33E+08	91.05%	7.30E+06	91.48%	7.27E+07	89.96%	5.26	0.29	2.87
19 - 20	8.56E+09	100.00%	4.49E+07	100.00%	2.47E+06	100.00%	2.46E+07	100.00%	5.25	0.29	2.88
Global Total	8.36E+10		5.02E+08		2.89E+07		2.45F+08		900	0.35	2 94

Table G-4. Fuel burned, emissions, cumulative fractions of emissions, and emission indices as a function of attitude (Summed over Latitude and Longitude) for the Mach 2.0 (Nominal EI(NOx)=15) HSCT fleet only, assuming passenger demand corresponding to 500 Mach 2.4 HSCTs flying on the universal network.

cum fuel	nei NOx (kg/vear)	cum NOx (%)	HC (kg/year)	cum HC (%)	CO (kg/year)	cum CO (%)	EI(NOx)	EI(HC)	EI(CO)
¥	Vear	(%)	(Ny year)	/6/	/ Z & 1				1
2.50%	3.15E+07	2.13%	2.50E+06	8.62%	2.34E+07	9.48%	14.89		_
3.41%	1.65E+07	3.25%	4.22E+05	10.07%	2.64E+06	10.55%	21.58		
4.31% 1	.65E+07	4.37%	4.22E+05	11.53%	2.64E+06	11.62%	21.58		
-	.65E+07	5.49%	4.22E+05	12.98%	2.64E+06	12.69%	21.58		
6.13% 1	.65E+07	6.61%	4.22E+05	14.44%	2.64E+06	13.76%	21.58		
7.03% 1	.65E+07	7.73%	4.22E+05	15.89%	2.64E+06	14.83%	21.58		
_	.65E+07	8.85%	4.22E+05	17.35%	2.64E+06	15.90%	21.58		
_	.65E+07	9.97%	4.22E+05	18.80%	2.64E+06	16.97%	21.57		
N	2.54E+07	11.69%	5.75E+05	20.79%	4.15E+06	18.65%	20.93		
•	5.75E+07	15.59%	1.10E+06	24.57%	8.66E+06	22.16%	20.70		
٠,	5.64E+07	19.40%	1.03E+06	28.11%	7.02E+06	25.00%	21.39		2.66
4	1.51E+07	22.46%	8.07E+05	30.90%	4.34E+06	26.76%			
	3.45E+07	26.83%	1.04E+06	34.47%	6.56E+06	29.42%			
•	3.63E+07	29.29%	4.75E+05	36.11%	9.40E+05	29.80%			
•••	3.63E+07	31.75%	4.75E+05	37.75%	9.35E+05	30.18%			
•	3.64E+07	34.21%	4.77E+05	39.39%	9.54E+05	30.56%			
•	.14E+08	41.95%	1.95E+06	46.12%	1.66E+07	37.30%			
	2.91E+08	61.65%	5.27E+06	64.29%	5.15E+07	58.14%	15.95		
•	4.19E+08	89.99%	7.65E+06	%29.06	7.63E+07	89.04%	15.76		
	.48E+08	100.00%	2.71E+06	100.00%	2.71E+07	100.00%	, 15.73	0.29	9 2.88
•	1		1000		9 47 5 , 00		17.48	0.34	2 9 9
7.	1.48E+09		2.90E+0/		Z.4/E+00		ř.		۱

Table G-5. Fuel burned, emissions, cumulative fractions of emissions, and emission indices as a function of altitude assuming passenger demand corresponding to 1000 Mach 2.4 HSCTs flying on the universal network. (Summed over Latitude and Longitude) for the Mach 2.0 (Nominal EI(NOx)=15) HSCT fleet only,

Attitude Band (km)	Fuel (kg/year)	cum fuel (%)	NOx (kg/year)	cum NOx (%)	HC (kg/year)	cum HC (%)	CO (kg/year)	cum CO	EI(NOX) EI(HC) EI(CO)	EI(HC)	EI(CO)
0 - 1	4 58F±00	9 87%	8 80E.07	0 070	1						
• •	200.7	6.07.9	0.095+07	2.37%	5.5/E+06	8.85%	5.25E+07	10.99%	14.60	1.22	11.46
7-1	1.59E+09	3.86%	3.40E+07	3.58%	9.06E+05	11.45%	5.85E+06	12.22%	21.38	0.57	3 60
2 - 3	1.59E+09	4.86%	3.40E+07	4.79%	9.06E+05	13.05%	5.85F±06	13 44%	24.20	0.0	9 0
3 - 4	1.59E+09	5.85%	3.40E+07	2.99%	9.06E+05	14.66%	5.85F±06	14.67%	2 2 2	0.0	00.0
4 - 5	1.59E+09	6.85%	3.40E+07	7.20%	9.09E+05	16.26%	5 88F±06	15.00%	21.30 24.36	0.0	0.00
9 - 9	1.59E+09	7.84%	3.40E+07	8.40%	9.09E+05	17.87%	5.89E+06	17.30%	24.20	0.57	0 . v
. 2 - 9	1.59E+09	8.84%	3.40E+07	9.61%	9 10F±05	10.48%	5.00E-106	10.000	00.19	0.57	3.70
7 - 8	1.59E+09	9.84%	3.40F+07	10.82%	0 105,05	24.00%	5.03 [+00	10.30%	21.30	0.5/	3.70
6 - 8	2.22E+09	11 23%	4 64E±07	42.479/	3.10E+03	21.09%	5.89E+06	19.59%	21.36	0.57	3.70
9 - 10	5 03E+09	14 27%	4.0411.00	12.47.70	1.12E+06	23.08%	8.00E+06	21.27%	20.92	0.51	3.60
2 7	5.77.00	14.57%	1.04E+08	16.14%	2.07E+06	26.74%	1.65E+07	24.72%	20.58	0.41	3.28
	5.5/E+09	17.86%	1.17E+08	20.29%	2.22E+06	30.66%	1.64E+07	28.16%	21.00	0.40	2.95
71 - 17	5.23E+09	21.14%	1.13E+08	24.29%	2.08E+06	34.33%	1.38E+07	31.04%	21.50	0.40	63
12 - 13	6.72E+09	25.34%	1.44E+08	29.41%	2.38E+06	38.54%	1.62E+07	34.43%	21 48	0.35	3 5
13 - 14	3.03E+09	27.24%	7.27E+07	32.00%	9.63E+05	40.24%	2.00E+06	34 84%	23.08		0.4
14 - 15	3.03E+09	29.14%	7.27E+07	34.58%	9.62E+05	41.95%	1.99F±06	35.26%	23.09	200	0.00
15 - 16	3.04E+09	31.04%	7.28E+07	37.16%	9.65E+05	43.65%	2.02E+06	35.68%	23.08	20.0	0.00
16 - 17	1.01E+10	37.35%	1.79E+08	43.52%	2 98F±06	4R 92%	2 34E,07	40 50%	17.00	20.0	0.0
17 - 18	2.89E+10	55.44%	4 67F±08	80 00%	9 375 0	69 70%	6.04F-407	40.36%	08.71	0.30	2.33
18 - 19	4 88F±10	85 07%	7.74 1.00	00.03 /6	6.37 F+06	03.72%	8.01 = +0/	57.34%	16.15	0.29	2.77
10 00	0.047.70	400.00	0.715+00	07.40%	1.41E+0/	88.59%	1.39E+08	86.49%	15.82	0.29	2.86
07 - 61	Z.Z4E+10	100.00%	3.53E+08	100.00%	6.46E+06	100.00%	6.45E+07	100.00%	15.73	0.29	2.88
Global Total	1.60E+11		2.82E+09		5 GGE 107		4 70E.00				
					3.00LT0/		4./8E+U8		17.63	0.35	2.99

Table G-6. Fuel burned, emissions, cumulative fractions of emissions, and emission indices as a function of altitude (summed over Latitude and Longitude) for the Mach 2.0 (Nominal EI(NOx)=15) HSCT fleet only, assuming passenger demand corresponding to 500 Mach 2.4 HSCTs flying on the 1993 AESA assessment network. (revised from NASA CR 4592)

Fuel	cum fuel	NOX	cum NOx	유	cum HC	8	cum CO	EI(NOx)	EI(HC)	EI(CO)
- 1	(%)	(kg/year)	(%)	(kg/year)	(%)	(kg/year)	(%)			
	2.52%	3.11E+07	2.12%	2.55E+06	8.81%	2.39E+07	9.75%	14.77	1.21	11.35
	3.45%	1.67E+07	3.25%	4.30E+05	10.30%	2.71E+06	10.85%	21.54		3.50
	4.38%	1.67E+07	4.39%	4.30E+05	11.79%	2.71E+06	11.96%	21.54		3.50
	5.30%	1.67E+07	5.53%	4.30E+05	13.27%	2.71E+06	13.06%	21.54		3.50
	6.23%	1.67E+07	6.67%	4.30E+05	14.76%	2.71E+06	14.17%	21.54		3.50
	7.16%	1.67E+07	7.80%	4.30E+05	16.25%	2.71E+06	15.27%	21.54		3.50
	8.09%	1.67E+07	8.94%	4.30E+05	17.74%	2.71E+06	16.38%	21.54		3.50
	9.05%	1.67E+07	10.08%	4.30E+05	19.22%	2.71E+06	17.48%	21.54		3.50
	10.39%	2.41E+07	11.72%	5.56E+05	21.15%	3.90E+06	19.07%	21.06		3.40
	13.35%	5.24E+07	15.29%	9.88E+05	24.56%	7.04E+06	21.94%	21.18		2.84
2.80E+09	16.70%	5.97E+07	19.35%	1.09E+06	28.32%	7.56E+06	25.03%	21.31	0.39	2.70
2.90E+09	20.17%	6.24E+07	23.60%	1.11E+06	32.17%	7.35E+06	28.02%	21.54		
3.82E+09	24.74%	8.15E+07	29.14%	1.33E+06	36.78%	9.46E+06	31.88%	21.32		
1.51E+09	26.55%	3.64E+07	31.62%	4.76E+05	38.42%	9.38E+05	32.26%	24.02		
	28.37%	3.64E+07	34.09%	4.76E+05	40.07%	9.38E+05	32.65%	24.02		0.62
	30.18%	3.65E+07	36.58%	4.78E+05	41.72%	9.54E+05	33.03%	23.99		0.63
	38.57%	1.19E+08	44.71%	2.05E+06	48.81%	1.77E+07	40.25%	17.04		2.53
	59.46%	2.79E+08	63.67%	5.04E+06	66.25%	4.92E+07	60.32%	15.96		2.85
2.53E+10	89.76%	3.99E+08	90.84%	7.30E+06	91.48%	7.27E+07	89.96%	15.76	0.29	2.87
8.56E+09	100.00%	1.35E+08	100.00%	2.47E+06	100.00%	2.46E+07	100.00%	15.73	0.29	2.88
0 26E 140		1 47E.00		2 R9F±07		2.45E+08		17.58	0.35	2.94
		1.4/ 1.40		£.03L⊤∨;		7.17.1			١	ı

·		

Appendix H. Altitude Distribution of Emissions for Year 2015 subsonic fleets

This appendix contains the tables which summarize the different Year 2015 subsonic emission scenarios occurring with fleets of 0, 500, and 1000 Mach 2.4 HSCTs. For each of the scenarios considered, the fuel burned and emissions (NOx, CO, and hydrocarbons) were summed over latitude and longitude and tabulated as a function of altitude in 1 km altitude increments (the resolution of the data set).

Cumulative fractions of fuel burned and emissions were calculated from the ground up to provide a simple way to evaluate how the emissions were distributed vertically. In addition, the effective emission index for each altitude band was calculated and tabulated.

The global total of fuel burned and emissions were calculated and listed at the bottom of each table. Also, included is the effective emission index for NOx, CO, and hydrocarbons, globally averaged over all locations and altitudes.

For the charts shown, the notation 1.00E+08 is equivalent to 1.00×10^8 . The emissions are in units of kilograms per year and the emission indices have units of grams of emissions per kilogram of fuel burned.

US Standard Atmosphere (1976) pressures and temperatures were used in the calculations. These altitudes correspond to the geopotential (pressure) altitudes of the US Standard Atmosphere grid.

Table H-1. Fuel burned, emissions, cumulative fractions of emissions, and emission indices as a function of attitude (Summed over Latitude and Longitude) for the 2015 scheduled subsonic passenger fleet, assuming 500 Mach 2.4 HSCTs are flying on the universal network.

\\	ruei (ko/vear)	cum fuel	NOX (kg/year)	cum NOX	HC (kg/year)	cum HC	CO (FG/FG/F	cum CO	EI(NOX) EI(HC) EI(CO)	EI(HC)	EI(CO)
	//) (2)	(ma Lau)	(6/	(ng/year)	(%)	(ng/year)	(%)			
0 - 1	2.61E+10	11.78%	2.50E+08	12.20%	3.06E+07	32.80%	3.40E+08	32.44%	9.56	1.17	12.99
1 - 2	6.95E+09	14.91%	8.75E+07	16.47%	6.37E+06	39.62%	6.03E+07	38.20%	_	0 92	8.67
2 - 3	6.09E+09	17.65%	7.48E+07	20.12%	5.44E+06	45.44%	5.13E+07	43.10%	,	0.89	8.43
3 - 4	7.81E+09	21.17%	1.05E+08	25.22%	4.94E+06	50.72%	4.52E+07	47.43%	•	0.63	5.79
4 - 5	6.68E+09	24.18%	8.18E+07	29.21%	5.47E+06	56.58%	4.71E+07	51.93%		0.82	7.06
2 - 6	6.11E+09	26.93%	7.26E+07	32.76%	4.52E+06	61.42%	4.72E+07	56.44%	11.89	0.74	7.73
2 - 9	5.19E+09	29.26%	5.98E+07	35.68%	3.63E+06	65.31%	4.05E+07	60.30%		0.70	7.80
7 - 8	5.52E+09	31.75%	6.09E+07	38.65%	3.99E+06	69.58%	4.37E+07	64.48%	11.03	0.72	7.93
6 - 8	6.13E+09	34.51%	6.54E+07	41.84%	4.23E+06	74.11%	4.58E+07	68.86%	10.67	0.69	7.48
9 - 10	6.73E+09	37.54%	6.67E+07	45.09%	4.17E+06	78.57%	4.39E+07	73.05%	9.91	0.62	6.52
10 - 11	4.32E+10	57.02%	3.39E+08	61.62%	6.44E+06	85.47%	9.47E+07	82.10%	7.83	0.15	2.19
11 - 12	9.54E+10	100.00%	7.86E+08	100.00%	1.36E+07	100.00%	1.87E+08	100.00%	8.24	0.14	1.96
Global Total	2.22E+11		2.05E+09		9.34E+07		1.05E+09	1	9.23	0.45	4.71

Table H-2. Fuel burned, emissions, cumulative fractions of emissions, and emission indices as a function of altitude (Summed over Latitude and Longitude) for the 2015 scheduled subsonic passenger fleet assuming 1000 Mach 2.4 HSCTs are flying on the universal network.

	Fuel	cum fuel	×ON	cum NOx	오	cum HC	8	cum CO	EI(NOX) EI(HC) EI(CO)	EI(HC)	EI(CO)
(kg/year)		(%)	(kg/year)	(%)	(kg/year)	(%)	(kg/year)	(%)			
2.48E+10		12.61%	2.32E+08	12.83%	2.92E+07	33.56%	3.27E+08	33.46%	9.32	1.18	13.18
6.66E+09		15.99%	8.24E+07	17.40%	6.11E+06	40.57%	5.81E+07	39.39%	12.36	0.92	8.71
5.83E+09		18.95%	7.03E+07	21.29%	5.19E+06	46.54%	4.93E+07	44.43%	,	0.89	8.46
7.41E+09		22.72%	9.71E+07	26.68%	4.72E+06	51.95%	4.34E+07	48.86%	13.10	0.64	5.85
6.40E+09		25.97%	7.70E+07	30.95%	5.25E+06	57.97%	4.52E+07	53.49%	12.03		7.07
5.84E+09		28.93%	6.81E+07	34.72%	4.29E+06	62.90%	4.53E+07	58.12%			7.76
4.93E+09		31.43%	5.55E+07	37.80%	3.41E+06	66.82%	3.89E+07	62.09%	11.26		7.88
5.24E+09		34.09%	5.64E+07	40.93%	3.75E+06	71.13%	4.19E+07	%26.32%			8.00
5.81E+09		37.04%	6.05E+07	44.29%	3.96E+06	75.68%	4.38E+07	70.85%			7.54
6.31E+09		40.25%	6.13E+07	47.68%	3.90E+06	80.15%	4.18E+07	75.12%			6.62
3.89E+10		29.99%	2.97E+08	64.17%	5.84E+06	86.86%	8.77E+07	84.09%	7.65		2.26
7.88E+10		100.00%	6.46E+08	100.00%	1.14E+07	100.00%	1.56E+08	100.00%	8.20		1.98
1.97E+11			1.80E+09		8.71E+07		9.78E+08		9.16	0.44	4.97

Table H-3. Fuel burned, emissions, cumulative fractions of emissions, and emission indices as a function of altitude (Summed over Latitude and Longitude) for the 2015 scheduled subsonic passenger fleet assuming no HSCTs are flying on the universal network.

Altitude Band (km)	Fuel (kg/vear)	cum fuel (%)	NOx (kg/vear)	cum NOx	HC (kg/vear)	cum HC	CO	com CO	EI(NOx) EI(HC) EI(CO)	EI(HC)	EI(CO)
	,		, , , , ,		/mar / Ent	2	Ima Laul	(5)			
0 - 1	2.73E+10	10.92%	2.67E+08	11.51%	3.18E+07	32.05%	3.49E+08	31.44%	9.78	1.17	12.79
1 - 2	7.20E+09	13.80%	9.22E+07	15.49%	6.57E+06	38.66%	6.19E+07	37.01%	_	0.91	8.60
2 - 3	6.32E+09	16.33%	7.92E+07	18.90%	5.63E+06	44.33%	5.29E+07	41.78%	•	0.89	8.38
3 - 4	8.18E+09	19.60%	1.12E+08	23.71%	5.13E+06	49.50%	4.68E+07	45.99%	•	0.63	5.72
4 - 5	6.92E+09	22.37%	8.61E+07	27.42%	5.67E+06	55.20%	4.87E+07	50.37%			7.03
5 - 6	6.35E+09	24.91%	7.68E+07	30.73%	4.73E+06	29.96%	4.87E+07	54.75%		-	7.67
2 - 9	5.44E+09	27.08%	6.41E+07	33.49%	3.82E+06	63.81%	4.20E+07	58.53%	11.79	0.70	7.72
7 - 8	5.78E+09	29.40%	6.52E+07	36.30%	4.21E+06	68.05%	4.53E+07	62.61%	11.27		7.84
6 - 8	6.42E+09	31.97%	7.00E+07	39.31%	4.47E+06	72.55%	4.75E+07	66.88%	10.90	_	7.40
9 - 10	7.50E+09	34.97%	7.53E+07	42.56%	4.45E+06	77.02%	4.62E+07	71.04%	10.04		6.15
10 - 11	5.04E+10	55.13%	4.04E+08	59.95%	7.30E+06	84.37%	1.06E+08	80.54%	8.01	0.14	2.09
11 - 12	1.12E+11	100.00%	9.29E+08	100.00%	1.55E+07	100.00%	2.16E+08	100.00%	8.28	0.14	1.93
Global Total	2.50E+11		2.32E+09		9.94E+07		1.11E+09		9.28	0.40	4.44

Table H-4. Fuel burned, emissions, cumulative fractions of emissions, and emission indices as a function of attitude (Summed over Latitude and Longitude) for the 2015 scheduled subsonic cargo fleet (unchanged from NASA Contractor Report 4592)

EI(CO)	17.35		12.36	8.65	12.30	12.16	11.70	11.59	10.68	10.86	2.97	2.13	4.90
EI(HC)	2.47	1.77	1.90	1.27	1.84	1.85	1.82	1.84	1.71	1.81	0.36	0.17	0.63
EI(NOx)	9.52	12.81	13.32	13.71	12.36	11.99	11.83	10.97	10.52	9.94	8.72	7.73	8.69
cum CO EI(NOx) EI(HC) EI(CO)	26.59%	31.07%	35.64%	39.69%	43.81%	48.03%	52.13%	56.53%	60.84%	65.19%	72.21%	100.00%	
CO (ka/vear)	7.36E+06	1.24E+06	1.26E+06	1.12E+06	1.14E+06	1.17E+06	1.13E+06	1.22E+06	1.19E+06	1.20E+06	1.94E+06	7.69E+06	2.77E+07
cum HC	29.38%	34.54%	40.00%	44.61%	49.41%	54.39%	59.33%	64.76%	70.12%	75.75%	82.43%	100.00%	
HC (ka/vear)	1.05E+06	1.84E+05	1.95E+05	1.64E+05	1.71E+05	1.78E+05	1.76E+05	1.93E+05	1.91E+05	2.00E+05	2.38E+05	6.26E+05	3.56E+06
cum NOx	8.23%	10.94%	13.72%	17.34%	19.68%	22.03%	24.36%	26.72%	29.11%	31.36%	42.99%	100.00%	
NOx (ka/vear)	4.04E+06	1.33E+06	1.36E+06	1.78E+06	1.15E+06	1.15E+06	1.15E+06	1.15E+06	1.17E+06	1.10E+06	5.71E+06	2.80E+07	4.91E+07
cum fuel (%)	7.52%	9.35%	11.16%	13.46%	15.10%	16.81%	18.52%	20.39%	22.36%	24.33%	35.95%	100.00%	
Fuel (ka/vear)	4.24E+08	1.04E+08	1.02E+08	1.30E+08	9.27E+07	9.62E+07	9.69E+07	1.05E+08	1.12E+08	1.11E+08	6.54E+08	3.62E+09	5.64E+09
Altitude Band (km)	0 - 1	1 - 2	2 - 3	3 - 4	4 - 5	9 - 9	2 - 9	7 - 8	6 - 8	9 - 10	10 - 11	11 - 12	Global Total

	·			

Appendix I. 3-Dimensional Scenario Data Format

The three dimensional emission scenario data files calculated by Boeing were delivered to NASA Langley electronically in a slightly different format than that used previously (Ref. 1). In addition to fuel and emissions, the total miles flown within in a cell is also provided. The format is now:

i, j, k; fuel(lb/day); NOx(lb/day); CO(lb/day); HC(lb/day); distance (nautical miles/day)

Only non-zero values are included in the ASCII data files.

Altitude:

Index k

means emissions in the band from altitude k to k+1 i.e. index 19 is emissions in the 19-20 km band

Values run from 0 to 22

Latitude:

Index i

means emissions in the band from latitude i to i+1

values run from 0 to 179

For i<=89 northern hemisphere

index 0 is emissions from equator to 1 degree N

For i>=90 southern hemisphere

index 90 is emissions from equator to 1 degree S

index 179 is emissions from 89S-90S

<u>Lonaitude:</u>

Wrap all the way around the globe.

Index i

means emissions in the longitude band j to j+1

values run from 0 to 359

For j<=179 east of prime meridian

index 0 is emissions from 0-1E

index 179 is emissions from 179E-180E

For i>=180 west of prime meridian

index 180 is emissions from -180W - -179W

index 359 is emissions from -1W - 0

Form Approved REPORT DOCUMENTATION PAGE OMB No. 0704-0188 Public reporting burden for this collection of information is estimated to average 1 hour per response, including the time for reviewing instructions, searching existing data sources, gethering and maintaining the data nandal, and completing and reviewing the collection of information. Send comments regarding this burden estimate or any other aspect of this collection of information, including suggestions for reducing this burden, to Washington Headquarters Services, Directorate for Information Operations and Reports, 1215 Jefferson Davis Highway, Suite 1204, Arlington, VA 22202-4302, and to the Office of Management and Budget, Paperwork Reduction Project (9704-9186), Washington, DC 20503. Information Operations and Reports, 1215 Jeffer 61 (0704-0188), Weshington, DC 20503. 1. AGENCY USE ONLY (Leave blank) 2. REPORT DATE 3. REPORT TYPE AND DATES COVERED July 1995 Contractor Report 4. TITLE AND SUBTITLE S. FUNDING NUMBERS Aircraft Emission Inventories Projected in Year 2015 for a High Speed Civil Transport (HSCT) Universal Airline Network C NAS1-19360 WU 537-09-23-02 6. AUTHOR(S) Steven L. Baughcum and Stephen C. Henderson 7. PERFORMING ORGANIZATION NAME(S) AND ADDRESS(ES) 8. PERFORMING ORGANIZATION REPORT NUMBER Boeing Commercial Airplane Group P. O. Box 3707 Seattle. WA 98124-2207 9. SPONSORING/MONITORING AGENCY NAME(S) AND ADDRESS(ES) 10. SPONSORING/MONITORING National Aeronautics and Space Administration AGENCY REPORT NUMBER Langley Research Center Hampton, VA 23681-0001 **NASA CR-4659** 11. SUPPLEMENTARY NOTES Langley Technical Monitor: Donald L. Maiden Final Report - Task 40 12a. DISTRIBUTION/AVAILABILITY STATEMENT 12b. DISTRIBUTION CODE Unclassified - Unlimited Subject Category 46 13. ABSTRACT (Maximum 200 words) This report describes the development of a three-dimensional database of aircraft fuel burn and emissions (fuel burned,NOx, CO, and hydrocarbons) from projected fleets of high speed civil transports (HSCTs) on a universal airline network. Inventories for 500 and 1000 HSCT fleets, as well as the concurrent subsonic fleets, were calculated. The objective of this work was to evaluate the changes in geographical distribution of the HSCT emissions as the fleet size grew from 500 to 1000 HSCTs. For this work, a new expanded HSCT network was used and flights projected using a market penetration analysis rather than assuming equal penetration as was done in the earlier studies. Emission inventories on this network were calculated for both Mach 2.0 and Mach 2.4 HSCT fleets with NOx cruise emission indices of approximately 5 and 15 grams NOx/kilogram fuel. These emissions inventories are available for use by atmospheric scientists conducting the Atmospheric Effects of Stratospheric Aircraft (AESA) modeling studies. Fuel burned and emissions of nitrogen oxides (NOx as NO2), carbon monoxide, and hydrocarbons have been calculated on a 1 degree latitude x 1 degree longitude x 1 kilometer altitude grid and delivered to NASA as electronic files. 15. NUMBER OF PAGES aircraft emissions, ozone impact, high speed civil transport, 126 16. PRICE CODE emissions inventory, atmospheric impact A07 17. SECURITY CLASSIFICATION 18. SECURITY CLASSIFICATION SECURITY CLASSIFICATION 20. LIMITATION OF ABSTRACT OF REPORT OF THIS PAGE OF ABSTRACT Unclassified Unclassified Unclassified

1			